A STUDY INTO FLAME INGRESSION AND FLAME ARRESTOR PERFORMANCE USING A POWERPLANT STANDARD CALIBRATED FLAME

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Premise

- There is no available data in the public domain regarding flame ingression and the performance of flame arrestors
- Starting point of this project for Resonate Testing, we recognize improvements can be made to the set up and running of tests – cooling airflow
- Provide data and results to determine if the industry recognized convention, that a straight tube with a length 10 times its diameter (10 L/D) acts as a flame arrestor
- To investigate how much flame ingresses through different size hole/slits/tubes when subject to a powerplant standard calibrated flame, under ambient conditions and pressure differentials
- Investigate how different configurations may affect flame ingression e.g: if the flame is directly impinging or scrubbing
- Consider how far above the flame ingression do the conditions exceed safe temperature limit for fuel

Whilst we are sharing this project, we cannot assume liability, as it is indicative R&D only. We will not be sharing instrumentation used. Data and results cannot be used for commercial gain or validation/certification purposes.







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Dynamic Rig









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New Rig Design

Horizontal box



Vertical box

Burner can be orientated vertically or horizontally

Burner moves in fromright to left and stopsunder each box

Design allowed the box to be lifted off the plate – investigate 'no box' scenario







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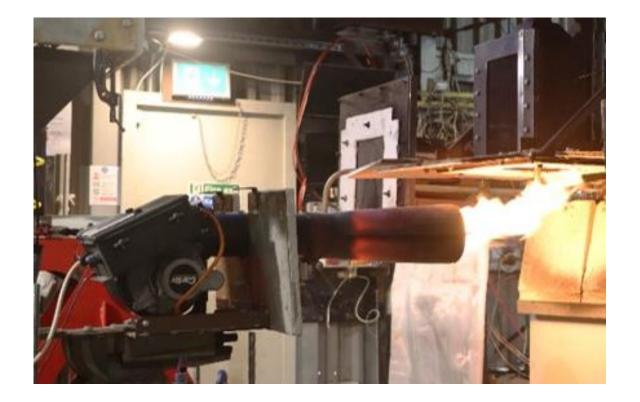
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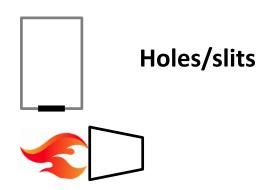
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Configurations

Buoyancy















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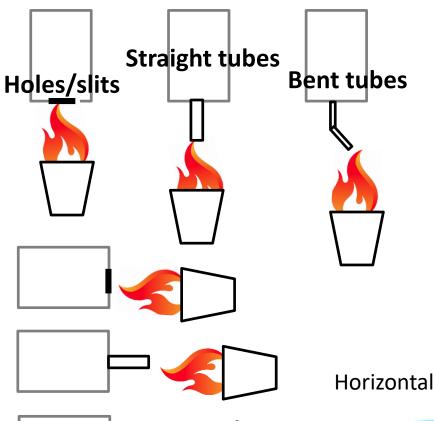
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Configurations

Direct Impingement

Vertical











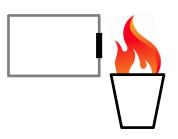
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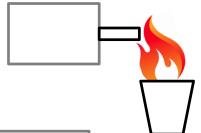
Configurations

Scrubbing









Straight tubes



Bent tubes





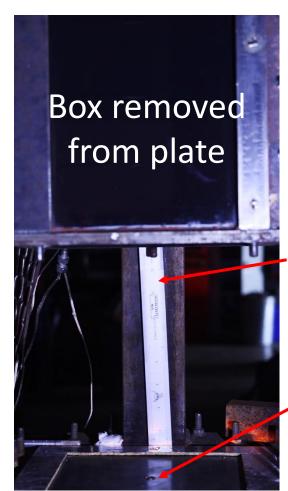


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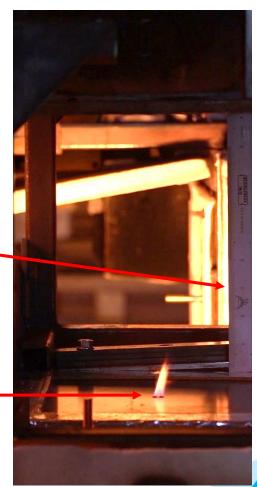
Configurations



