



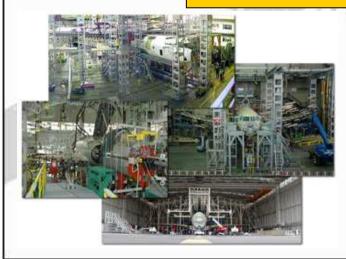
#### MINISTÈRE DE LA DÉFENSE



# **DGA Aeronautical Systems**

(ex. CEAT) « Fire Safety Department »

Fire Behaviour of Structural Composite Materials Submitted to a Hidden Fire Source





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# → Objectives of the works

# → Propane Hidden Fire Source

→ First test results & next works

## → Radiant Heat Source

→ First test results & next works

# → Underload Fire Behaviour

→ 4-point-bending test method







# → <u>Study's Aim</u>

→ To check the <u>ability of structural composite materials to keep their integrity</u> when they are submitted to a <u>hidden fire source</u>

AC 20-107 (Composite Aircraft Structure) :

- § 11.b : « ... The exposure of composite structures to high temperatures needs to extend beyond the direct flammability and fire protection issues to other thermal issues ... »

- → 3 different damaging sources will be used :
  - Propane fire source
  - Radiant heat source
  - Electric Arc source (test method to be define)

<u>Note</u> : The main goal of the study is more to assess the mechanical behaviour of the structural composite materials than to assess their flammability behaviour.

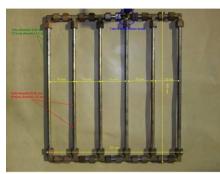


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PROPANE FIRE SOURCE



A propane fire source has been designed on the basis of the FAA foam block fire source characteristics, assuming that these characteristics are representative of a declared hidden fire :





> The Heat Flux Density & T° are similar to the flame characteristics produced by the FAA foam block

The Flame size is wider to produce an <u>homogeneous damaged area</u> compatible with the mechanical test specimens to be removed (area <u>~</u> 150 mm X 300 mm)



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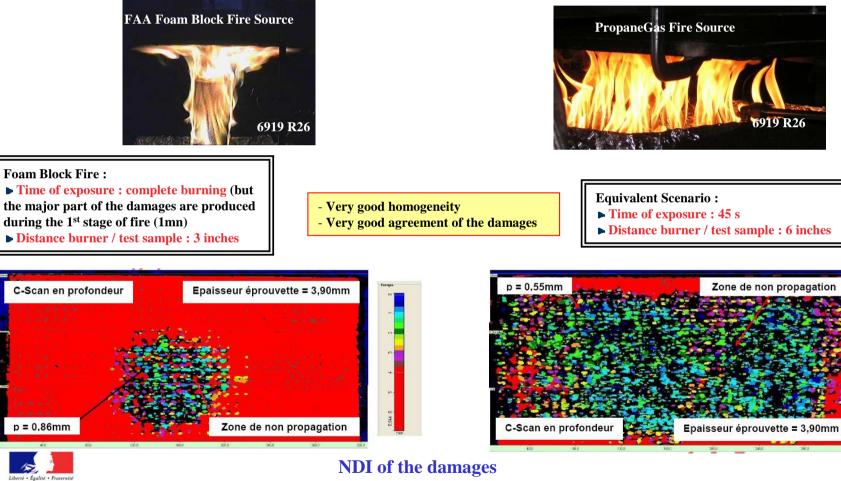
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### PROPANE FIRE SOURCE



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## PROPANE FIRE SOURCE

#### ▶ FIRE TESTS

**BASELINE TEST (representative of the foam block fire** scenario) :

- ► Time of exposure : 45 s
- Distance burner / test sample : 6 inches

#### Test on :

- T300 / 914 Carbon / Epoxy 16 plies / 2,4 mm  $\geq$
- T800H / DA508 Carbon / Epoxy 16 plies / 2,4 mm  $\geq$
- T800H / 5245 Carbon / Epoxy-Cyanate-Bismaleimid 16 plies / 3 mm  $\geq$
- Aluminium 2024  $\geq$

