## Experiments and Numerical Modeling of Fires Associated with Lithium-Ion Batteries Thermal Runaway

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## **Computational Fluid Dynamics Lab**

#### **Principal Investigator:**

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#### Lab Mission:

- To continue to improve the accuracy and realism of the chemistry and physics underlying *computational models* of combustion, fire, and fire behavior.
- To design/perform *normo- and micro- gravity experiments* that provide data that can help clarify, prove, or suggest fire models.

#### **Research Interests:**

Fire modeling, material flammability, solid pyrolysis, ignition and flame spread, microgravity combustion, wildland fire, battery fire.





## Lithium-Ion Battery (LIB) Fires



Samsung Galaxy Note 7 Explosion (2016). Picture courtesy of New York Time.



A Tesla Model S fire after crash (2018) [NTSB/SR-20/01, 2020]



Fire of ESS in a renewable energy facility in South Korea (2018) [Park et al, Fire Sci. Engr., 2018]



A Tesla Model S was in a junkyard for 3 weeks and suddenly burst into flames. Picture courtesy of The Washington Post.

- Fire incidents related to lithium-ion batteries are more and more frequent.
- The global demand for battery cells is expected to double from 725 GWh in 2020 to 1500 GWh in 2030 [Duffner et al., 2021]



#### **Flammable Venting Gases**



Gas release from 18650 cells thermal runaway in Argon [Golubkov et al., The Royal Society of Chemistry, 2014]

Gas release from 10 Ah pouch (a) 10 Ah single cell, (b) 10 Ah array in Nitrogen.

SOC, %

[Kennedy et al., Journal of Power Sources, 2021]



 $H_2$ 

 $CO_2$ 

CO

 $CH_4$ 

×

100



## **Objectives**

- Perform *experiments* to investigate the LIB thermal runaway and its subsequent fires.
- Obtain parameters that are needed to construct a *numerical model* for the LIB fires.
- Develop a numerical model to study fire *propagation* between cells and to understand the *scalability* of battery fire.





#### **Experiment Apparatus**





- Chamber volume ~ 600L.
- The FTIR detects 21 gas species: H<sub>2</sub>O, CO<sub>2</sub>, CO, NO, NO<sub>2</sub>, N<sub>2</sub>O, SO<sub>2</sub>, HCl, HCN, HBr, HF, NH<sub>3</sub>, C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>6</sub>, C<sub>3</sub>H<sub>8</sub>, C<sub>6</sub>H<sub>14</sub>, CH<sub>4</sub>, HCHO, C<sub>6</sub>H<sub>6</sub>O, C<sub>3</sub>H<sub>4</sub>O, and COF<sub>2</sub>.





## **Schematics of the Experiment Setup**



- PID controlled heating tape (cell heating rate: 10 °C/min).
- K-type thermocouples on cell surface.
- Mass balance (0.1 g precision).
- Cell voltage measurement.
- Front and side video recorders.
- FTIR gas analyzer (21 gas species).
- H<sub>2</sub> sensor (in progress).





#### **Cylindrical Cell Setup**









## **Cell Conditioning**



# All battery experiments were conducted within <u>24 hours</u> since the cell conditioning.

Step 1: Rest 30s

Step 2: Charge: 1.3A to 4.2V, 4.2V until current falls to 130mA Step 3: Rest 30s

Step 4: Discharge:

4-1: 1.3A for 3599s (Sampling rate: 0.1 Hz)

4-2: 1.3A for 1s (to 50% SOC) (Sampling rate: 100 Hz)

4-3: Internal resistance measurement: Current pulse under -3C (-7.8 A) for 100 ms (sampling rate: 100Hz)

4-4: 1.3A for 1s. (Sampling rate: 100 Hz)

4-5: 1.3A to 2.7V (Sample rate: 0.1 Hz)

Step 5: Rest 30s

Repeat steps 1-5

Step 6: Charge: 1.3A to 4.2V, 4.2V until current falls to 130mA

Step 7: Rest 30s

Step 8: Discharge: 1.3 A to the desired SOC.





