

AircraftFire Project

Fire risks assessment and increase of passenger survivability

FP7 EASN Project - EU Grant Agreement n° 265612

2011 - 2013

www.aircraftfire.eu



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1/ Presentation of the AircraftFire project and first results

2/ Fire performance of aeronautical composites

- New experimental setup
- Fire behaviour of composite materials

The AircraftFire Project



Evaluation of fire threats and passenger survivability in new generation of aircrafts

- Characterisation of the fire performance of composite materials (physical/chemical/thermal flammability and burning properties) for aircraft design and fire safety analysis (modelling)
- Development and validation physical models correlated to the evolution of the fire scenarios,
- Modelling of the cabin fire growth and passenger evacuation
- Recommendations for efficient industrial technologies

The fire threat in new generation of aircrafts

Aluminium is substituted by **flammable composites** for decorative panels, hull, wing, cowling, structure, etc.

The fire threat can significantly increase due to...

- The flammability of materials in high temperature environment
- The toxicity of the smokes
- The total aircraft fuel load

With impact on the fire development and the passenger evacuation

Higher energy supply for avionics and electronics

➔ ***fire risks (ignition,...)***

Material fire performance Fire Growth and Evacuation

1/ Material performance during fire (experimental)

- ✓ Material characterisation and behaviour during fire
- ✓ Ranking of material performances
- ✓ Behaviour under low pressure (partly simulation of altitude)
- ✓ Behaviour under load

Work Package 3

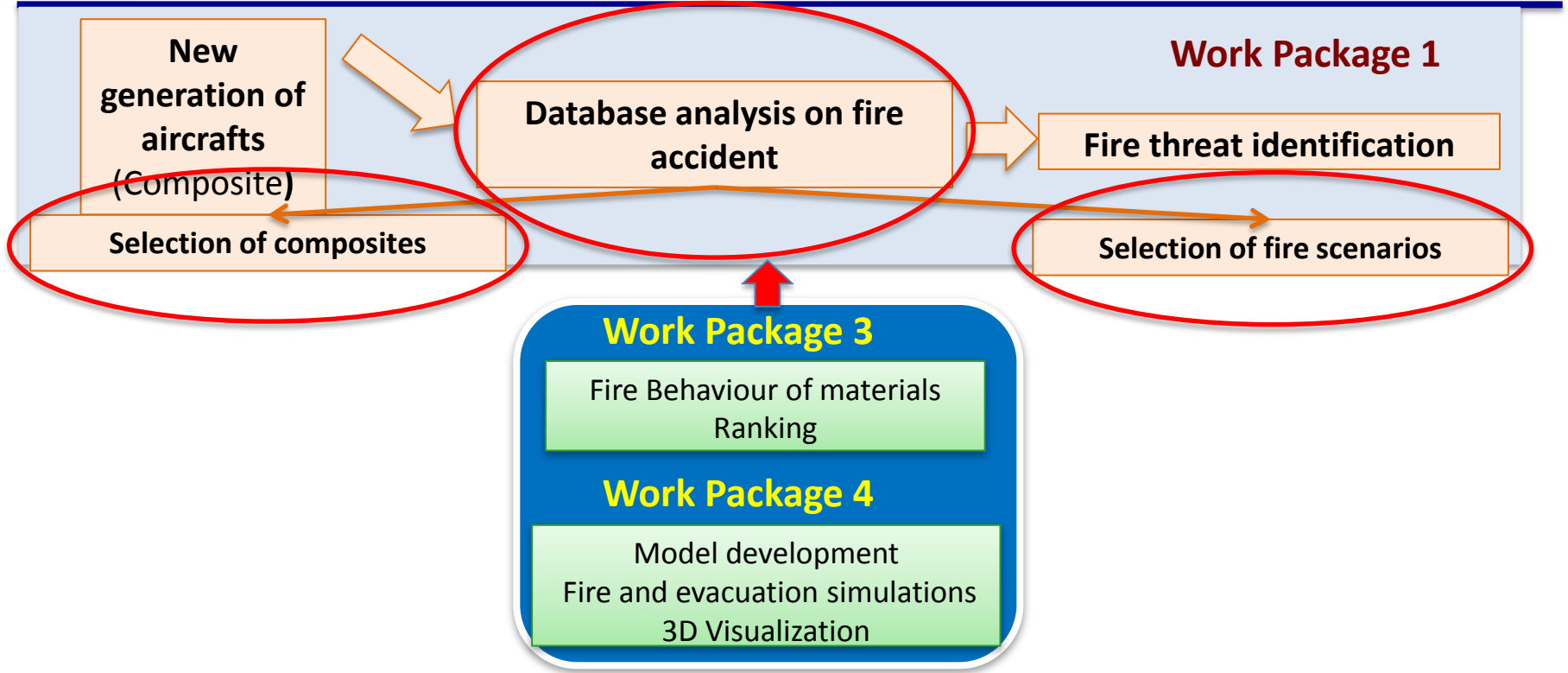
Fire Behaviour of materials
Ranking

Work Package 4

Model development
Fire and evacuation simulations
3D Visualization

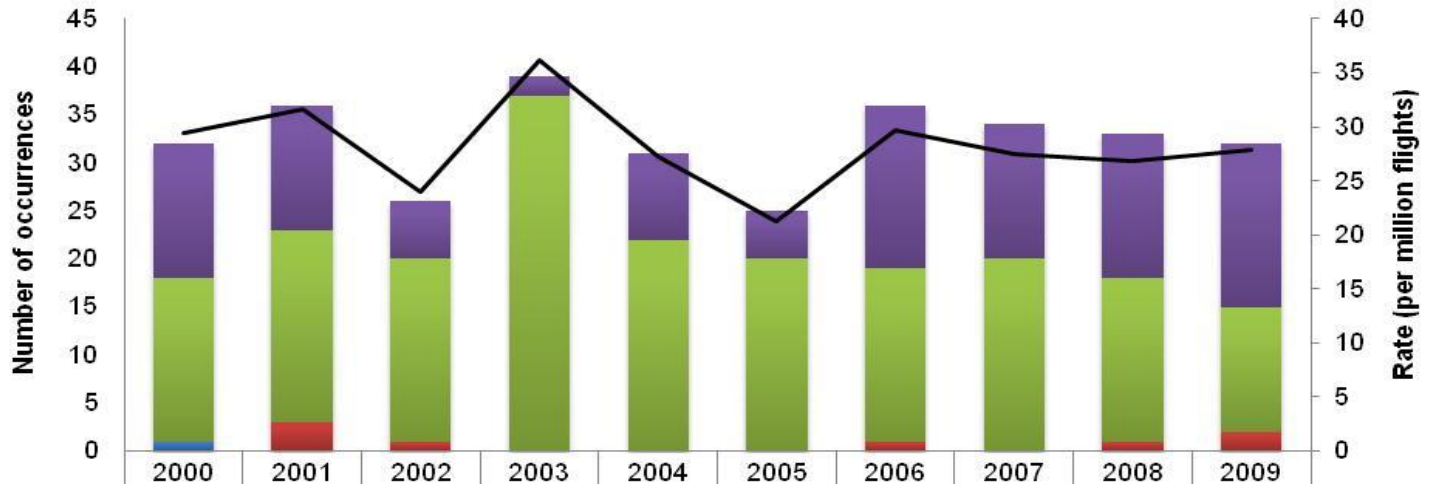
2/ Fire growth and evacuation (modelling)

- The enhancement of a full scale modelling of fire development (**SMARTFIRE**) in new generation of aircrafts;
- The adaptation and enhancement of a numerical evacuation model (**airEXODUS**) during post-crash.
- 3D Visualisations



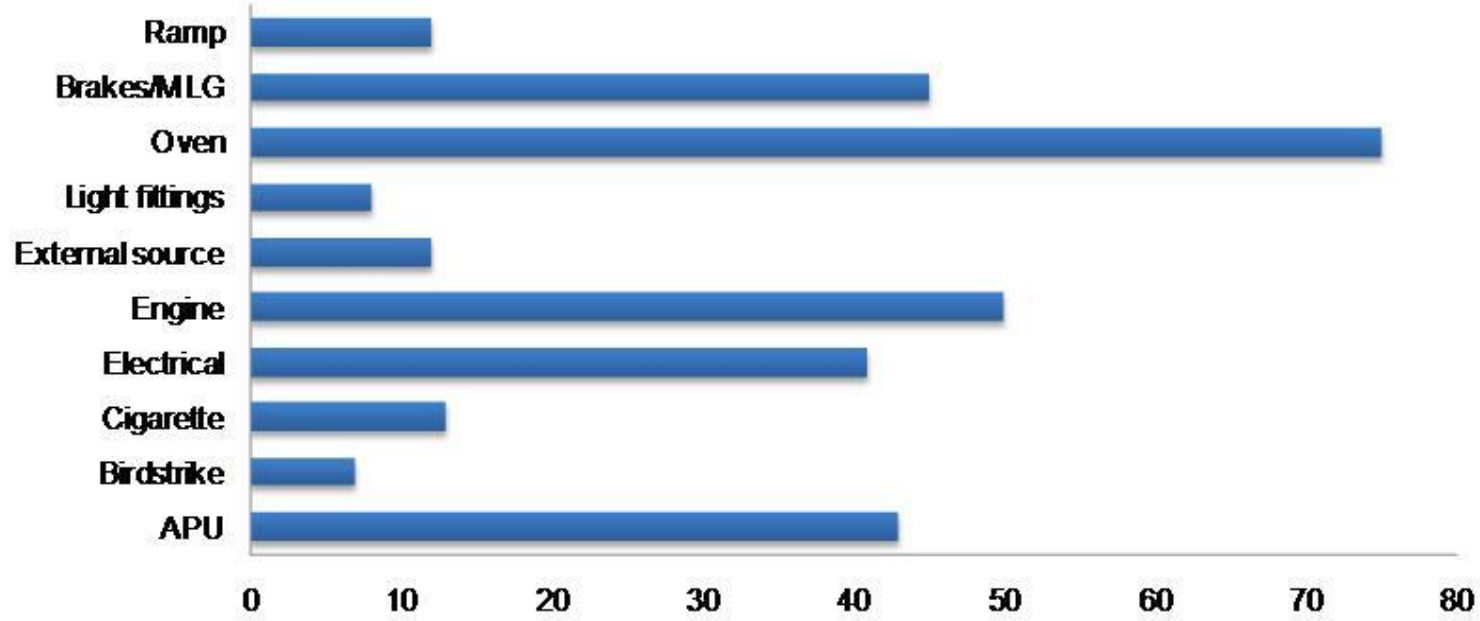
Fire occurrences by severity grade

Number and Rate of Fire Related Occurrences (UK Fleet) A-High Severity and D Low Severity



	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009
D	14	13	6	2	9	5	17	14	15	17
C	17	20	19	37	22	20	18	20	17	13
B	0	3	1	0	0	0	1	0	1	2
A	1	0	0	0	0	0	0	0	0	0
— Rate per million flights	29.42	31.69	24.01	36.17	27.27	21.28	29.74	27.46	26.89	27.82

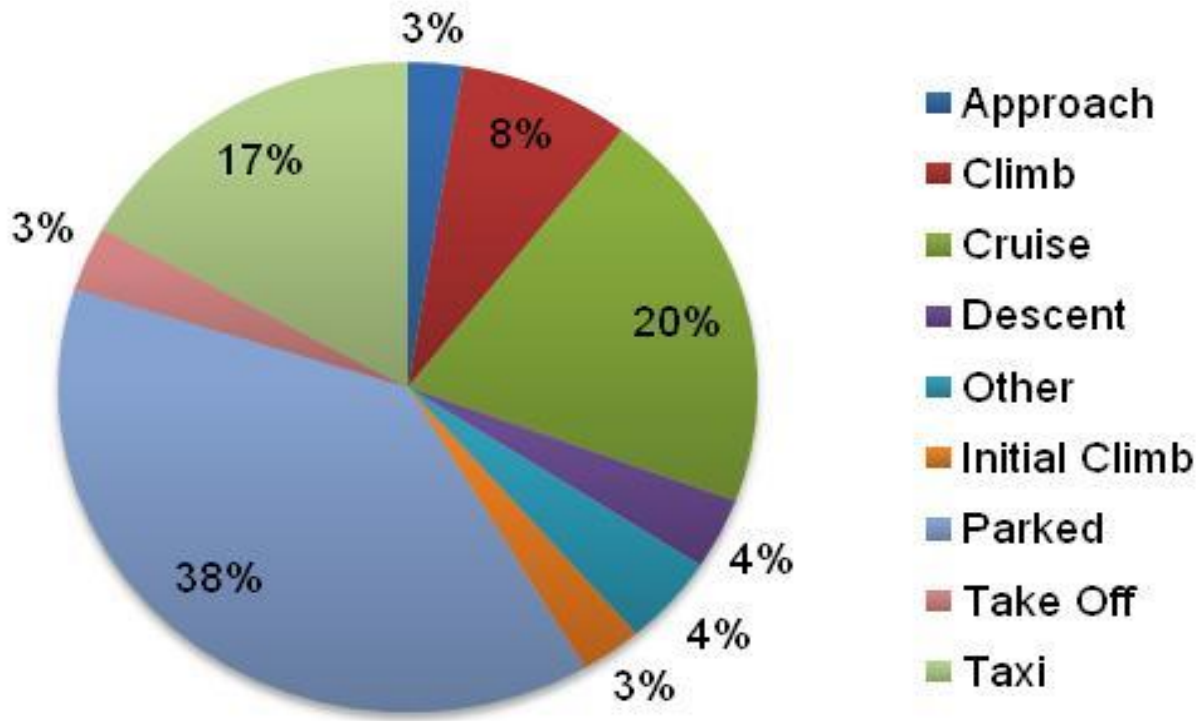
Causal factors for Fire occurrences



	APU	Birdstrike	Cigarette	Electrical	Engine	External source	Light fittings	Oven	Brakes/M LG	Ramp
■ Total	43	7	13	41	50	12	8	75	45	12

number of occurrences

Distribution of Fire occurrences by phase of flight



Composite materials in aircrafts

A composite material =
Matrix + Fibres
(1D fibres or woven fabric)

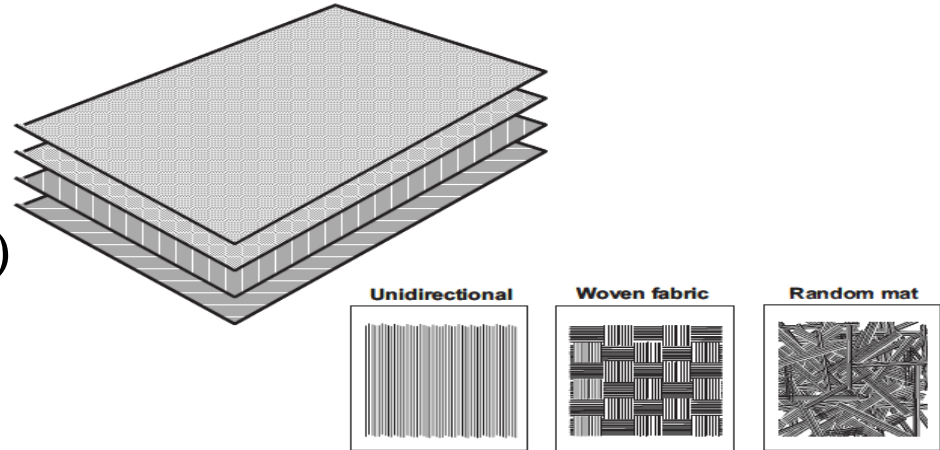


Figure 6.1. Ply structure of laminated composites and common examples of ply architecture.