1,6 mm





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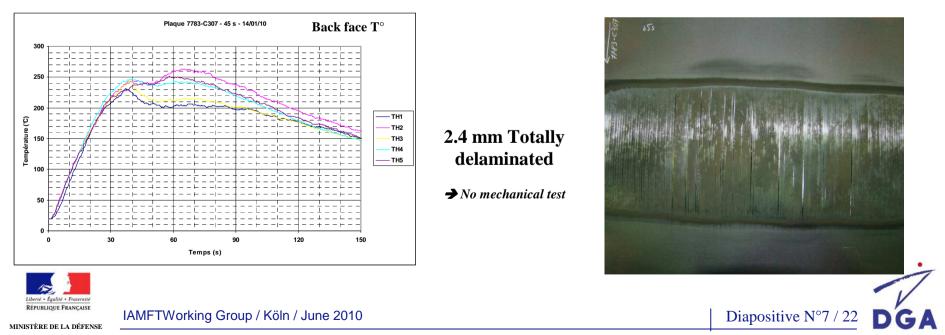


#### PROPANE FIRE SOURCE

▶ FIRE TESTS

BASELINE TEST (representative of the foam block fire scenario) :
Time of exposure : 45 s
Distance burner / test sample : 6 inches

#### > T300 / 914 Carbon / Epoxy 16 plies / 2.4 mm





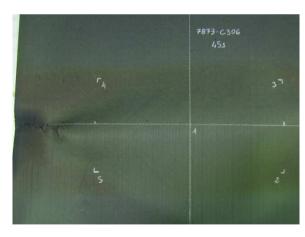


#### PROPANE FIRE SOURCE



BASELINE TEST (representative of the foam block fire scenario) :
Time of exposure : 45 s
Distance burner / test sample : 6 inches

#### > T800H / DA508 Carbon / Epoxy 16 plies / 2.4 mm



#### 2.4mm Totally delaminated

➔ No mechanical test





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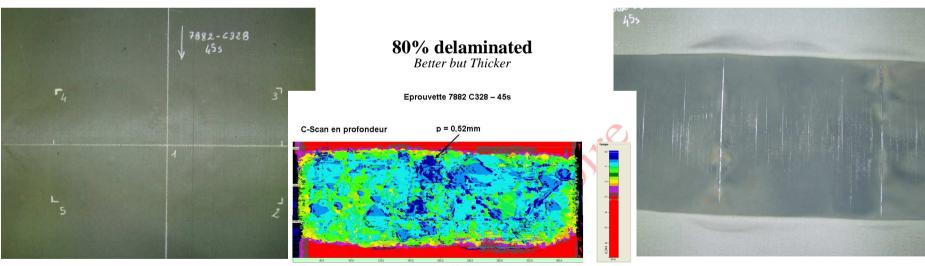


## PROPANE FIRE SOURCE

▶ FIRE TESTS

BASELINE TEST (representative of the foam block fire scenario) :
Time of exposure : 45 s
Distance burner / test sample : 6 inches

> T800H / 5245 Carbon / Epoxy-Cyanate-Bismaleimid 16 plies / 3 mm



Epaisseur éprouvette = 3,02mm



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### PROPANE FIRE SOURCE

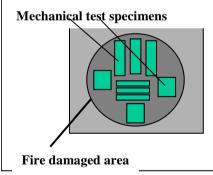
**FIRST TEST RESULTS** 

BASELINE TEST (representative of the foam block fire scenario) :
Time of exposure : 45 s
Distance burner / test sample : 6 inches

> The mechanical test results shown that :

Under the baseline test conditions (representative of the foam block fire scenario used for the ignition time on the intermediate scale hidden fire test):

 $\checkmark$  A 16 plies composite material representative to a fuse lage skin is at least 80% delaminated



T300 / 914 Carbon / Epoxy	2.4 mm (16 plies)	Totally delaminated
T800H / DA508 Carbon / Epoxy	2.4 mm (16 plies)	Totally delaminated
T800H / 5245 Epoxy-Cyanate- Bismaleimid	3 mm (16 plies)	80% delaminated

➔ These test conditions are too severe to make a study on the mechanical behaviour of the composite materials used for fuselage applications



