# Development of In-Flight Flammability Test for Composite Fuselage Aircraft

Presented to: International Aircraft Materials Fire Test Working Group – Köln, Germany

By: Robert Ian Ochs

Date: Wednesday, June 17, 2009



Federal Aviation Administration

# Outline

- Introduction
- Objective
- Test Plan
- Radiant Heat Transfer
- Summary



# Introduction

- Modern commercial aircraft are being designed with increased amounts of composite materials in the aircraft fuselage and structures
- Composite resins can have a very wide range of flammability
- Traditional aircraft fuselage and structures are constructed from aluminum, which does not react when exposed to a hidden fire source in flight
- It must be proven that if an aircraft is to be constructed of non-traditional materials, the materials chosen must provide at least an equivalent level of safety to aluminum
- Intermediate scale tests have been used to date to show equivalency, but a lab scale test with well defined criteria is necessary for future certification purposes



# Objective

- Develop a lab-scale test to determine the propensity of a non-traditional fuselage material to propagate a flame or to sustain flaming combustion
- Test criteria is to be based upon intermediate scale testing
  - Standard fire source used to simulate a hidden fire
    - 4" x 4" x 9" untreated urethane foam block
    - 10cc of heptane soaked into foam to provide more uniform burning
  - Various materials of similar mass and rigidity will be tested, both aircraft grade and non-aircraft



# **Materials to Test**

### Fiber-reinforced polymer composites

- Carbon-epoxy
  - Unidirectional and woven carbon fiber layups
  - Variations of resin systems
    - From most flammable to least flammable
    - Create a sample set of materials with a particularly flammable resin system
    - Dope some samples with various amount of flame retardants
      - Brominated epoxies to effect gas phase (high smoke/low char)
      - Phosphorous compounds to effect condensed phase (low smoke/high char)
    - Flammability "should" directly link to percentage of flame retardant compounds mixed in the resin system
- Sandwich panels
  - Structural plies bonded to honeycomb cores



% additives





**Structural Plies** 



### Test Configuration Intermediate Scale

- Panel Construction
  - 18" x 48", varying thicknesses 1/8" and up
  - Solid laminates
  - Thin laminates (<10 plies) sandwiching honeycomb core
- Panel at 45° angle to foam block
- Flat panels only, no curvature
- No structural members
- Fire source untreated urethane foam block, 4" x 4" x 9"



**Composite Fuselage Flame Propagation** June 17, 2009 – Köln, Germany

Federal Aviation

Administration



**Composite Fuselage Flame Propagation** June 17, 2009 – Köln, Germany





### Intermediate Scale





# Test Configuration Lab Scale

- Use identical materials from intermediate scale
  - Sample size 12" x 24"
- Use radiant panel apparatus for lab scale testing
  - Develop test parameters based on intermediate scale results
    - Calibration heat flux
    - Pre-heat
    - Flame impingement time



# **Radiant Heat Transfer**



- Emissivity, thermal conductivity of sample materials will dictate surface temperature
- Surface temperature directly relates to the volatilization of material components and therefore the flammability of the material
- For a standard incident radiant heat flux, different materials will attain varying surface temperatures
- A preheat time should be determined that can bring most materials to a particular surface temperature range



### Sample



1.5" —



11





**Composite Fuselage Flame Propagation** June 17, 2009 – Köln, Germany





- Heater calibrated to
  2.2 BTU/ft<sup>2</sup>s
- Sample exposed for 15 min
- Sample allowed to cool for 15 min





Back T/C Temperatures 1.5" x 1.5" x .125" Samples, 2.2 BTU/ft<sup>2</sup>s Heat Flux





14

### **Painted Composite Samples – Before**



Three composite samples, 1/8" thick, 1.5" x 1.5", painted with high temp spray paint

Thermocouple on front surface (shielded from radiant heat) and on center of back surface

Kaowool insulation around and behind the sample



### After



Silver sample exhibited no delamination or smoking

Gray and White samples exhibited smoking, delamintation, and swelling

### Front and Back Surface Temperatures **Silver Composite** 1000 Front ٠ Rear **Onset of Vaporization** 800 Temperature, °F 600 400 200 0 10 15 0 5 20 25 30 Time, min

**Composite Fuselage Flame Propagation** June 17, 2009 – Köln, Germany



### Front and Back Surface Temperatures White Composite 1000 Front ٠ Rear **Onset of Vaporization** 800 Temperature, °F 600 400 200 0 10 15 0 5 20 25 30 Time, min

#### **Composite Fuselage Flame Propagation** June 17, 2009 – Köln, Germany



#### Front and Back Surface Temperatures Gray Composite



**Composite Fuselage Flame Propagation** June 17, 2009 – Köln, Germany



19

#### **Front Surface Temperatures**



June 17, 2009 – Köln, Germany

Federal Aviation Administration

#### **Rear Surface Temperatures**



June 17, 2009 – Köln, Germany

# **Observations**

- Surface color determines the amount of radiant heat absorbed by material
- Shiny surfaces reflect more radiant heat than darker surfaces
- For this carbon/epoxy material exposed to a radiant heat flux, the surface color determines the amount of time it takes for the surface temperature to reach the onset of vaporization
- Determine if this has an effect on flame propagation in both intermediate scale and lab scale



# Summary

- Intermediate scale testing will begin with non-aircraft materials
  - Plywood
  - Acrylic
  - Honeycomb panels
  - Fiberglass
- Custom formulated composites will be ordered
- Effect of surface color on flame propagation will be studied



# Composites Task Group – Thursday A.M.

- Discuss approach to intermediate scale flame propagation
- Materials
- Lab scale test parameters



Contact: Robert Ochs DOT/FAA Tech Center BLDG 287 Atlantic City Int'l Airport NJ 08405 <u>robert.ochs@faa.gov</u> 1 (609) 485 4651