5 Thermosets

- **Carbon fibres reinforced epoxy composites** (hull, wing, structure)
flammable and decompose when exposed to fire
- **Glass fibres reinforced phenolic composites** (decorative panels)
low flammability and good fire resistance

2 Thermoplasts

- **Seats, next aircraft generation**
better mechanical properties, recycling

5 Cabin Materials

- **Cabling, seating, thermo-acoustic, carpet,...**

CAA, EADS, Airbus

➤ Hidden zone fire

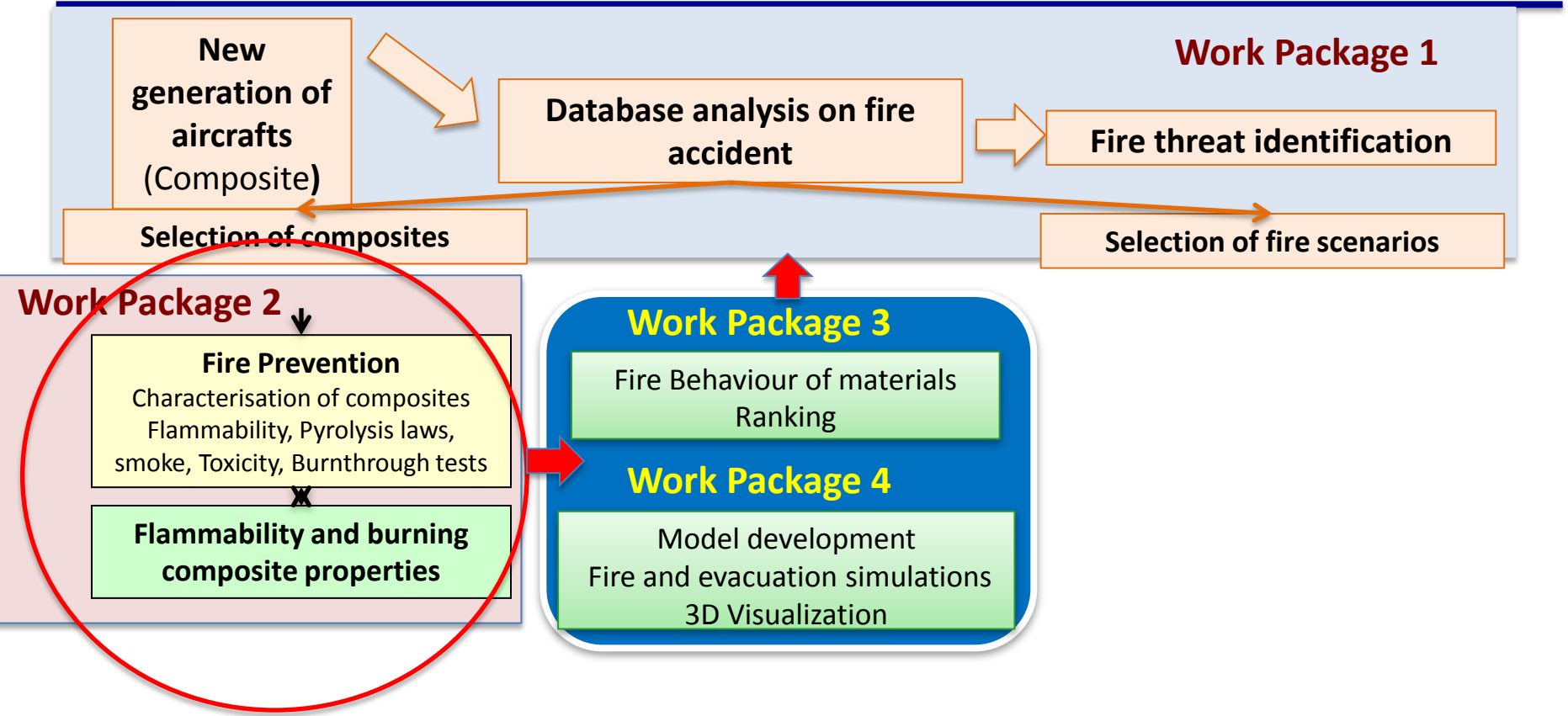
- ✓ Fire spread, fire propagation

➤ In-flight fire

- ✓ Flammability of materials under load and at low pressure + flame impact
- ✓ Sustainability of flame in altitude

➤ Post-crash fire

- ✓ Kerosene pool fire modelling
- ✓ Fire growth and evacuation
 - Post-crash fire with cabin integrity
 - Post-crash fire with rupture of the cabin or cracks of the skin

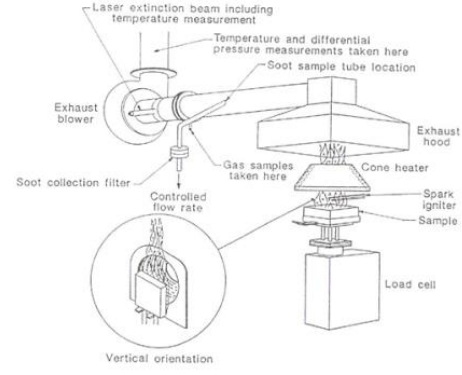


Methodology to determine material flammability properties

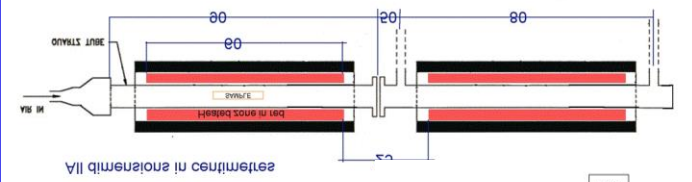
Key Flammability properties	Techniques
Conductivity, Specific heat, Heat of pyrolysis	MDSC
Glass transition temperature, Melting temperature, Heat of melting, Heat of pyrolysis, Specific heat	DSC
Ignition temperature (or the critical heat flux) % of residues, Kinetic parameters for reaction (i.e. activation energy and pre-exponential factor)	TGA
Quantification and history of gases emission	TGA - FTIR
Heat of combustion, efficiency of combustion Heat released rate / mass loss rate, CO, CO ₂ , smoke fields Smoke point height	Cone calorimeter
Influence of the ambient medium, equivalence ratio	Universal flammability apparatus (UFA)
Optical density of smoke	Smoke chamber

Methodology to determine material flammability

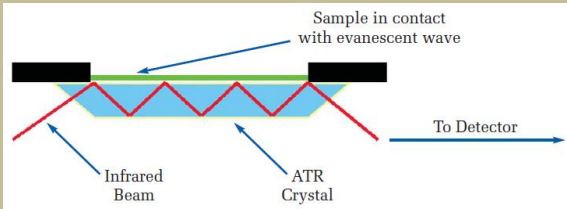
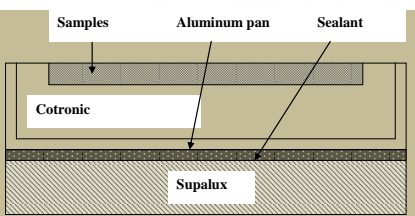
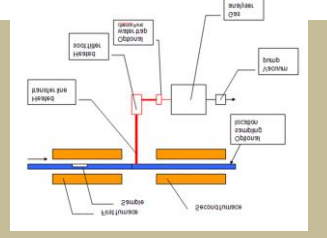
Cone calorimeter



Universal Flammability Apparatus

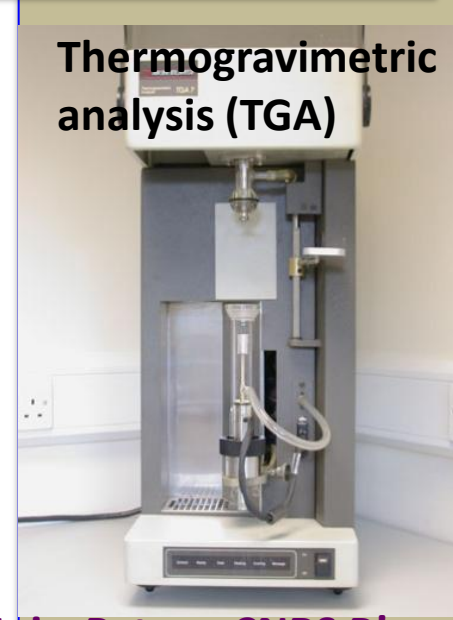


Tube furnace

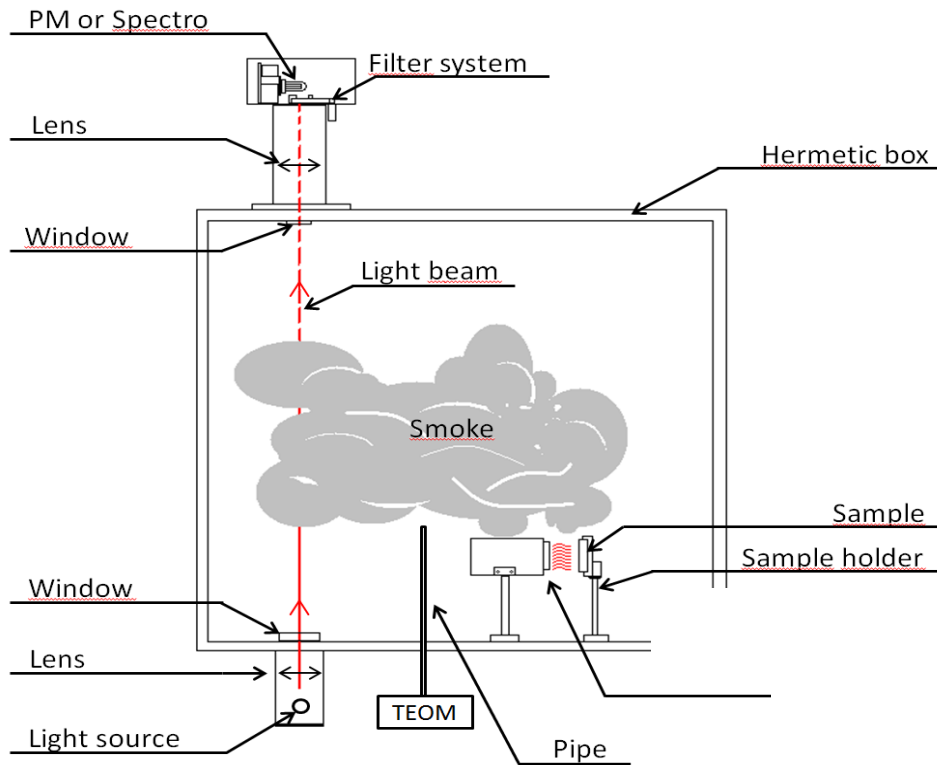


FTIR Spectroscopy: Attenuated Total Reflectance (ATR)

Thermogravimetric analysis (TGA)



**Objectives: measurement of the optical properties of smokes
 ==> correlation with their concentration and size**



Transmittance: $T = \frac{I}{I_0}$

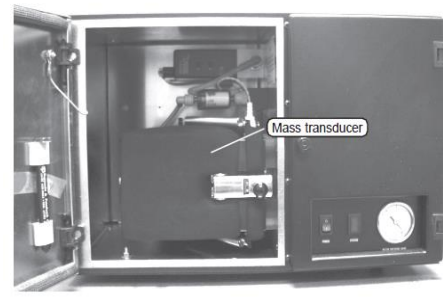
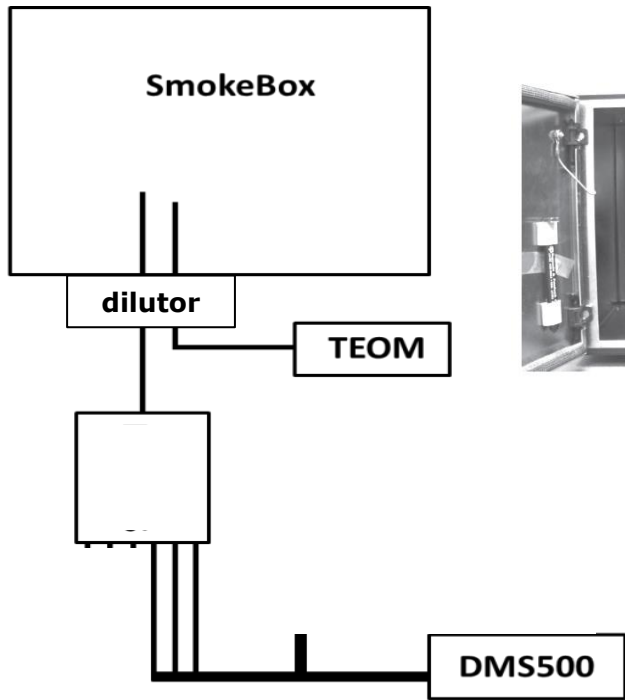
optical density $D = \log\left(\frac{1}{T}\right)$

Specific optical density: $D_s = \frac{V}{AL} D$

Extinction coefficient $K_{ext} = \frac{1}{L} \ln\left(\frac{1}{T}\right)$

CORIA

Smoke sampling and devices for measuring particle parameters



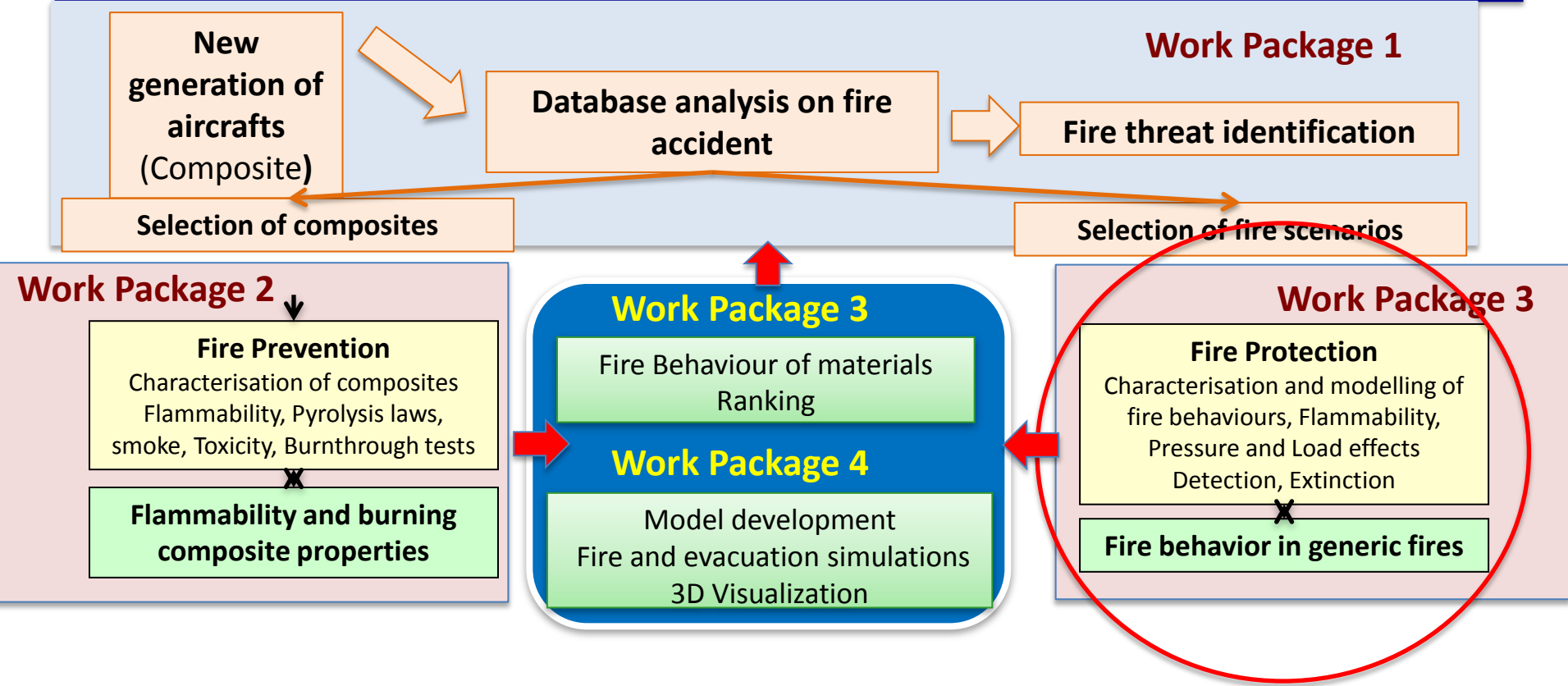
TEOM: Mass concentration
(tapered element oscillating microbalance)