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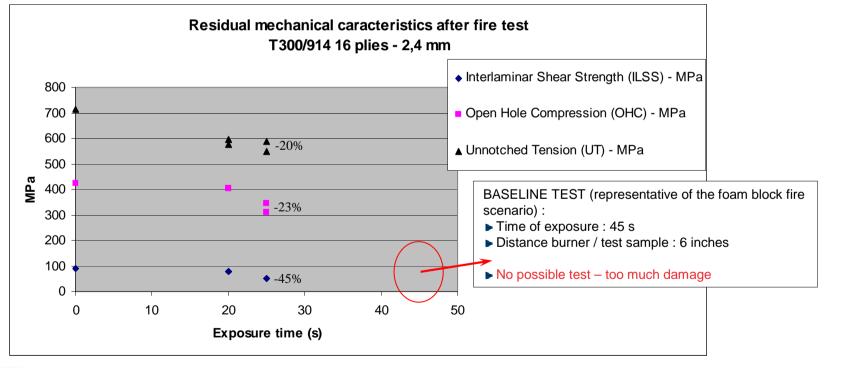
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#### ▶ PROPANE FIRE SOURCE

2 other scenarios were tested with a reduced time of exposure

**FIRST TEST RESULTS** 





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## PROPANE FIRE SOURCE

> The next step will be to determine less severe scenarios which will be able to discriminate and classify the composite materials :

✓ By reducing the gas flow-rate

✓ without reducing the baseline time of exposure which is already very short (45s)

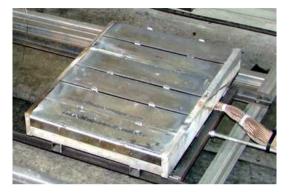








## **RADIANT HEAT SOURCE**



We have designed a damaging test rig using a radiant panel :



> The composite test sample is 10 cm above the horizontal radiant panel



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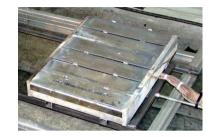
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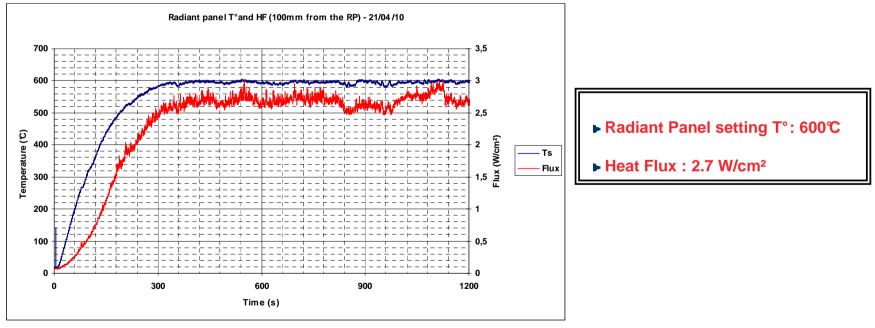




#### **RADIANT HEAT SOURCE**



#### Characterisation of the radiant heat source (d = 10 cm)





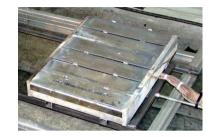
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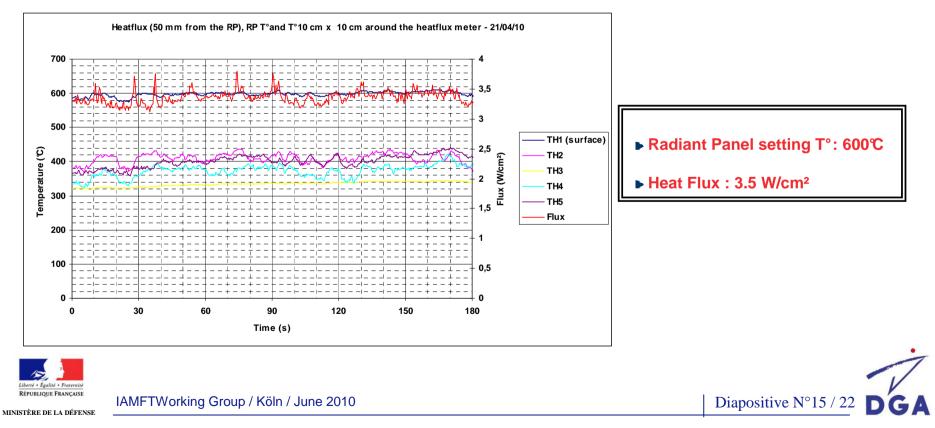