'No box'

Rule to measure flame ingression

Plate with hole/slit









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Hole/Slit/Tubes Tested

Holes, Ø in / mm	Slits, width in / mm	Straight tubes	Bent tubes/Tortuous paths
0.2" / 5mm	0.08" / 2mm	-6 5L/D	-6 20L/D 45°
0.6" / 15mm	0.2" / 6mm	-6 10L/D	-6 20L/D 90°
1" / 25mm	0.4" / 10mm	-6 15L/D	-12 10L/D 45°
		-6 20L/D	-12 20L/D 90°
		-12 5L/D	
		-12 10L/D	
		-12 15L/D	
		-12 20L/D	

-6 = 3/8" tube

-12 = 3/4" tube

L/D is defined as the ratio of the length of tube to the diameter

Note: dimensions are approximate





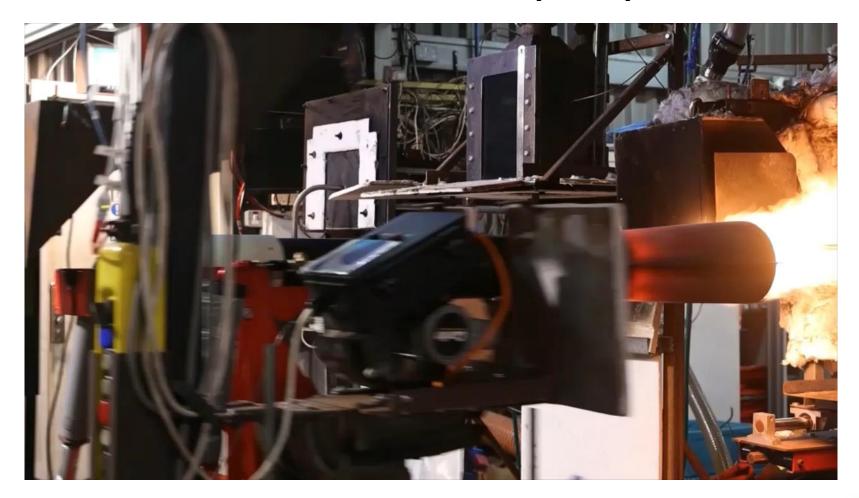


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Burner Transition video - -12 (3/4") 20L/D 90°









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Variables considered within the body of testing

Test Setup/Rig Overview	Flame Arrestor	Flame Ingression	Buoyancy/Direct Impingement/Scrubbing
Carlin vs Sonic	Straight Tubes	L/D ratios	Tortuous Paths
Hole and Slit Size	Pressure Differentials	Ambient Conditions	Larger Volume Setups
Flame Calibration Temperature	Flame Height	Pressure Drops	Flame temperature at discrete locations inside the box







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Straight Tubes

-6ST (3/8") 10L/D

Flame observed

No flame observed

	Vertical DI*	Horizontal DI*	Buoyancy	Scrubbing
Ambient conditions (box)	** 2.5"	•	•	•
Ambient conditions (no box)	0.5"	0.5"	•	•
Pressure differential	3.2"	6"	5.8"	2.1"

^{*}DI = Direct impingement

Note: Flame was observed in -6ST 20L/D test under pressure differential conditions:

4" in horizontal direct impingement configuration

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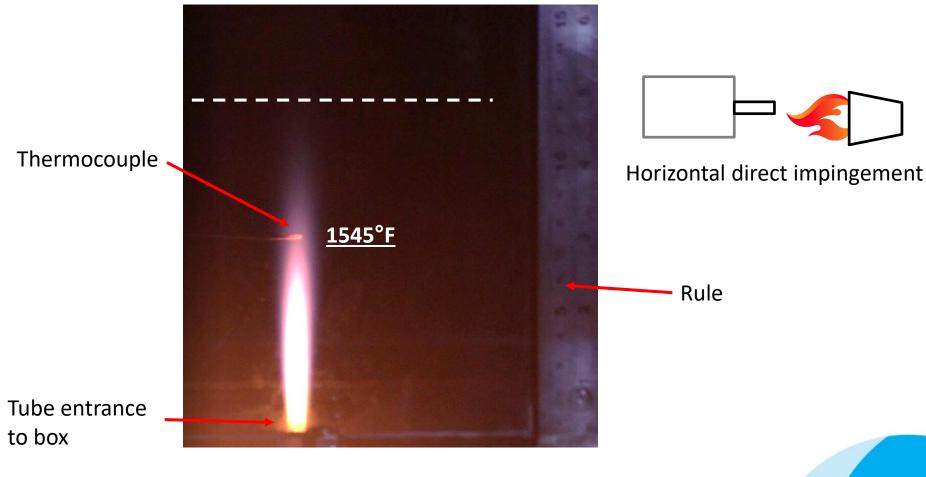
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^{**} flame height observed

Horizontal Direct Impingement Flame Ingression -6 (3/8") 10L/D Straight Tube at -0.7psi









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Straight Tubes

-12ST (3/4") 10L/D

Flame observed

No flame observed

	Vertical DI		Horizontal DI		Buoyancy		Scru	bbing
Ambient conditions (box)	•	9"		2"		5"		—
Ambient conditions (no box)	•	4.5"		4.5"		2.5"		—
Pressure differential	•	10"	•	11"		11"		3.5"

Note: Flame was observed in -12ST 20L/D test under ambient condition

2.6" vertical direct impingement configuration

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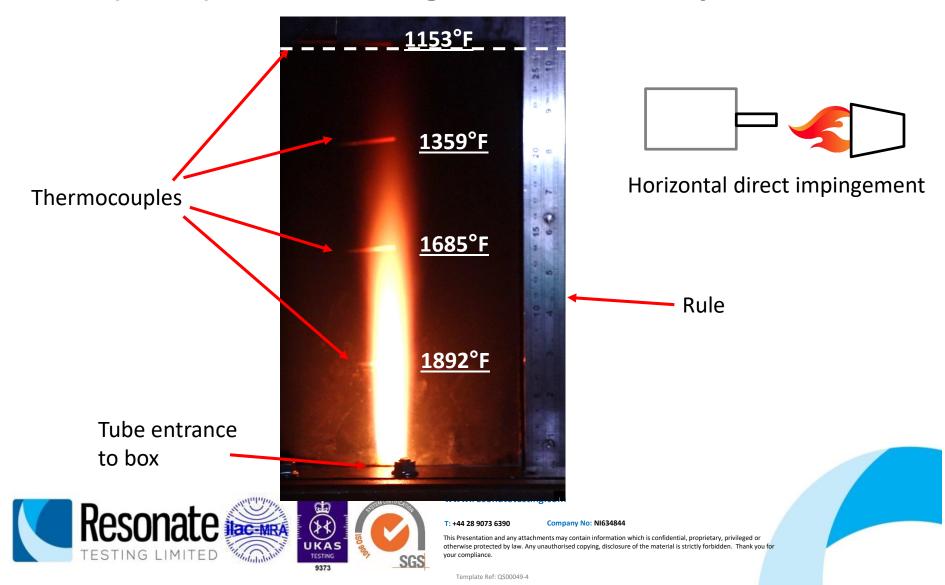