DMS: particles size distribution

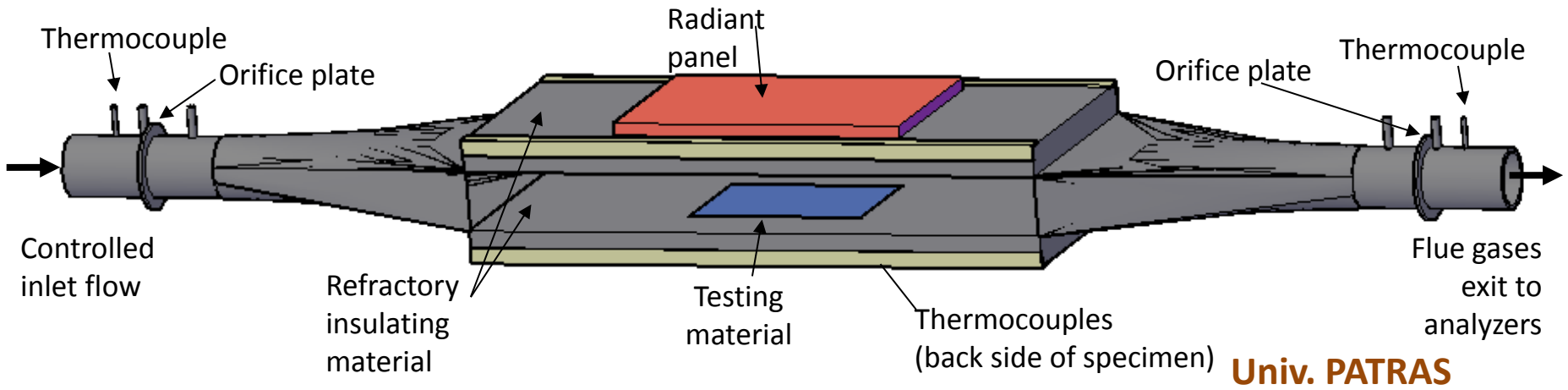
CORIA

AircraftFire: Organisation



Objective: To evaluate the consequences of fire in hidden zones, and its propagation into cabin and cockpit

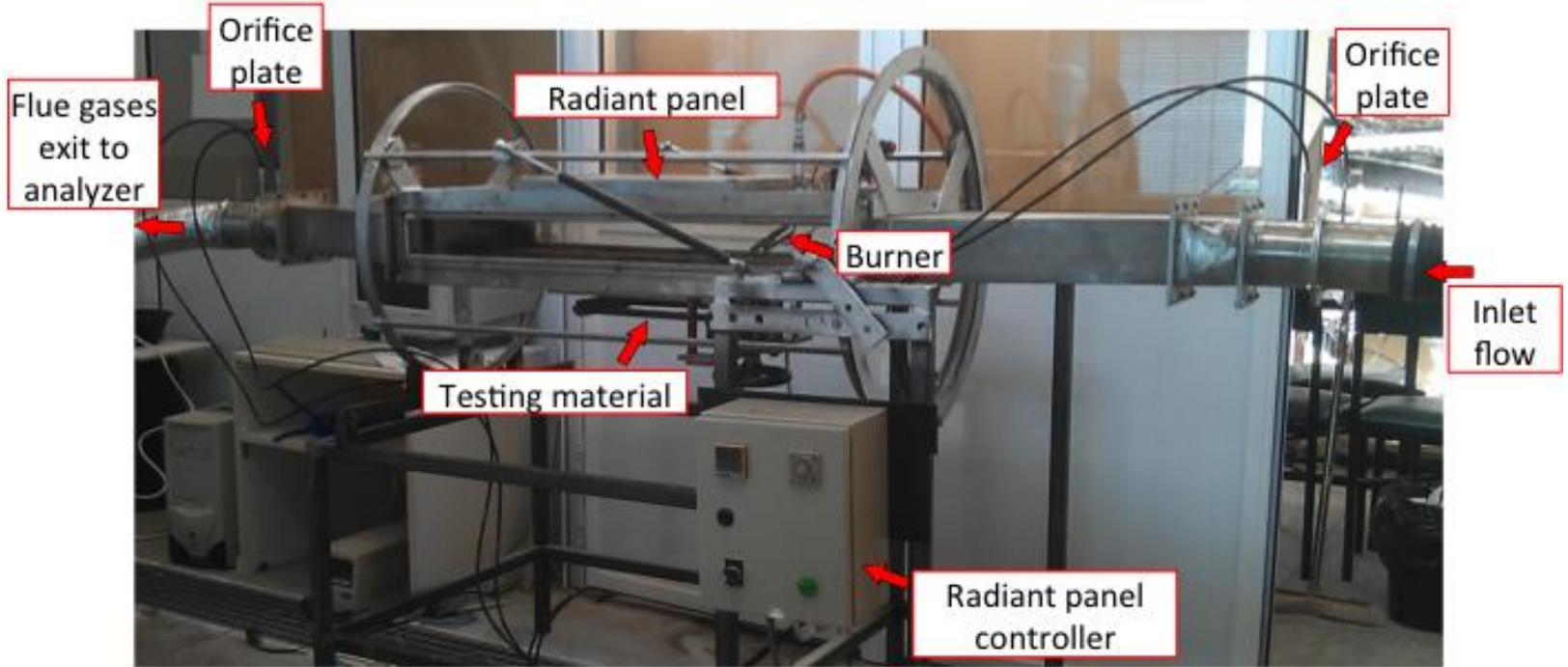
- The effect of under ventilation and of the depletion of oxygen
- Smouldering
- Fire spreading from a local initial fire
- Presence of unburned pyrolysis gases which may ignite if oxygen concentration is increased
- Burnthrough related phenomena



Univ. PATRAS

Generic Hidden Zone Fire

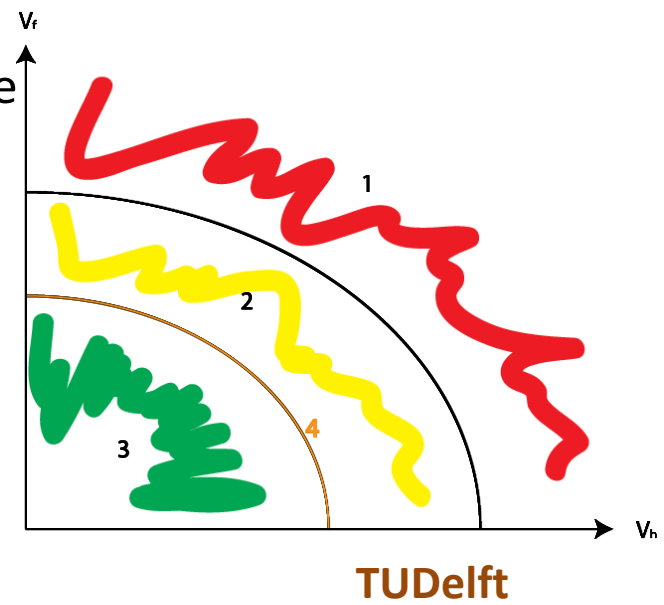
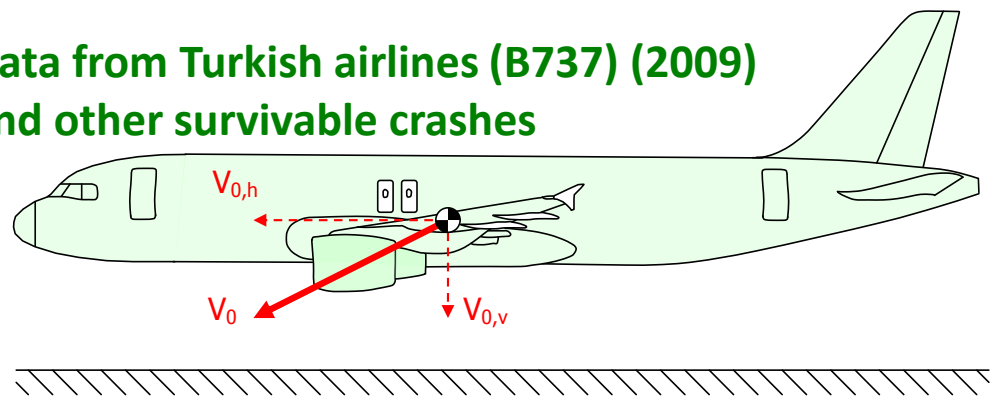
Univ. of Patras Experimental device

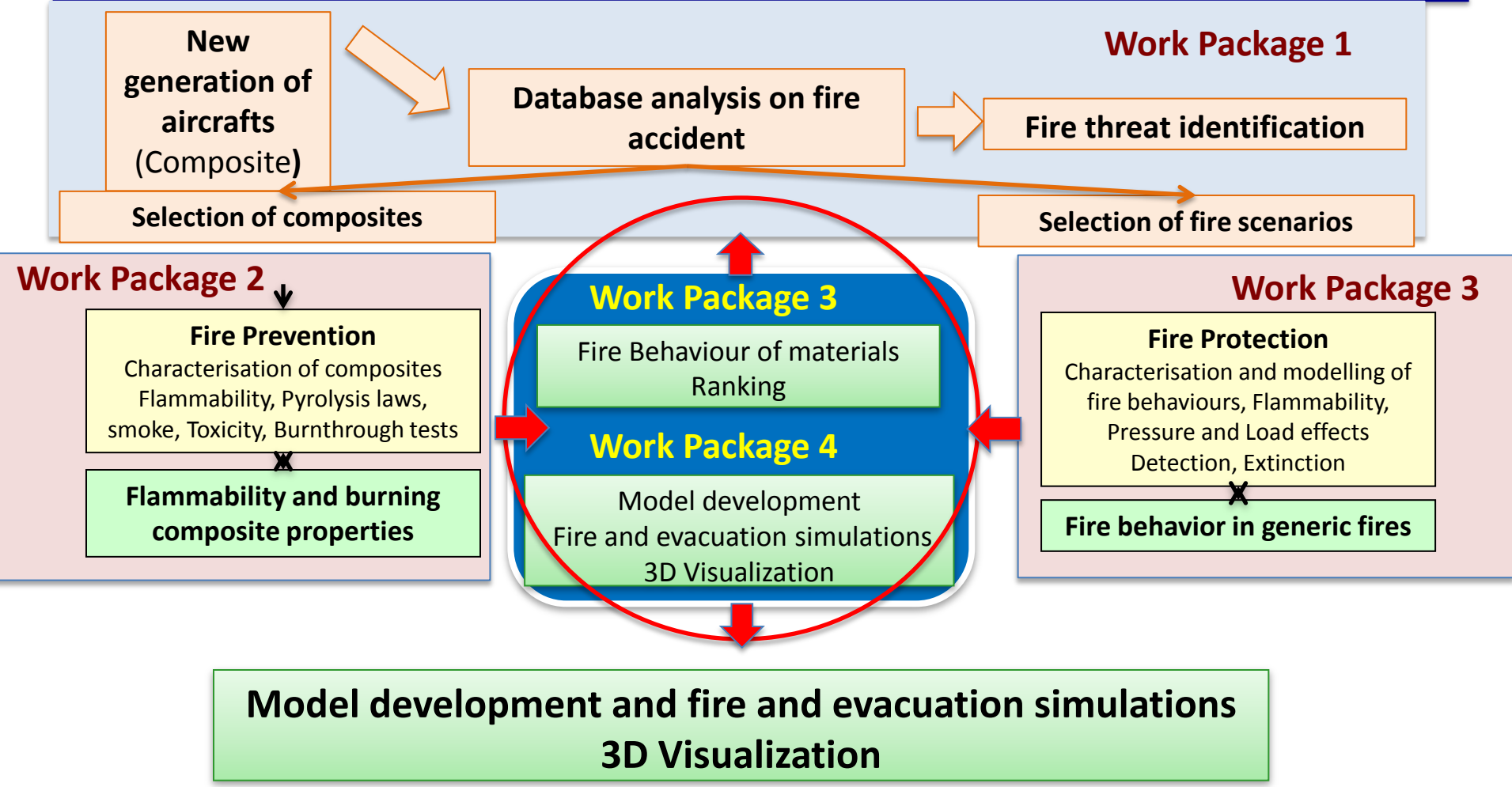


Create dynamic models to compare crash between metallic and composite aircrafts

- Therefore compare existing metallic body with composite
- Can compare the crash characteristics of an A320/B737 with simulated performance of a composite
- Examine forward velocity effects
 - Certification vertical drop only
 - Confirm model with actual crash response

Data from Turkish airlines (B737) (2009) and other survivable crashes

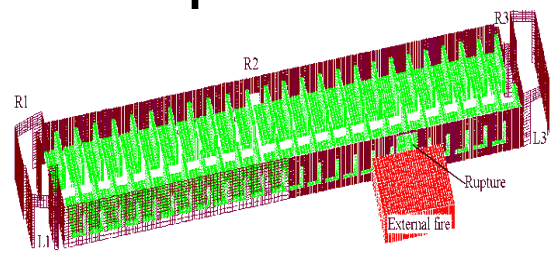
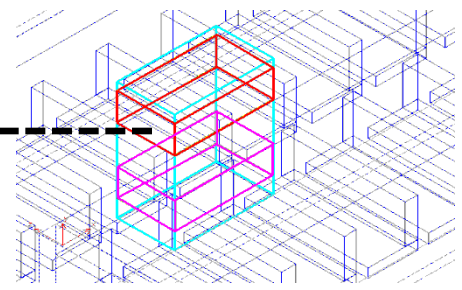




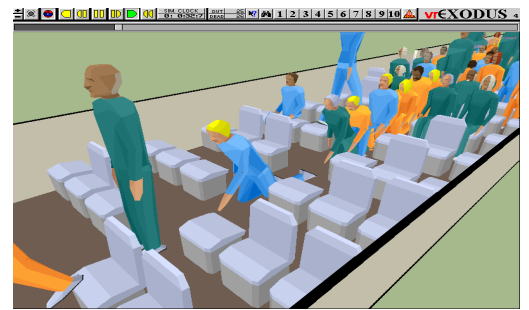
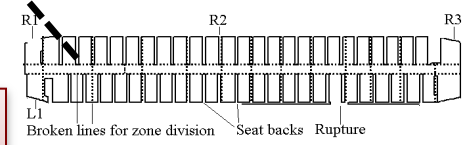
An Application of the Fire/Evacuation Methodology: Manchester Airport B737 Fire August 22nd, 1985

SMARTFIRE CFD
Fire Simulation

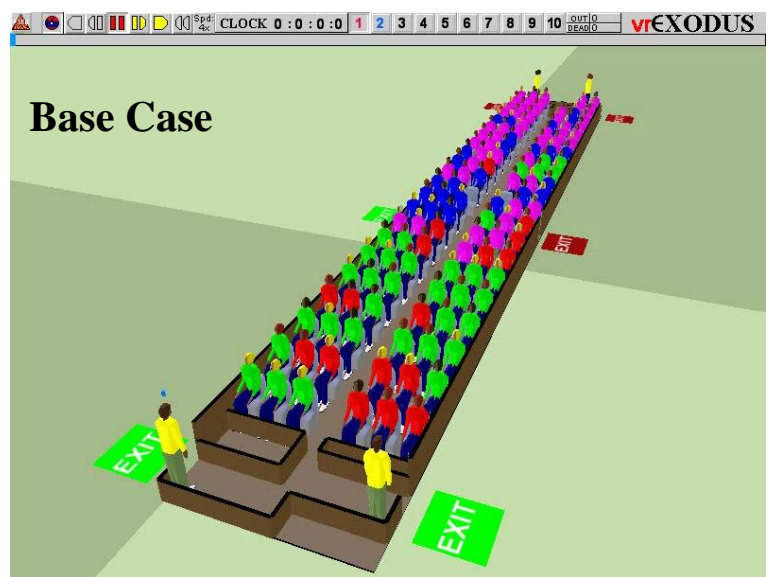
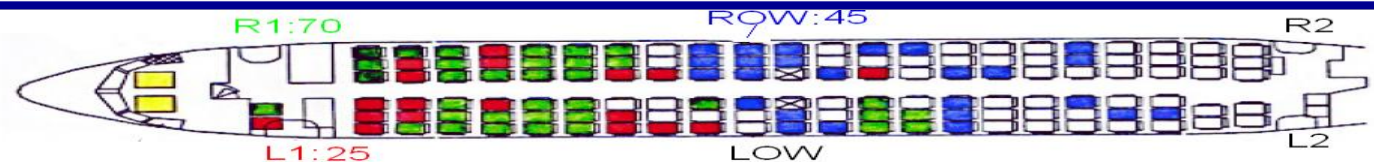
Fire Hazards at Specified Zones