#### **RADIANT HEAT SOURCE**



#### Characterisation of the radiant heat source (d = 5 cm)



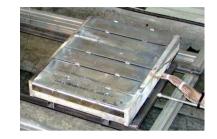




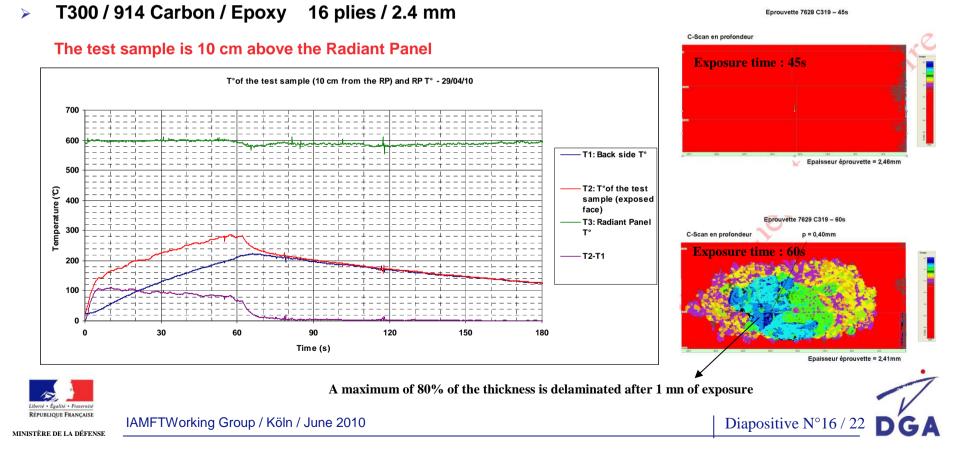
#### RADIANT HEAT SOURCE

 $\geq$ 

**FIRST TEST RESULTS** 



Eprouvette 7628 C319 - 45s







## **RADIANT HEAT SOURCE**

**FIRST TEST RESULTS** 

> The first test results show that :

Under exposure conditions (1mn under 2.7 W/cm<sup>2</sup>) less severe than the conditions used for the Radiant Panel Test for electrical wiring (1mn under <u>~</u>3 W/cm<sup>2</sup>):

✓ A 16 plies composite material representative of a fuselage skin is 80% delaminated

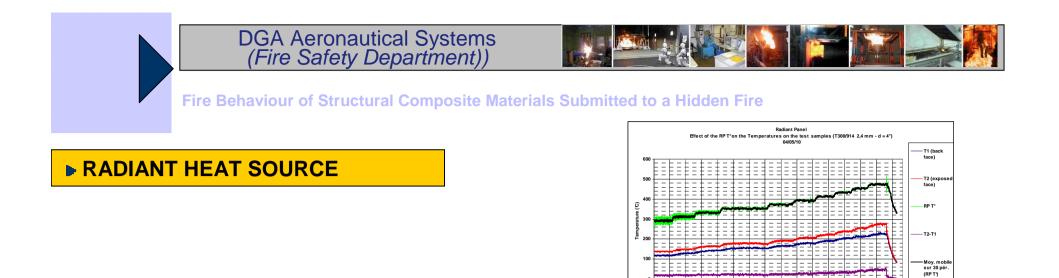
→ These test conditions are too severe to make a study on the mechanical behaviour of the composite materials used for fuselage applications



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The next step was to find the setting T<sup>o</sup> of the radi ant panel which generates surface  $\geq$ temperatures of the composite material close to the resin glass transition T°(190 / 200°C):

We found that:

 $\checkmark$  380°C / 3mn generates a T° of ~ 200°C on the exposed face (170°C on the opposite face) (no visible damages by NDI)

 $\checkmark$  460°C / 2mn generates a T° of ~ 255°C on the exposed face (200°C on the opposite face) (beginning of the damages visible by NDI)

→ We have now to determine the best scenarios of exposure around these settings to compare the residual mechanical properties of various composite materials