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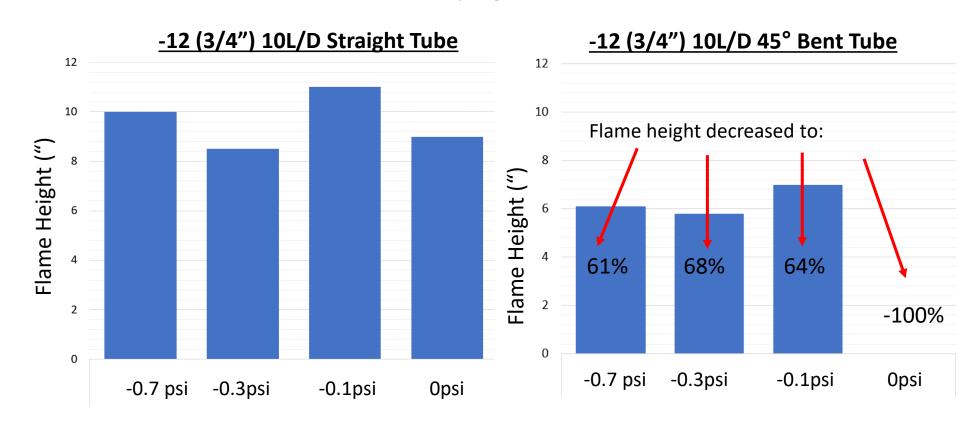
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Horizontal Direct Impingement Flame Ingression -12 (3/4") 10L/D Straight Tube at -0.7psi



Tortuous Paths

Vertical Direct Impingement - Carlin



Both tests show a decrease in flame height from -0.7psi to -0.3psi but an increase in flame height from -0.3psi to -0.1psi, which is around 1" higher than flame height measured at -0.7psi in both cases

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Holes

Flame observed

No flame observed

	Hole Ø	Vertical DI	Horizoi	ntal DI	Buoyancy	Scrubbing		
Ambient	0.2" / 5mm	•	•	1"	•	•		
conditions	0.6" / 15mm	•	•	4"	•	•		
(box)	1" / 25mm	5.3 "	•		•	•		
Ambient	0.2" / 5mm	n/a – test not carried out						
conditions (no box)	0.6" / 15mm	• 4"	•		•	•		
	1" / 25mm	• 5.5"	•		•	•		
Pressure differential	0.2" / 5mm	•	•	3.1"	•	•		
	0.6" / 15mm	•	•	10"	•	•		
	1" / 25mm	•	•	10.5"	•	•		

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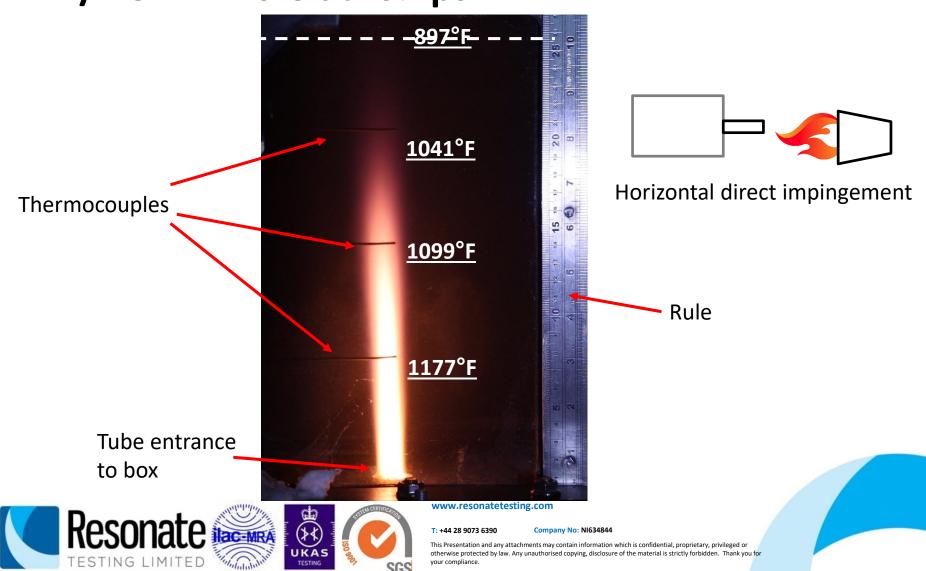


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Horizontal Direct Impingement Flame Ingression 1" / 25mm hole at -0.7psi