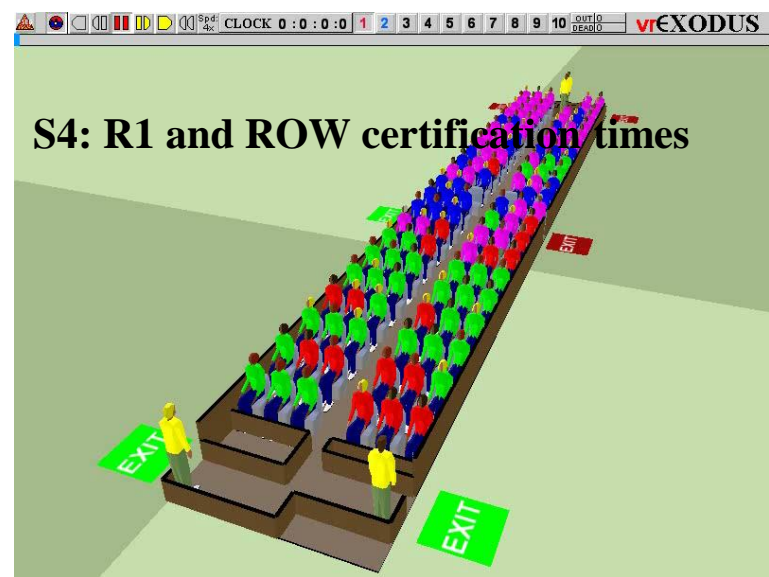
airEXODUS Evacuation Simulation



Impact of Exit Opening Times On Evacuation

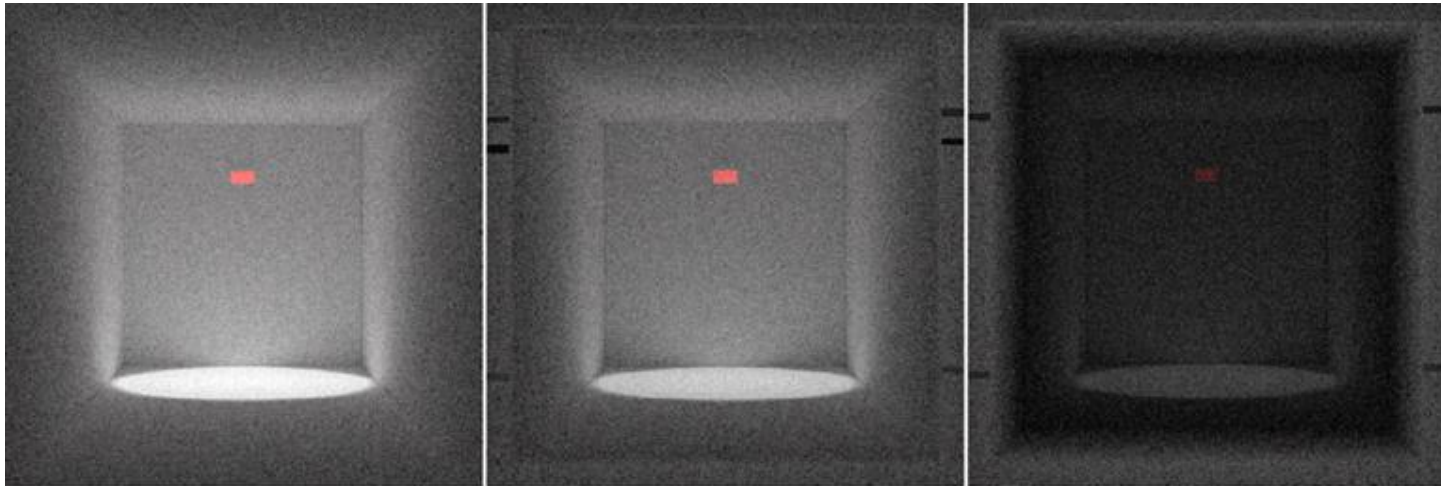


Base Case: the reconstruction with the actual times to open the exits in the accident **L1(25s), R1 (70s), ROW (45s), R2 (0s)**



Scenario 4: **10s** for R1 and **12s** for ROW – ideal case, all exits opened as planned

**Could the loss of life have been significantly reduced if the R1 exit was opened earlier?
Did the delay in opening the ROW exit impact survivability?**

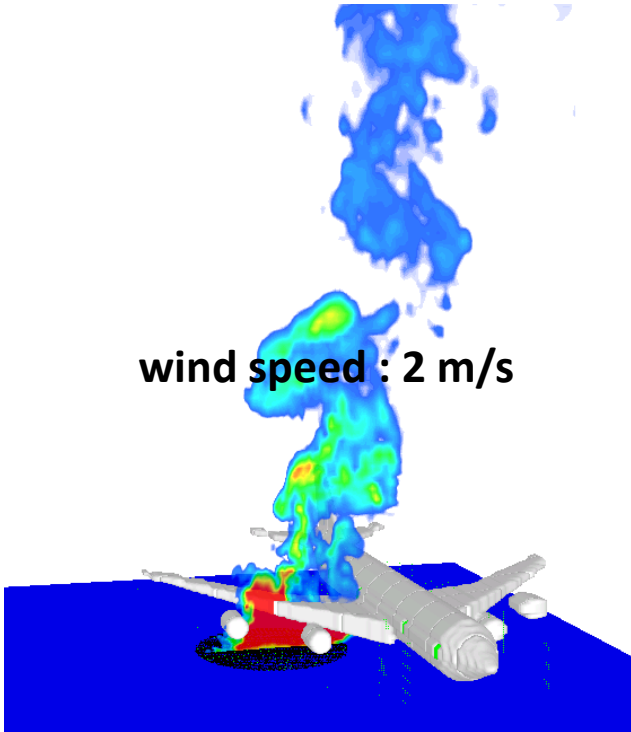


Smoke visualisation: from left to right the density of smoke increased at same light source parameters

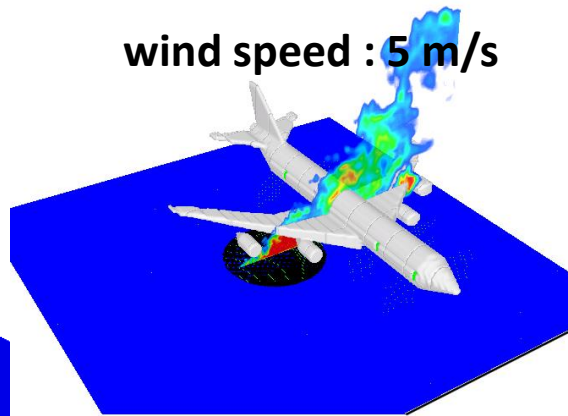
Temperature, flame spread rate, CO/soot over the composite fuselage

- ✓ Pool size from 10, 20, 30 to 40 m
- ✓ Fuel position : below one engine
- ✓ Burning rate of the liquid fuel : about 6 mm/min
- ✓ Heat release rate : higher than 800 MW
- ✓ Time to steady state : about 30 s

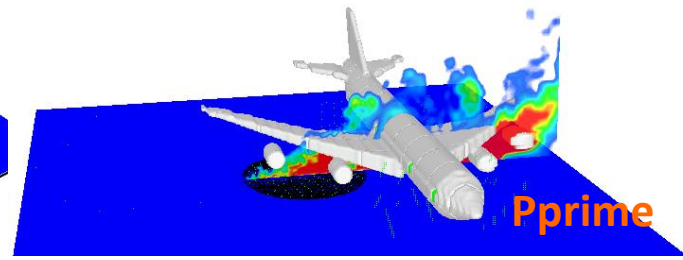
wind speed : 2 m/s



wind speed : 5 m/s



wind speed : 10 m/s



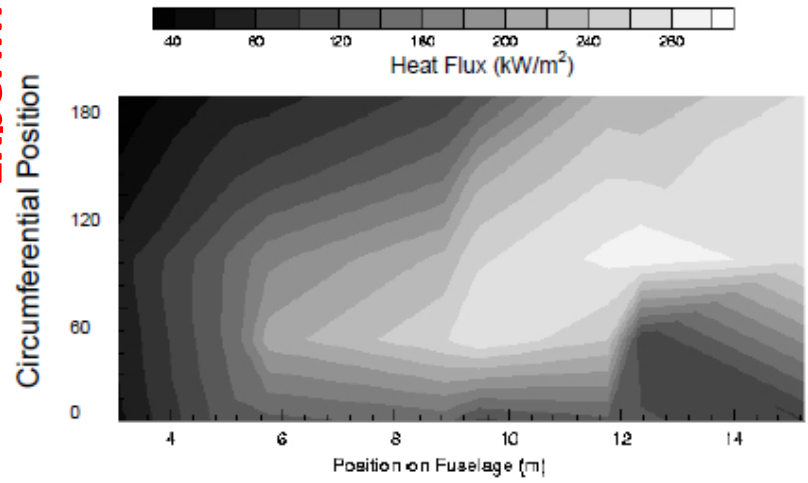
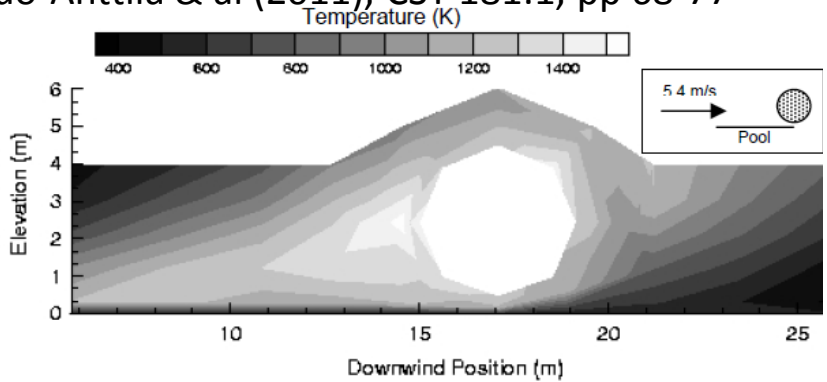
Temperature and heat flux on the fuselage surface

Experimental and Numerical fields

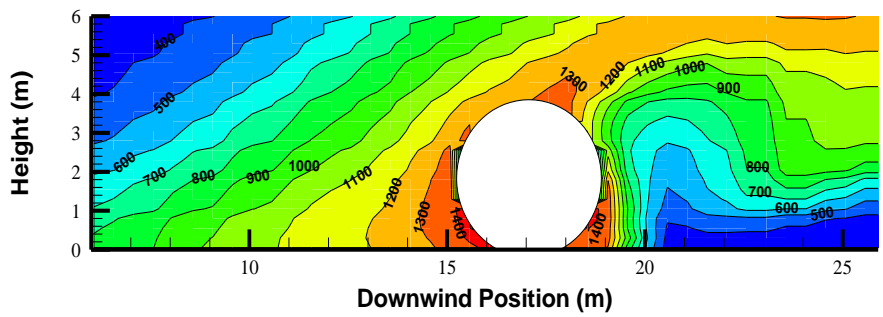
Wind - kerosene pool fire (D=19 m) engulfing a large cylinder object (d=3.7 m)

Suo-Anttila & al (2011), CST 181:1, pp 68-77

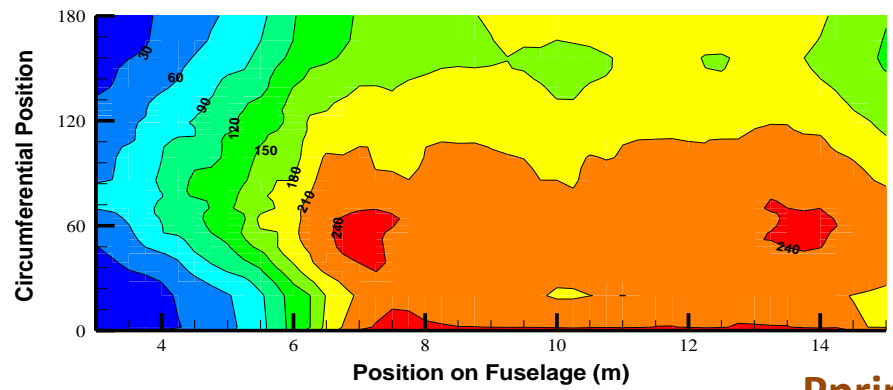
Experimental data



Temperature °C



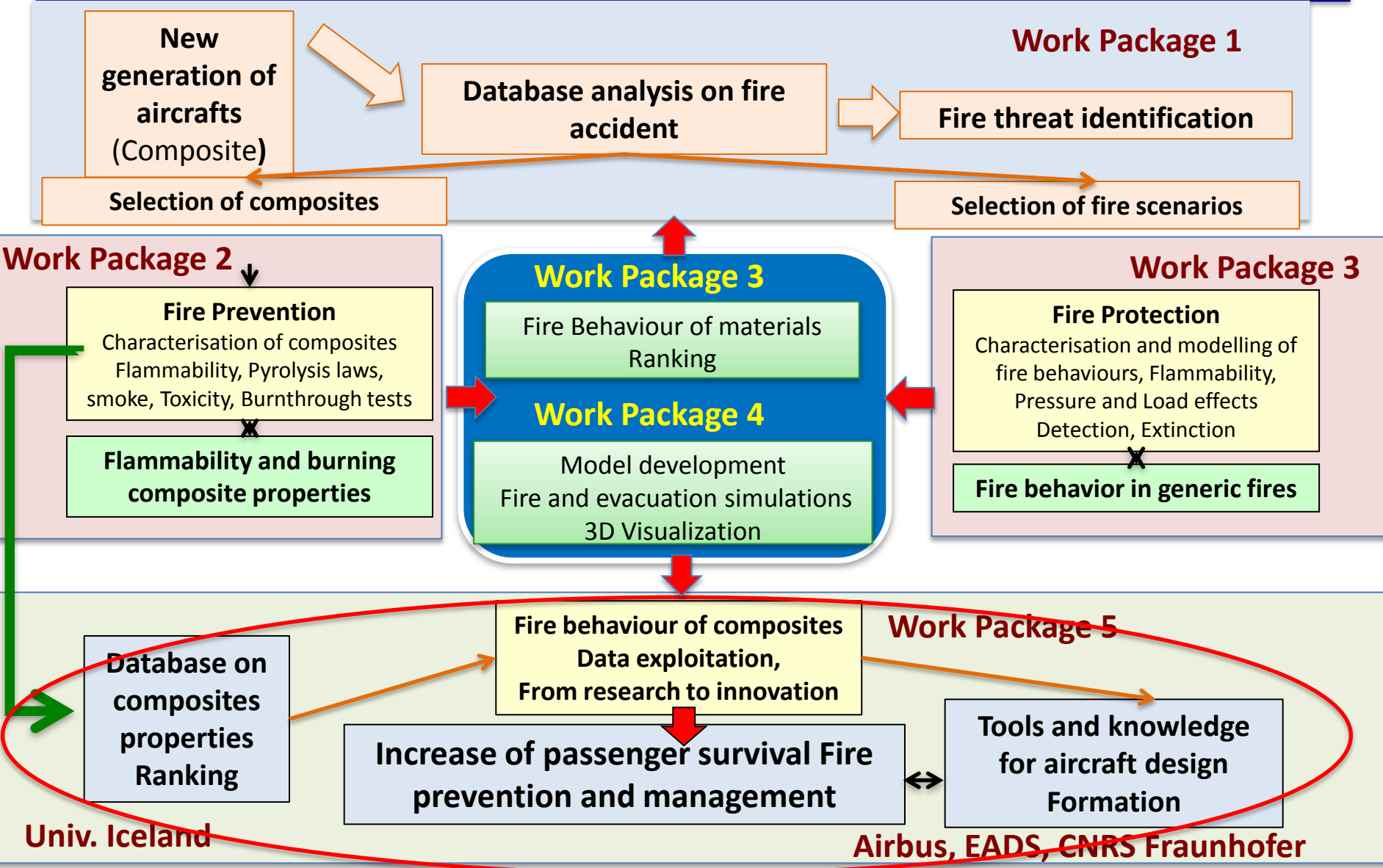
Heat Flux kW/m²



Modelling

Pprime

AircraftFire: CONCLUSIONS

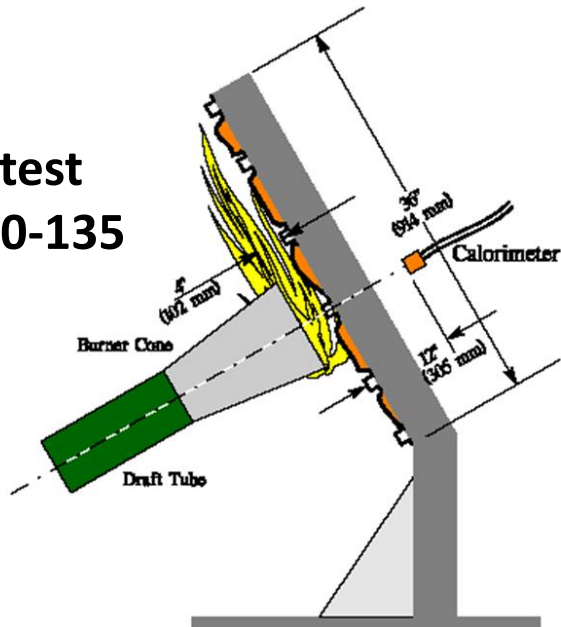


In-house Burnthrough test Facility

Pprime

The burnthrough test: → Time of burnthrough
Efficiency of the barrier to the flame