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Time (s



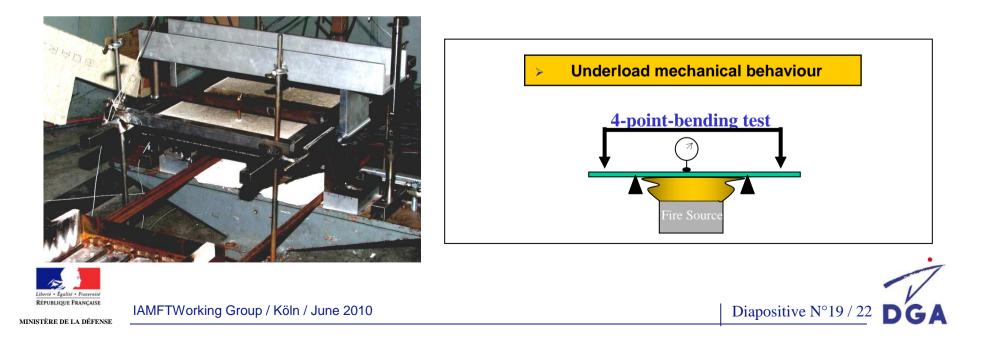




## UNDERLOAD FIRE BEHAVIOUR

To assess the mechanical behaviour of composite materials during the exposition to a hidden fire :

- We designed a 4-point-bending test rig
- Using the gas fire source or the radiant source
- The load (100 MPa) is representative of the fuselage in-flight stress
- The test sample is 6 inches above the heat source
- Continuous recording of the bending displacement measured at the centre of the test sample







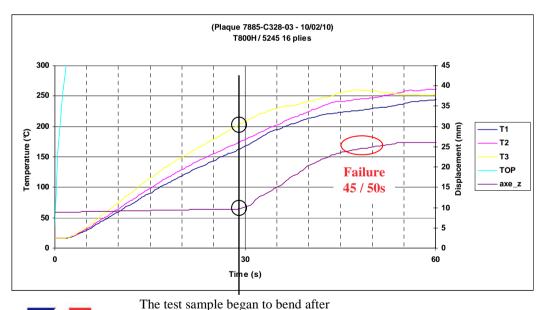
## UNDERLOAD FIRE BEHAVIOUR

**FIRST TEST RESULTS** 

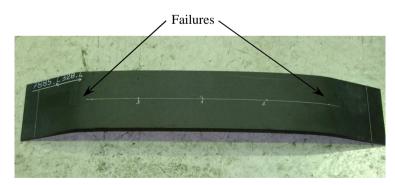


Thermocouples on the back side

> T300 / 914 Carbon / Epoxy 16 plies / 2.4 mm







Test sample after test

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DG



29s at 200°C max (close to the Glass Transition T°) IAMFTWorking Group / Köln / June 2010





## CONCLUSIONS

We have designed

> a propane fire source representative of the FAA foam block fire source used for the ignition of the intermediate scale fire test

> a radiant heat source to assess the behaviour of materials submitted to a heat source without flame

> a 4-point-bending test rig to assess the underload behaviour of materials submitted to a thermal threat with or without flame





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## CONCLUSIONS

We thought that the hidden fire source or the heat source used to test the cabin materials would have been a good source for the assessment of the fire and mechanical behaviour of composite materials for fuselage.

> We are surprised that these fire sources are too severe, leading to a delamination of (at least) 80% of the thickness (16 plies of carbon-epoxy, 2.4mm, representative of a fuselage skin).

If a fire would propagate with the same characteristics, all the exposed parts of the composite fuselage would lose most of their mechanical properties within less than 1 minute?

> Are they realistic scenarios for the assessment of the flammability behaviour (propagation) but not realistic for the assessment of the mechanical behaviour?

> Or are they only intended to be representative of a local ignition source but not intended to be representative of a realistic larger in-flight fire?





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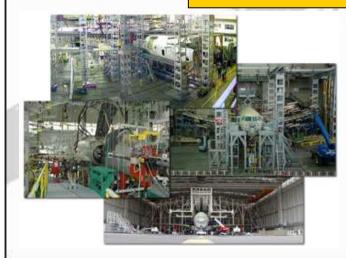


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