Slits

Flame observed

No flame observed

	Slit width	Vertica	l DI	Horizo	ntal DI	Buoy	ancy	Scr	ubbing
	0.08" / 2mm	• :	1.4"	•				•	
Ambient conditions (box)	0.2" / 6mm		3.8"			•			
Conditions (box)	0.4" / 10mm	•	7.4"	•		•			
Ambient conditions (no	0.08" / 2mm	n/a					0.8"		
	0.2" / 6mm	n/a					1.8"		n/a
box)	0.4" / 10mm			n/a		•	2.5"		n/a
Pressure differential	0.08" / 2mm	•		•	4.3"				
	0.2" / 6mm	•		•	9.5"				
	0.4" / 10mm				10.5"				

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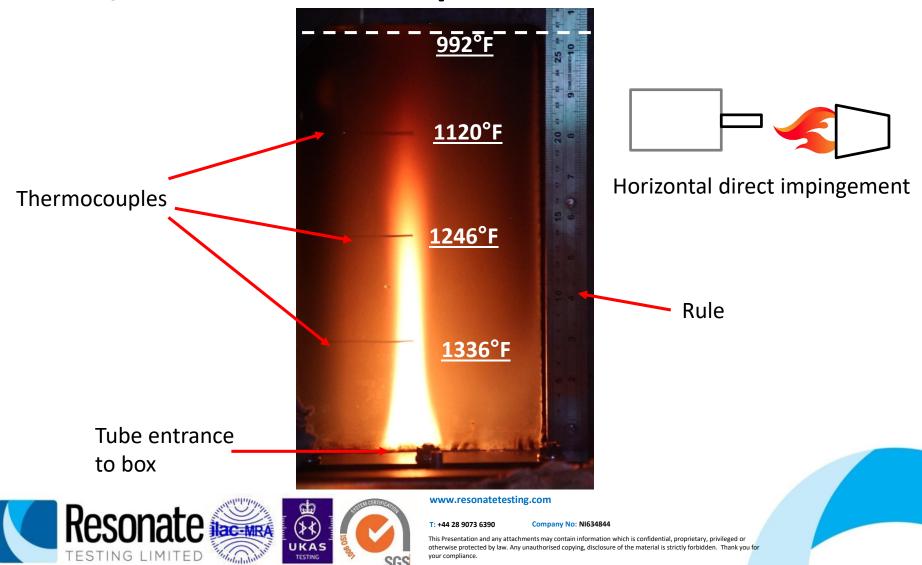


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Horizontal Direct Impingement Flame Ingression 0.4" / 10mm slit at -0.7psi



Summary

- 10L/D convention needs to be treated with caution and on a case-case basis
- Even a small pressure differential results in flame ingression
- Tortuous paths improve flame arrestor properties
- Generally, the larger the tube/gap the larger the flame is drawn through
- Gaps need to be treated with caution (both small and large) especially where there is a chance of (even a small) pressure differential
- Selected trials were run with both the Carlin and Sonic burner with the aim of distinguishing if one burner caused more flame ingression than the other. Results are inconclusive.
- Generally, temperatures recorded inside the boxes exceeded the safe temperature limit for fuel of ~400°F, unless there was no flame/glow observed







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Future Work

- This was a starting point of the R&D project we know there is room for improvement in the set up.
- Investigate how we can make changes to test set up to make it a more realistic installation –
 e.g.: add cooling airflow across the tubes to mimic zonal airflows across volumes on other side
 of firewall.
- Conduct further trials, with different sized holes, slits and tubes and also repeat data points to build upon collected data, with the aim of establishing consistent results and observing trends
- Run more trials with both Carlin and Sonic burners to build on data already collected and to
 establish if one burner causes more flame ingression than the other cannot identify from
 current data
- Understand and process existing thermocouple data. When more trials are run, gather more temperature data from thermocouples inside the box, with the aim to observe trends and examine how far above the flame the safe temperature limit for fuel is.







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Contact the following email addresses to discuss flame ingression and flame arrestor testing:

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THANK YOU FOR LISTENING ANY QUESTIONS?







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For further information on capabilities of **Resonate Testing Ltd** please do not hesitate to contact:

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