FAA test
AC 20-135



Flux 182kW/m² (fuselage, wing, structure)
Flux 106 kW/m² (engine)
Gas Temperature: 1100°C



Photos from FAA website

Material Characterization with In-house Burnthrough Test Facility

❖ Features:

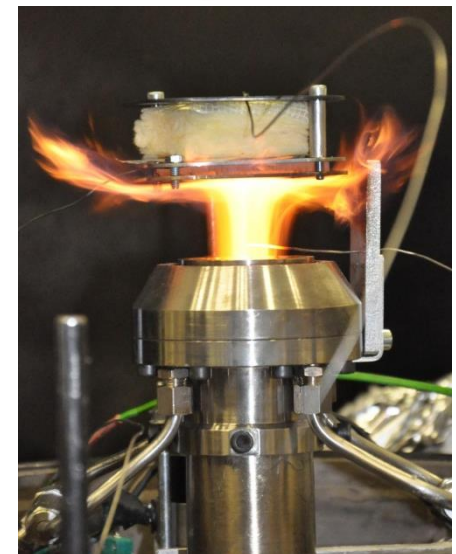
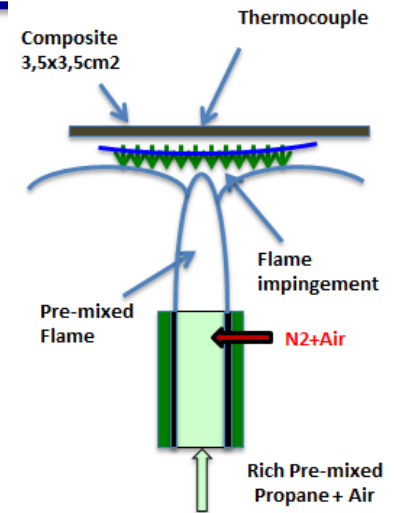
- Premixed burner
- Inside diameter injection D: 35 mm
- Burner / Sample distance 1.7, 3.5 and 5.2 cm
- Co-flow outside Nitrogen

❖ Parameter Setting:

- Burner exit temperature, T_{exit} : 830 to 1172 °C
- Output speed constant cold: $u_c = 2.3$ m/s; hot: 12m/s
- Turbulent flow $Re \cong 4700$
- Mass fraction of $y_{\text{O}_2} = 0$ to 0.06 at the burner exit
- Pressure 0.2 to 1 atm, load effects

❖ Diagnostics during tests:

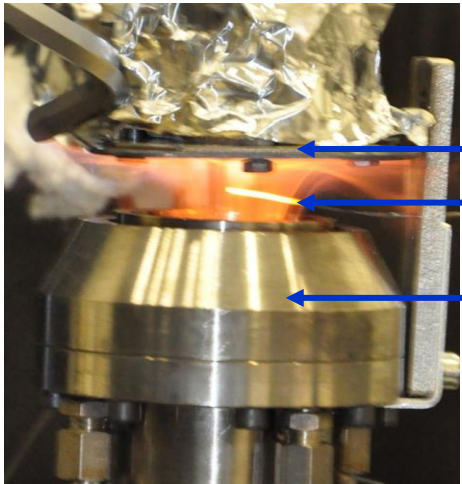
- Flowmeters for air, fuel gas, nitrogen
- Weight sensor → Mass loss → Mass Loss Rate MLR
- Thermocouples
- Video camera



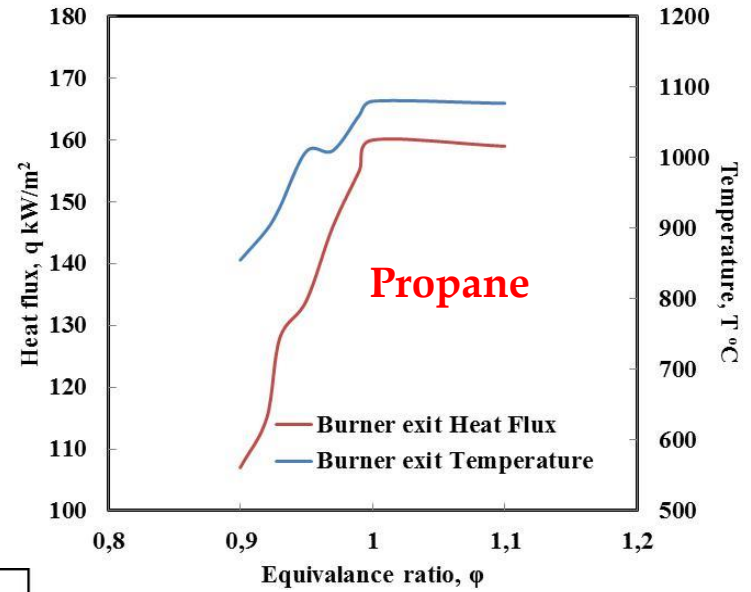
Schematic and snapshot of facility

Heat Flux calibration

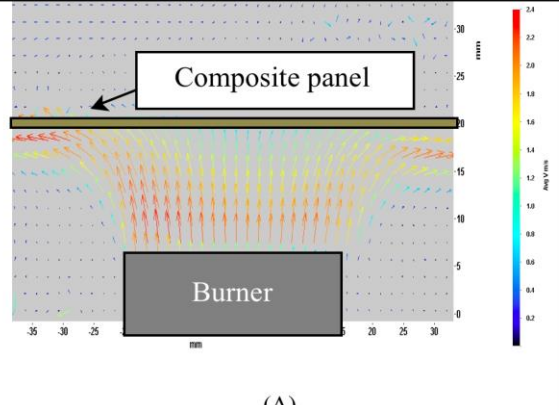
Radiometer – Tube calorimeter



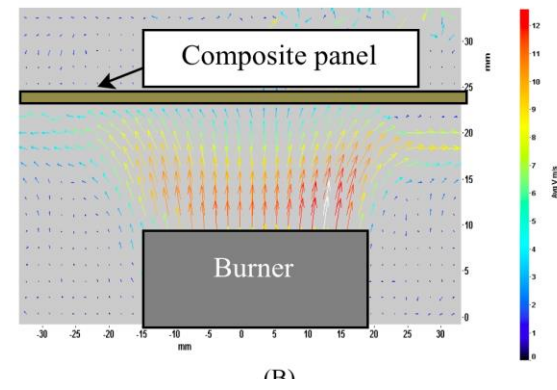
Radiometer
Thermocouple
Burner



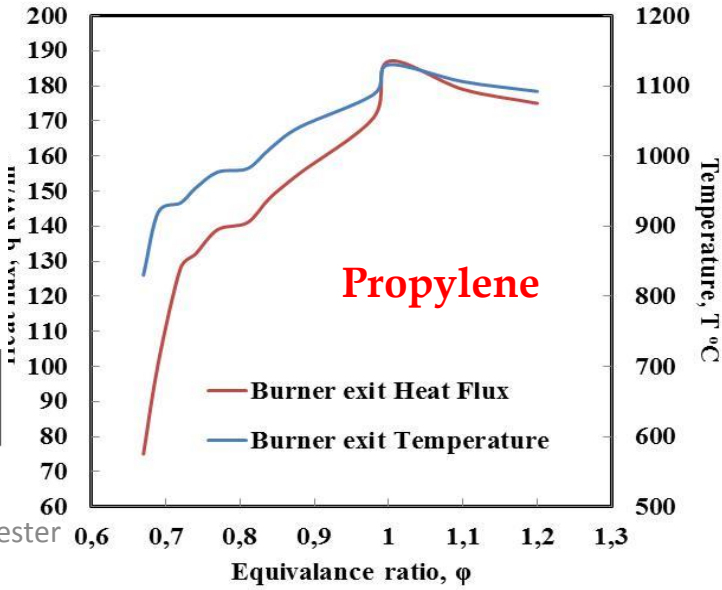
PIV



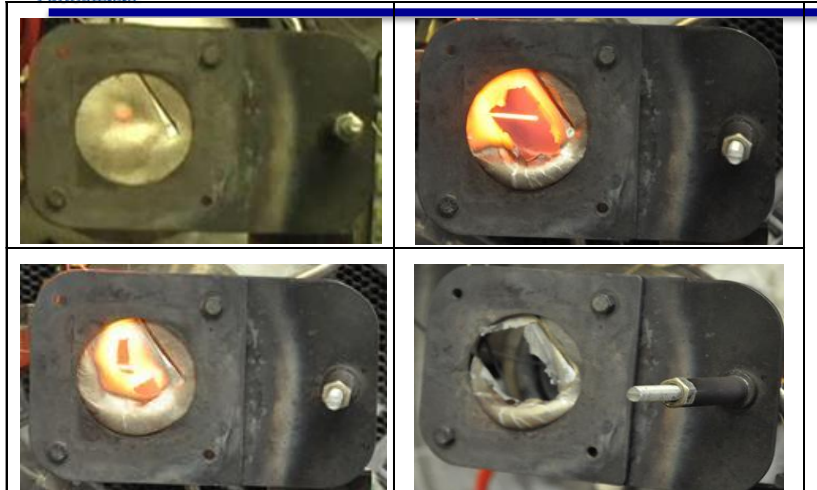
Cold Flow $u = 3$ m/s



Hot Flow $u = 12$ m/s

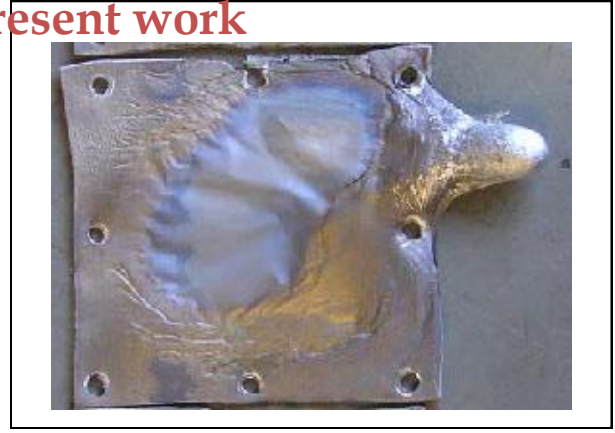


Aluminium (2mm thickness)

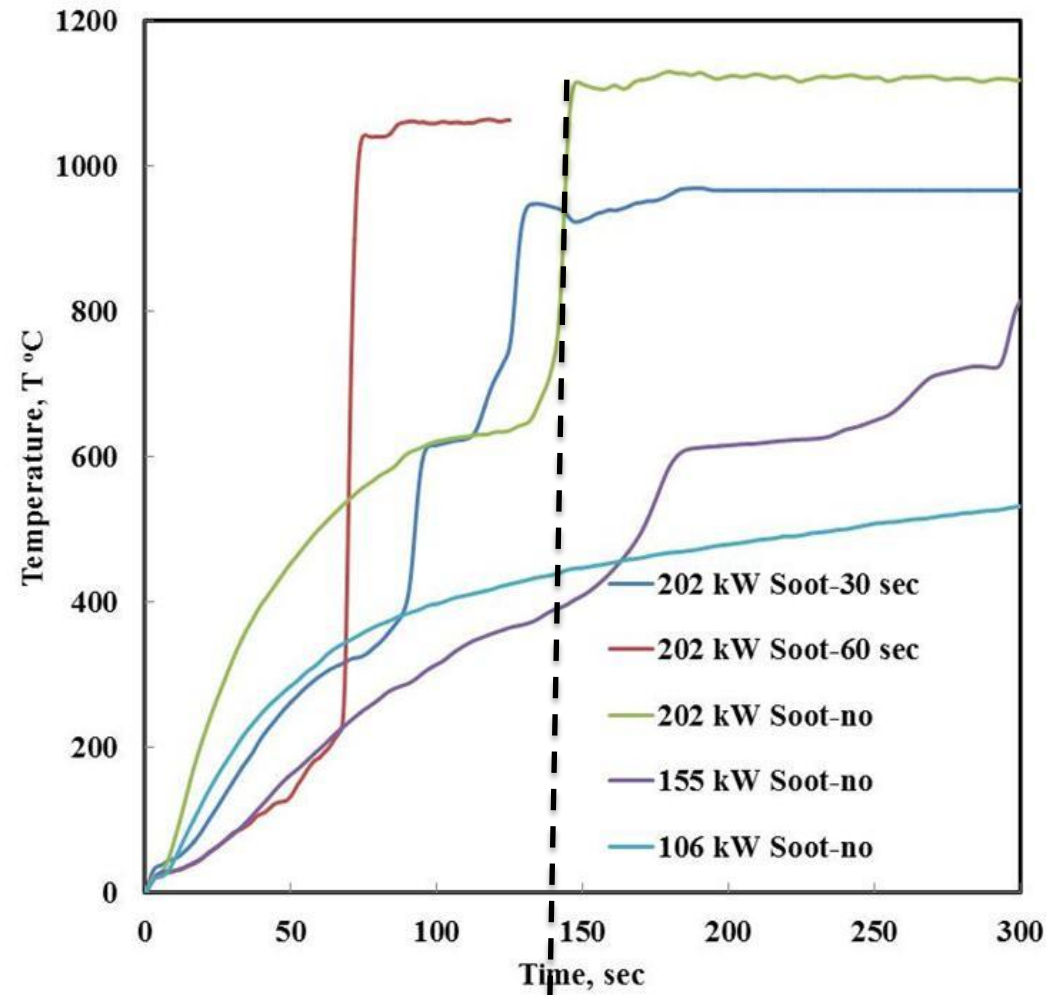


Aluminium Burnthrough Test:

Present work



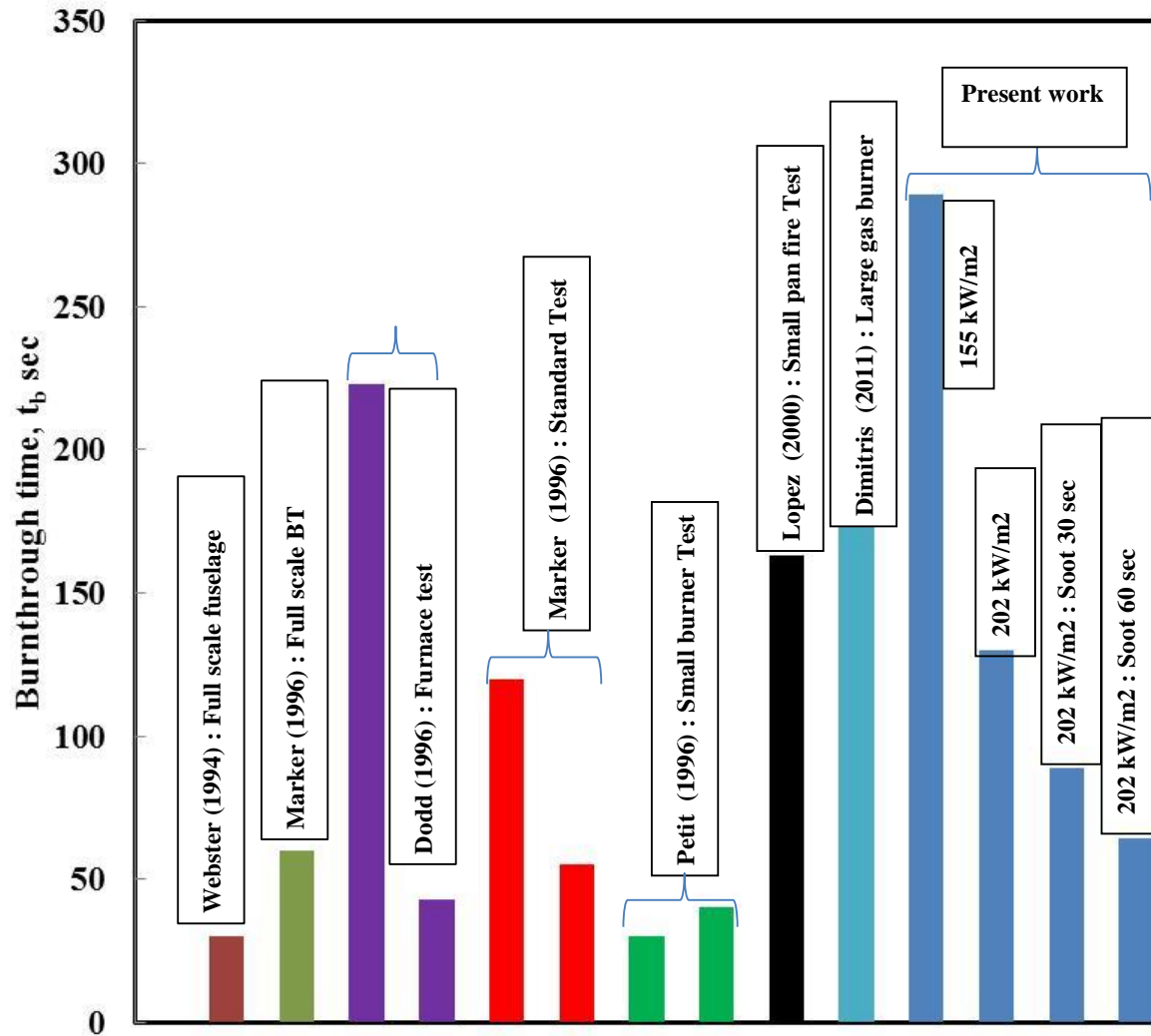
Aluminium Burnthrough Test:
Literature



BT= 140s

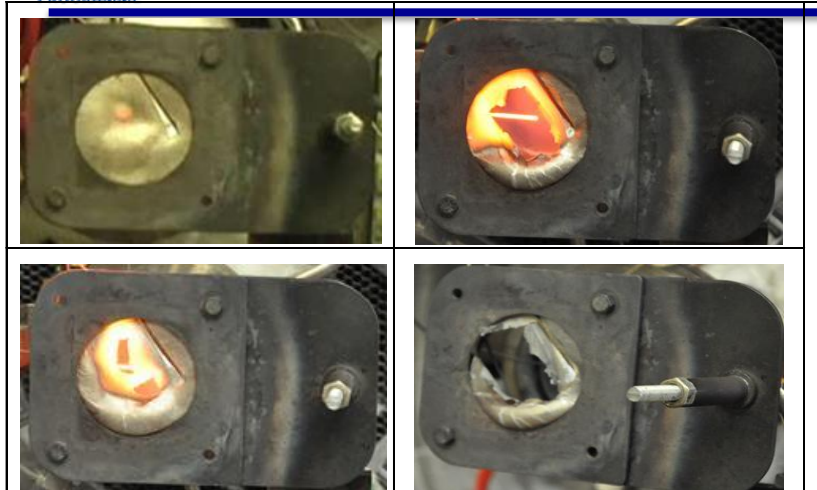
Aluminium: Burnthrough Data

Authors	Burnthrough time, t_b sec	Sample surface and Test No,	Device of tests
Webster, H (1994), FAA	30		Full scale fire test on aircraft fuselage
Marker (1996), FAA	60		Full scale burnthrough test
Dodd (1996), CAA	223	clean	Burnthrough furnace test
	43	sooted	
Marker (1996), FAA	120	1	Standard burnthrough test
	55	2	
Petit (1998), CEAT	30	1	Small burner burnthrough test
	40	2	
Lopez (2000)	163		Small scale pan fire
Dimitris et al. (2011)	173		Large In-house gas burner
Present work (Pprime)	289	1	Small In-house gas burner
	130	2	
	89	3	
	64	4	



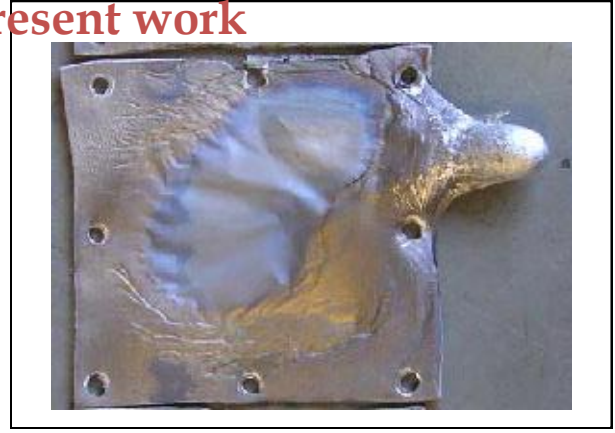
Complete burnthrough data for aluminium $b=2$ mm

Aluminium (2mm thickness)



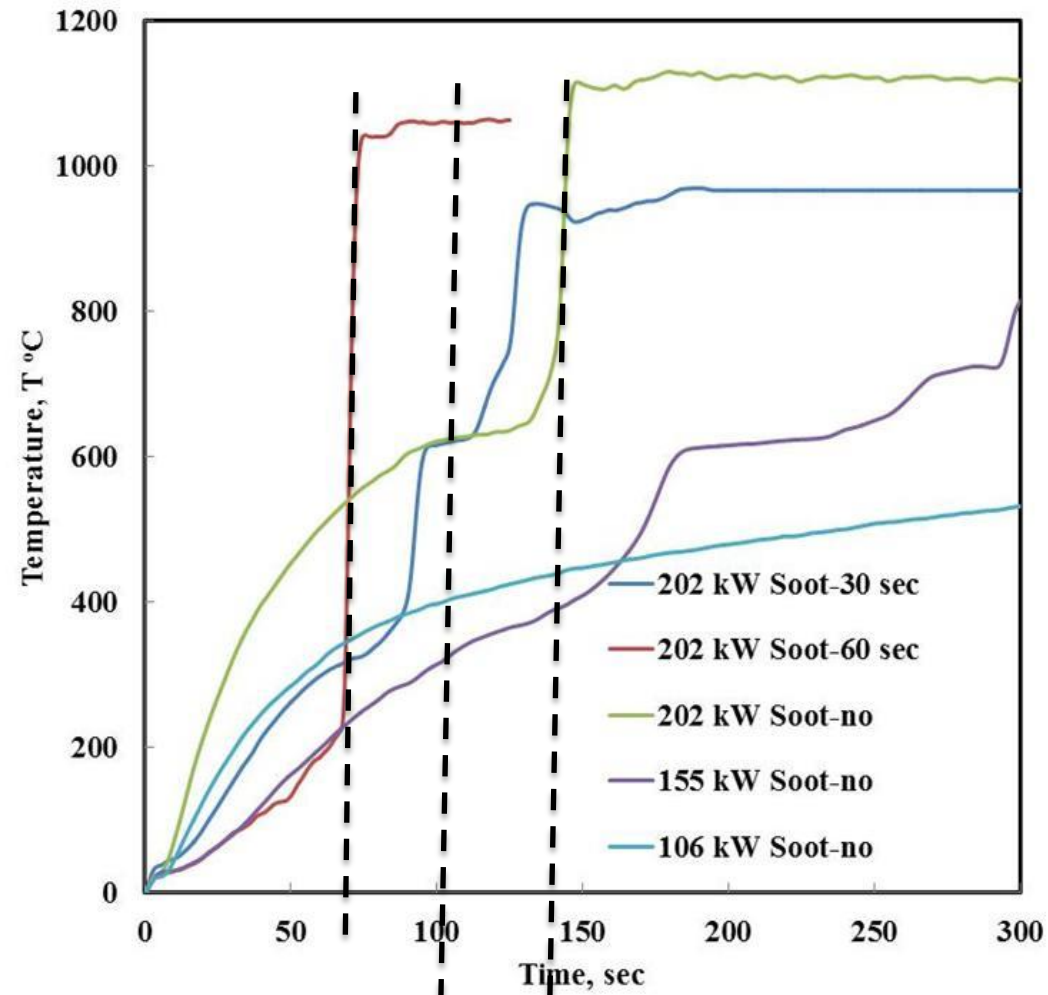
Aluminium Burnthrough Test:

Present work



Aluminium Burnthrough Test:
Literature

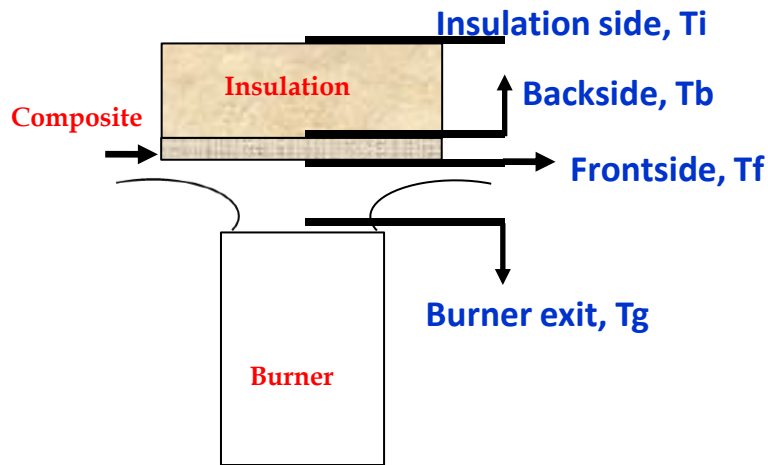
June 19-20th, 2013



Soot dep.(60s), BT = 64 s **BT= 140s**

Soot dep.(30s), BT = 100s

Burnthrough time for composite Material AcF2



Test conditions:

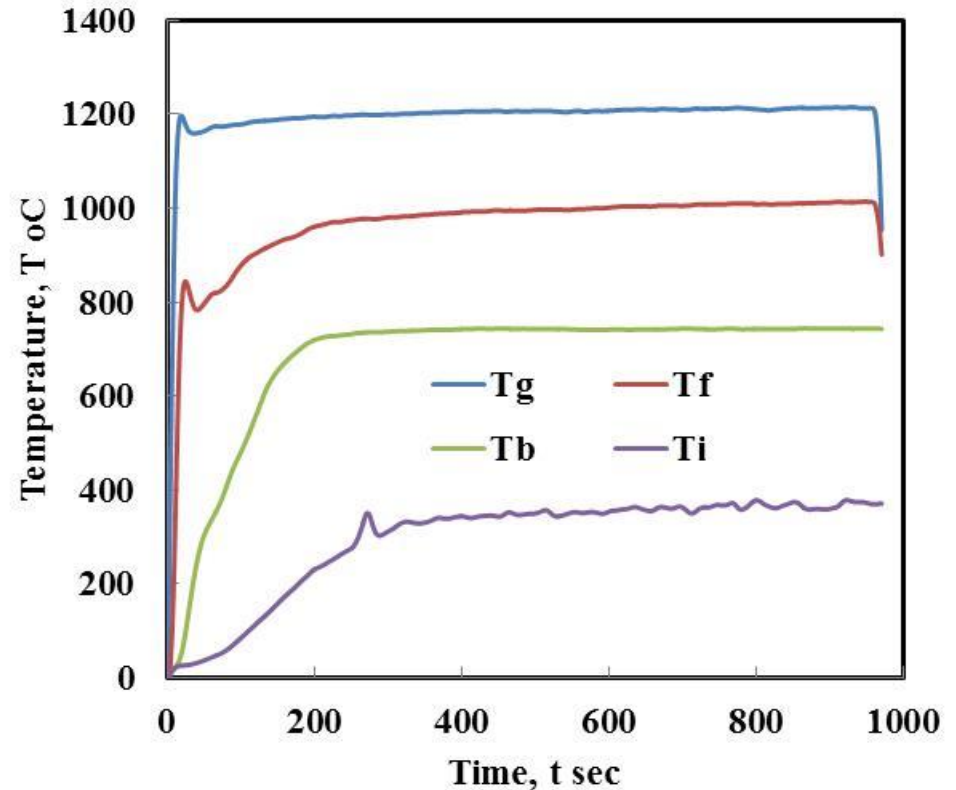
Total heat flux $q = 70$ to 202 kw/m^2

Strain rate, $\tau = 430 \text{ s}^{-1}$

$y_{O_2} = 0$ to 0.06

Sample thickness $b = 2 - 4 \text{ mm}$

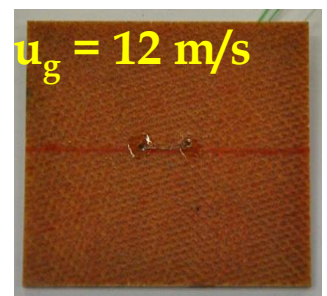
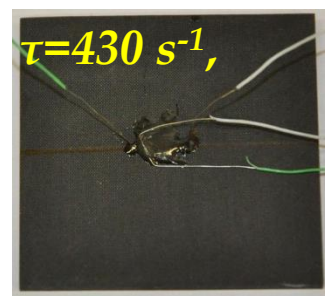
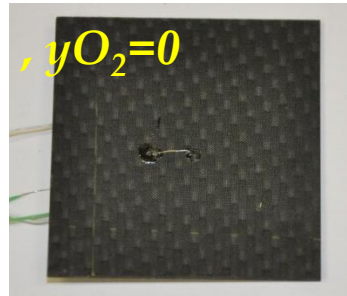
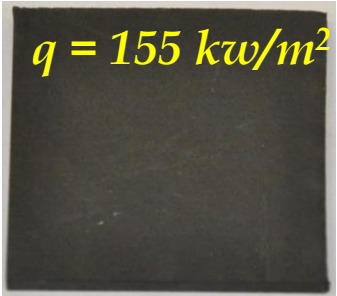
$u_g = 12 \text{ m/s}$



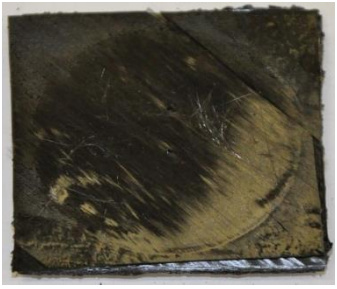
Burnthrough time > 17 minutes (1000 seconds)

No Burnthrough is observed

Composites : Material Swelling



Virgin sample



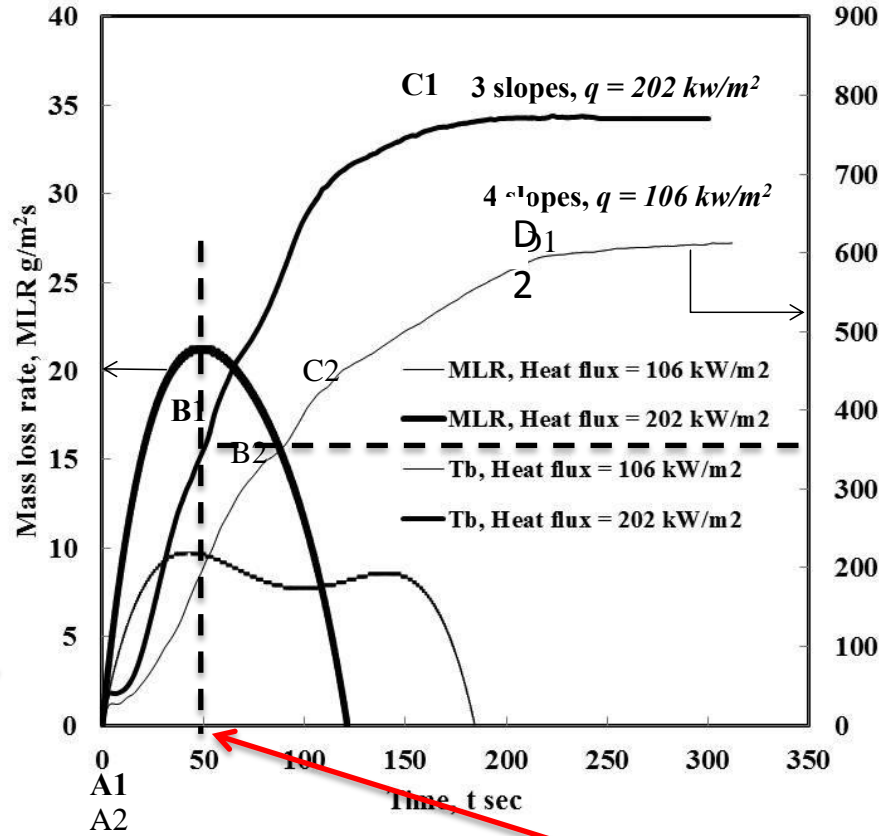
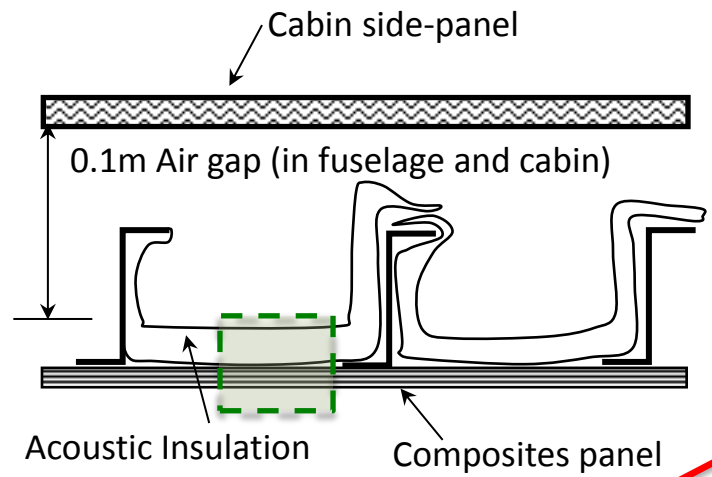
Sample swells expands

During resin vaporization, the resin escaped through closely spaced fibre (carbon or glass). This in turn produces internal pressure in the composites and therefore the sample swells i.e. the composite expands in response to internal pressure.

Temperature and Mass Loss Rate (AcF2)

Backside Temperature / MLR correlation

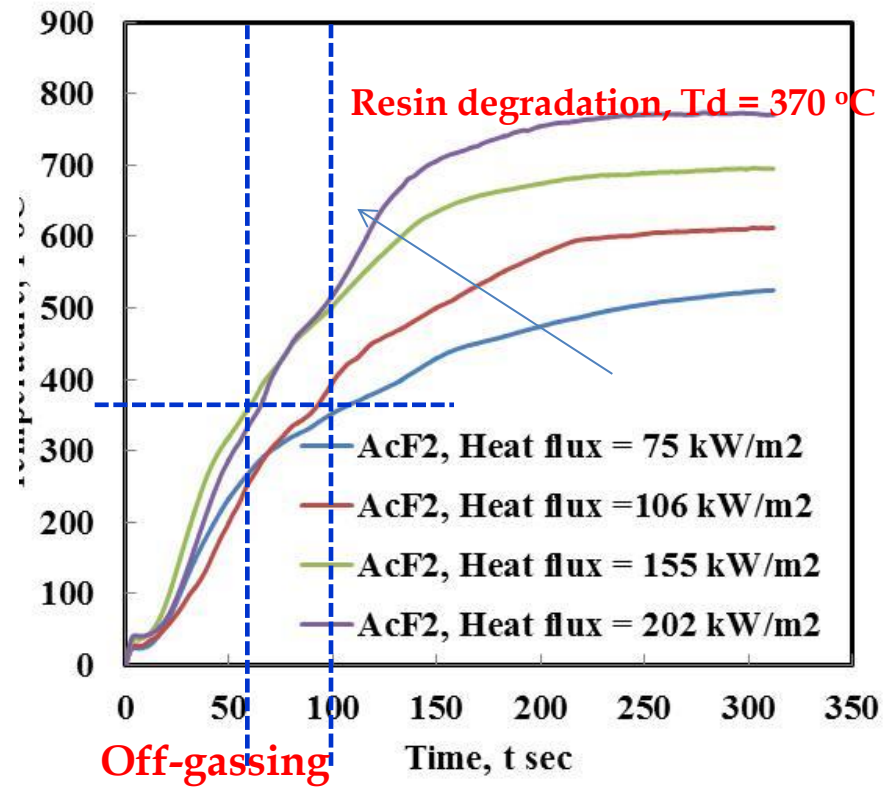
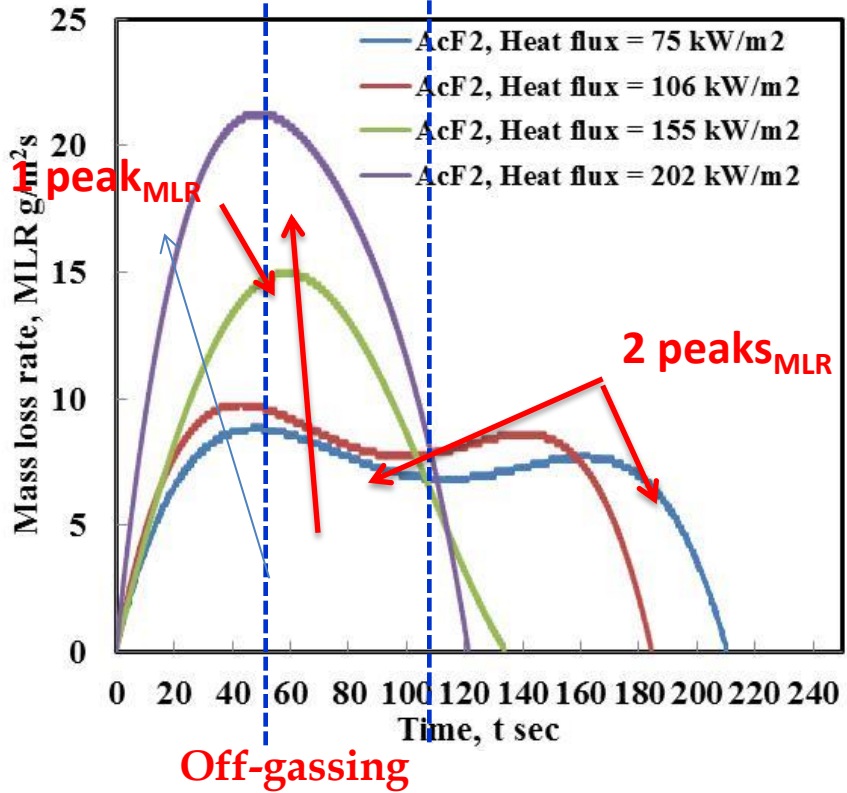
Test condition: Strain rate, $\tau=430 \text{ s}^{-1}$ and sample thickness $b=4 \text{ mm}$, $u_g=12 \text{ m/s}$



$A_i \rightarrow B_i$ Burning of resin – heat penetration
 B: Maximum of MLR (or HRR) $T_{\text{backside}} = T_{\text{degradation}}$
 C: End of resin burning

Off gassing : Toxicity and Potential ignition [Video](#)

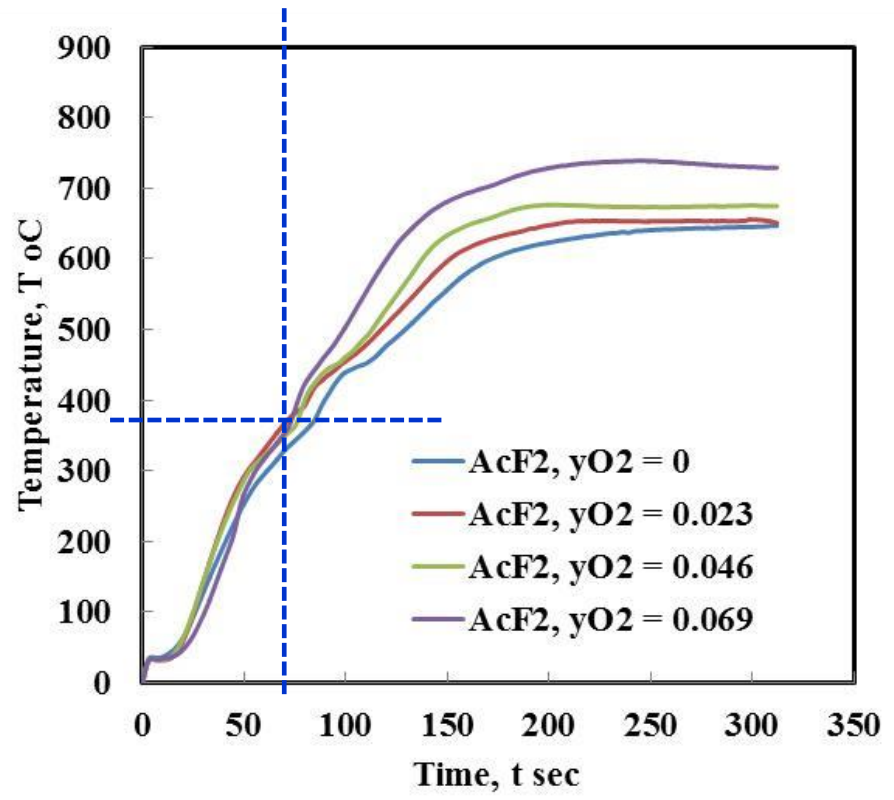
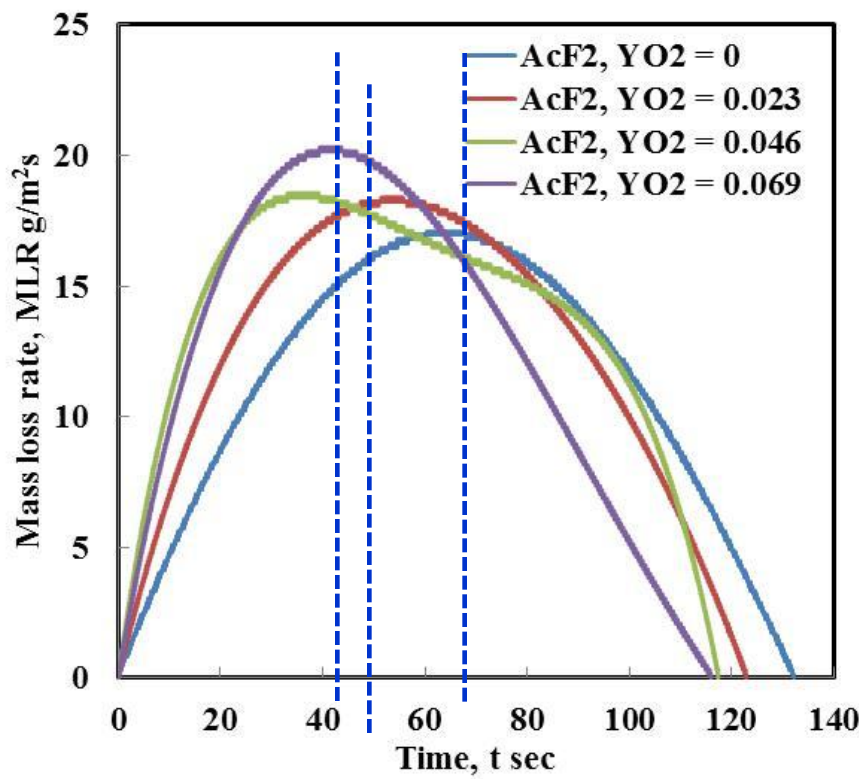
Mass Loss Rate - Temperature Material AcF2



$q \uparrow \Rightarrow \text{MLR} (V_{\text{comb}}) \uparrow \text{ and } T_{\text{backside}} \uparrow$

Higher heat flux => 1 peak_{MLR} : Formation and oxydation of char
Lower heat flux => 2 peaks_{MLR} : Combustion, formation of protective char layer, char oxydation, resin burning

Influence of Y_{O_2}

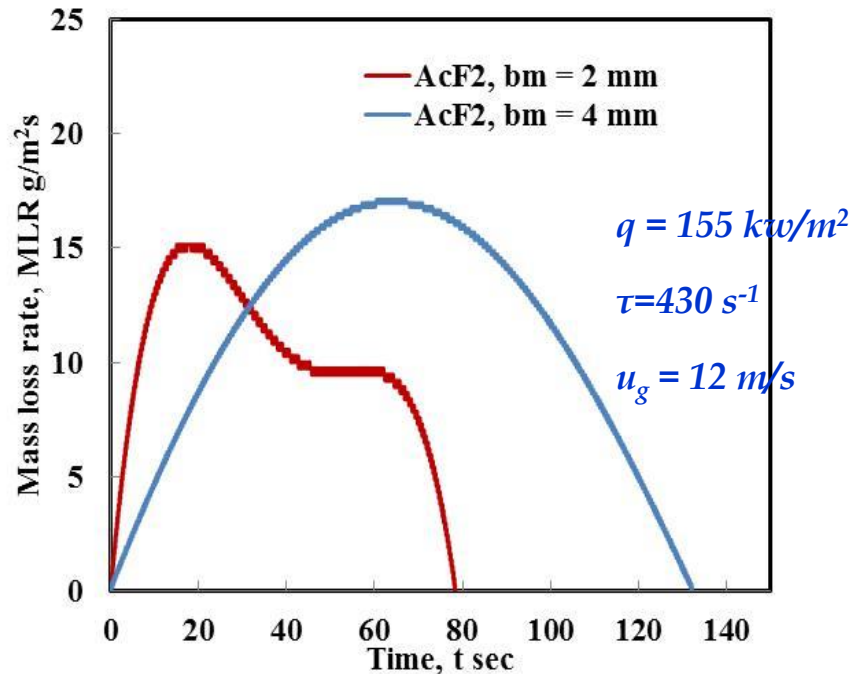


MLR
 $Y_{O_2} \uparrow \Rightarrow \text{MLR: } V_{\text{comb}} \uparrow \text{ and } T_{\text{backside}} \uparrow$

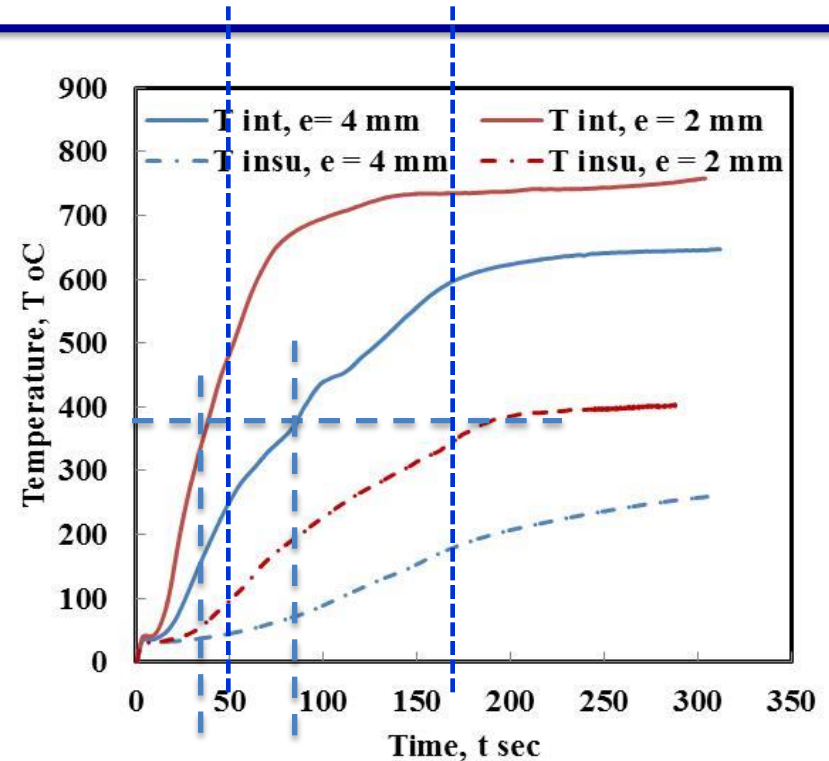
Backside Temperature

- Pyrolysis and burning of resin degradation products
- Maximum of MLR peak \uparrow with $Y_{O_2} \uparrow$
- Strong influence of O_2 due to high temperature reaction ($T=1100^{\circ}\text{C}$)

Influence of material Thickness b



MLR



Backside Temperature

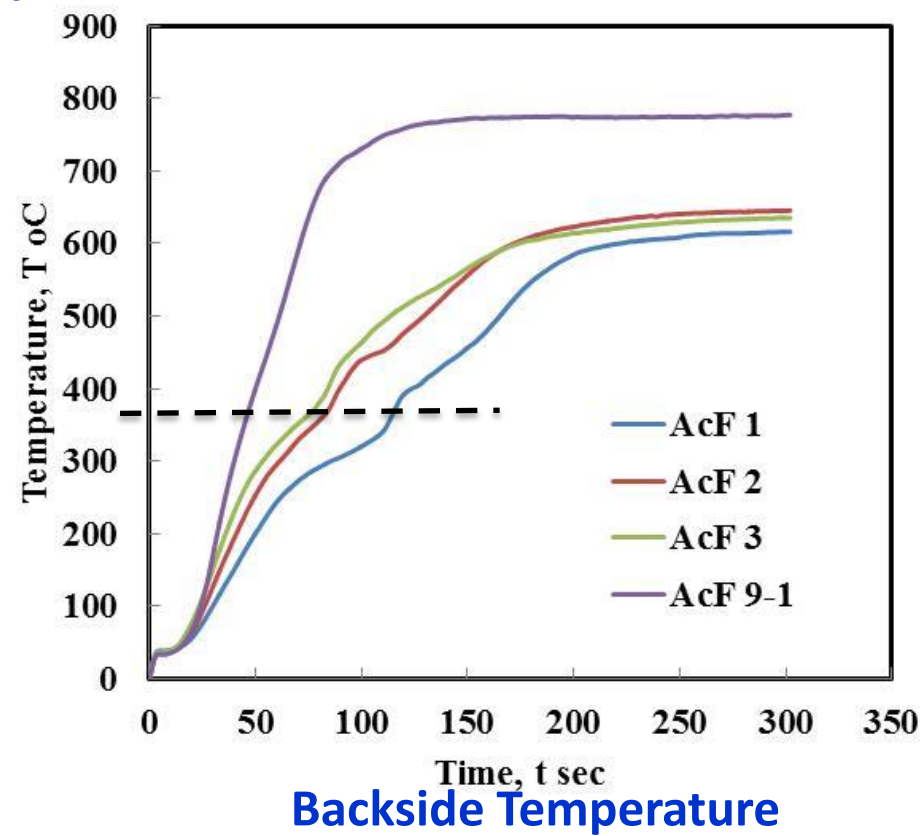
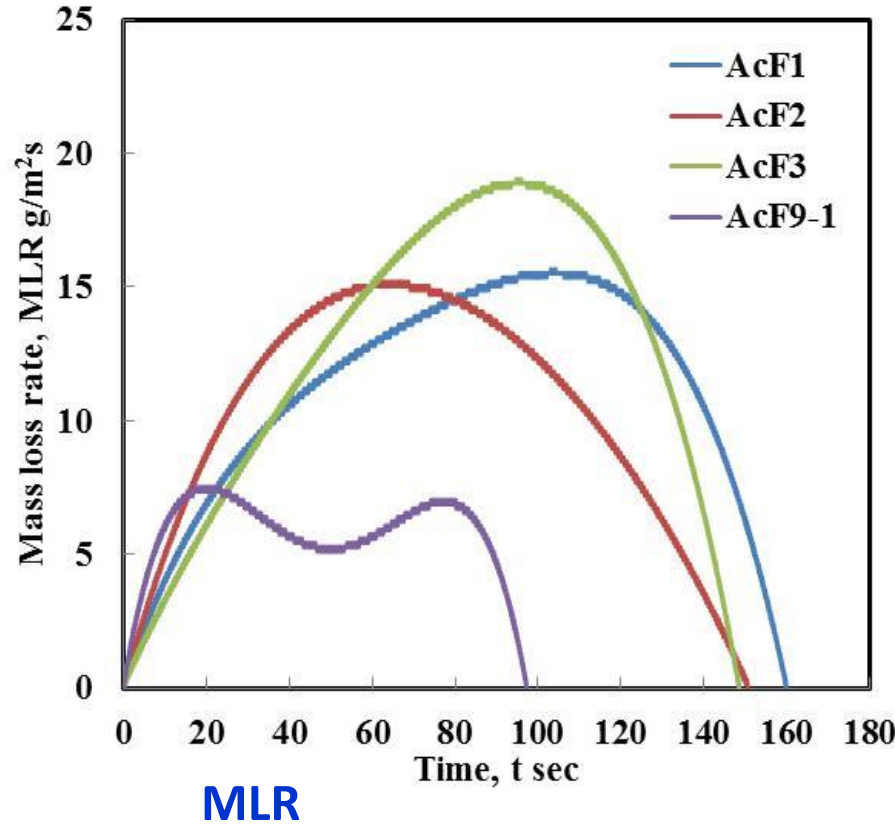
$b \uparrow \Rightarrow \text{MLR: } V_{comb} \approx \text{ and } T_{backside} \downarrow$

- ✓ $b=2\text{mm}$: 2 peaks_{MLR} (low heat flux) $e=4\text{mm}$: 1 peak_{MLR}
- ✓ $V_{comb, b=2\text{mm}} \approx V_{comb, b=4\text{mm}}$ (thermal effect)
- ✓ $b \uparrow \Rightarrow \text{Fire Resistance} \uparrow$
- ✓ $b=2\text{mm}$: insulation effect on backside with higher dT/dt

Comparison AcF1, AcF2, AcF3 (Epoxy/graphite fibers)

AcF9-1 (Phenolic/Glass fibers)

$q = 155 \text{ kW/m}^2, y_{O_2}=0.06 \quad \tau=430 \text{ s}^{-1}, u_g = 12 \text{ m/s}$



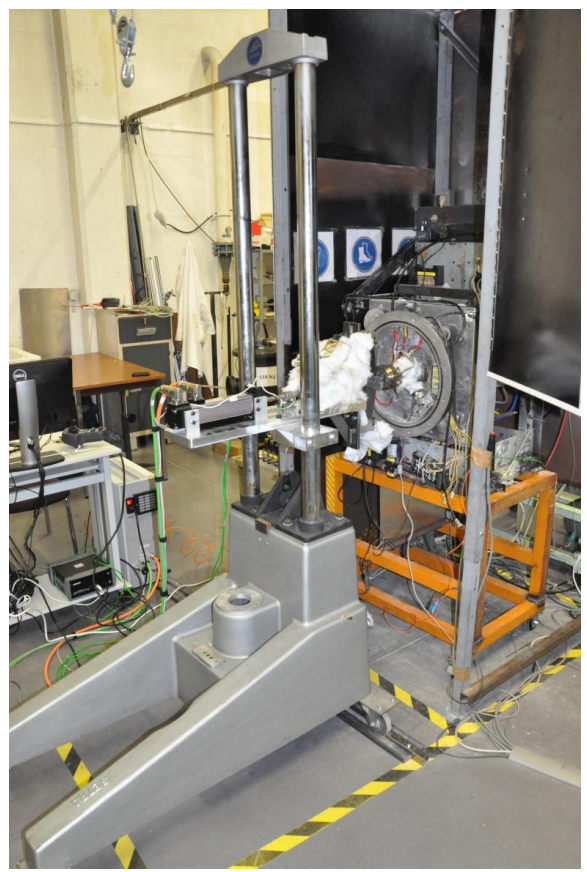
- ✓ $V_{\text{comb epoxy+FC}} > V_{\text{comb phenolic+FC}}$
- ✓ $T_{\text{int epoxy+FC}} < T_{\text{int phenolic+FC}}$ (thermal conductivity)
- ✓ Always char layer formation with phenolic resin

Degradation times and respective peaks of MLR

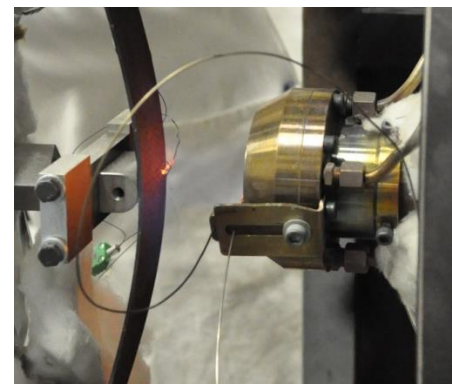
Sr. No.	Experimental Parameters variations	Aluminium		Composite	
		Burnthrough time (seconds)	Time for backside degradation (seconds)	Maxima of MLR (g/m ² s)	
1	Heat Flux, q (kW/m ²)	75	-	115	7.26
		106	infini	100	7.84
		155	175	60	16.96
		202 (no soot deposition)	130	46	21.12
		202 (soot deposition during 30s)	85	-	-
		202 (soot deposition during 30s)	64	-	-
2	Thickness b_m (m) (Heat Flux, $q = 202$ kW/m ²)	0.002		20	15.5
		0.004		60	16.96

Material burning under load

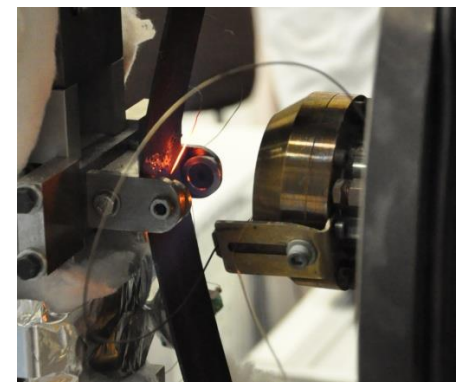
Experiment consists of exposing a sample of composite material to a flow of hot gases generated in the burner while applying a bending load



Experimental device

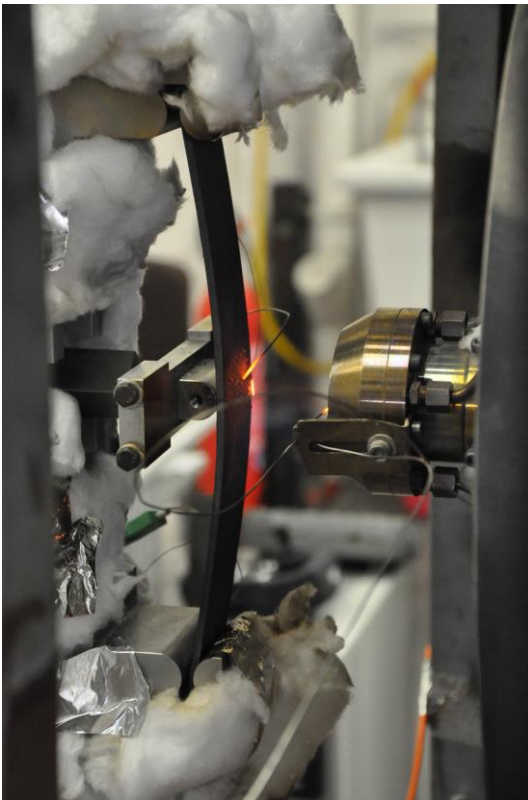


Contraint in fibers exposed to the flame: Tension stress

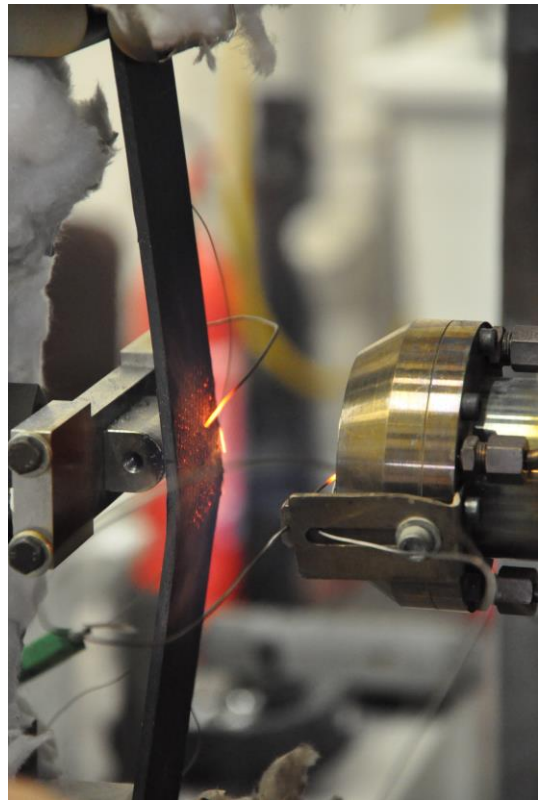


Contraint in fibers exposed to the flame: Compression stress

Material burning under load



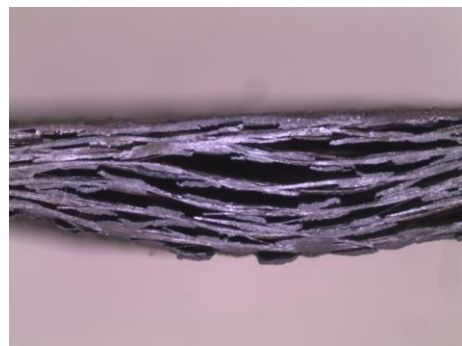
Before crack



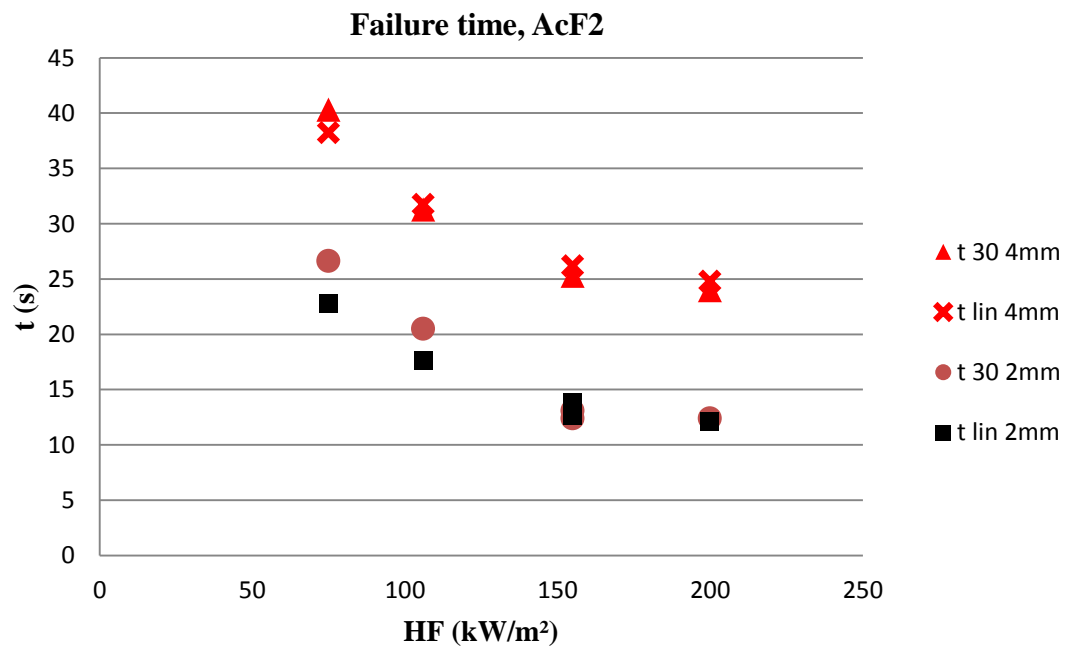
After crack

Material burning under load

Sample after testing

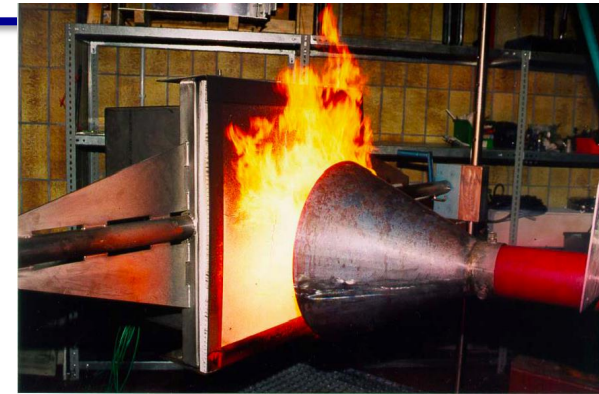


AcF2 Failure Time (HF)
 $b=2\text{mm}$ (Deflection 30mm)
 $b=4\text{mm}$ (Deflection 15mm)



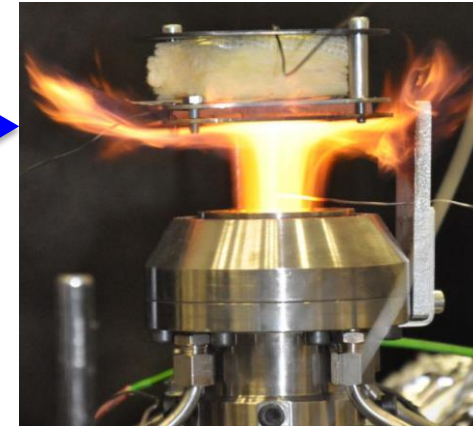
Burner – composite distance: 5.2cm

Burnthrough standard test burner



- **Parameters:**
 - Temperature and heat flux at the material location, imposed geometry
 - Type and Material thickness
- **Main Result:** burnthrough time (passed/failed tests)

Burnthrough AircraftFire burner



- **Parameters:**
 - Temperature and heat flux at the material location
 - Material thickness, Y_{O_2} , τ , Pressure, Load, etc.
- **Results:**
 - Burnthrough time!
 - Burning rate (combustion regimes (char), effects of additives)
 - Measurements of interface temperatures (heat flux inside the composite)

Fast and low cost tests for materials (composites)

➤ No burnthrough observed for composites in the studied conditions (up to 15minutes)

- Heat flux: 182kW/m² Gas Temperature: 1100°C

➤ Main results

- ✓ V_{combustion} mass loss of 24-30% in mass of the sample resin

Peak 1 of MLR

- Pyrolysis and combustion
 - End of resin combustion (less than 3 minutes)

✓ Peaks 2 of MLR

- Protective char formation
- Char combustion

➤ Fire propagation in the cabin consequences

◆ **Aluminium** : Time for Burnthrough

◆ **Composite**: Time for beginning of backside off gassing $T_{back} = T_{deg}$

➔ Potential diffusion of toxic gases in the cabin

➔ Ignition of fuel degradation products

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THANK YOU FOR YOUR ATTENTION