#### **Test Matrix**

-	SOC (%)	Mass (g)	Internal Resistance (m $\Omega$ )	Capacity (Ah)	Final Voltage (V)
-	30%	45.23	57.30	2.43	3.70
	30%	45.19	56.30	2.44	3.70
_	50%	45.27	58.70	2.42	3.77
	50%	45.10	62.60	2.45	3.77
Fire	50%	45.20	54.80	2.45	3.77
	50%	45.14	56.50	2.43	3.77
	75%	45.21	61.10	2.40	3.93
	75%	45.18	53.60	2.42	3.93
	100%	45.14	57.30	2.45	4.19
	100%	45.18	57.40	2.40	4.19
	Avg	45.18	57.56	2.43	
	Stdev	0.05	2.56	0.02	





#### **Example Result: Thermal Runaway at 75 % SOC**

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#### **Example Result: Cell Temperature (75 % SOC)**



Fire Dynamics Laboratory Cell swelling (t = 548.5 s)
 Cell V drop (t = 573.8 s)
 Cell venting (t = 805.5 s)
 Stronger gas emission (t = 943.6 s)
 Thermal runaway, spark and fire (t = 963.0 s)
 Expulsion of cell contents (t = 964.0 s)
 Fire extinguished (t = 983.6 s)

- Tape heating rate is at ~ 0.172°C/s or 10.32 °C/min.
- Cell voltage drops at ~ 120  $^\circ\text{C}.$
- Prior to thermal runaway, mid TC has the highest reading and the bottom TC shows the lowest.
- TC readings show a momentary dip around the onset of venting.



#### **Example Result: Cell Mass Loss and Vent Gas Species (75 % SOC)**





#### **Power Input to the Heating Tape**



6. Expulsion of cell contents

7. Fire extinguished

- 1. Cell swelling
- 2. Cell V drop
- 3. Cell venting
- 4. Stronger gas emission

**Cumulative Energy** 

$$E(t) = \int_0^t P \, dt = \int_0^t (V \times I) \, dt$$

Energy equation for a cell before thermal runaway

$$\rho c_v V \frac{dT}{dt} = \dot{q}_{tape} + \dot{q}_g - hA(T_s - T_\infty)$$

$$\uparrow$$
10 °C/min Assume negligible before

$$\Rightarrow \dot{q}_{Tape} = \frac{dE}{dt} = mc_{v}\frac{dT}{dt} + hA(T_{s} - T_{\infty})$$
Assume Increases linearly constant w.r.t. time.



TR

#### **Results: Venting and Thermal Runaway at All SOCs**

SOC: 30 %	50 %	75 %	100 %

The videos are played at <u>3 times rate.</u>





#### **Results: Venting and Thermal Runaway**



think beyond the possible

#### **Temperatures at Key Events**



- Voltage drop temperatures are insensitive to SOC.
- Venting and thermal runaway occurred at a lower temperature at a higher SOC.





#### **Cell Mass Loss at Different SOC**





#### Numerical Model (Work-in-Progress): Gas + Solid + Interface



## Numerical Model (Work in Progress): Gas



\*This preliminary simulation used mass flow inlet with 0.02kg/s of pure CH<sub>4</sub>.

- Reynolds-Averaged Navier-Stokes (RANS) equations with k-epsilon turbulence model.
- Non-premixed species combustion model.
- SIMPLE scheme with second order discretization method.
- Transient solver.





## Numerical Model (Work in Progress): Solid



- Transient solid conduction equation.
- Cell pseudo-properties deduced from the experimental data.

$$\dot{q}_{Tape} = mc_p \frac{dT}{dt} + hA(T_s - T_{\infty})$$

$$m = 0.045 \ kg; \dot{q_0} = 7.74 \frac{J}{s}; \frac{dT}{dt} = 0.172 \frac{K}{s}$$

$$\rightarrow c_p = 1,000 \frac{J}{kg \cdot K}; \rho = \frac{0.045 \, kg}{1.654 \times 10^{-5} m^3} = 2,720.60 \frac{kg}{m^3}$$



#### Numerical Model (Work in Progress): Interface

(g/s)



• UDF boundary conditions at the cell-gas interface:



- *F<sub>i</sub>* : mass fraction of species *i* in the venting gas
   *T<sub>cell</sub>*: cell temperature, solved by the solid
   model.
- f<sub>1</sub> and f<sub>1</sub> can be expressed explicitly using functions (e.g., Arrhenius equations), through look-up tables, or through ML.



#### Summary

- Experiments are performed to study Lithium-ion battery (LIB) thermal runaway and its subsequent fires, using a 600L environmental chamber.
- A standard operating procedure (SOP) along with a chamber clean-up procedure are developed for the experiments.
- Temperature, voltage, and mass loss of the battery cell, concentrations of the venting gas species, and the energy input to the battery cell are measured in-situ. Results of cells at different State of Charge (SOC) are compared.
- The time-resolved experimental data is processed to deduce parameters for model development. These include *pseudo-properties of the battery cell, venting gas compositions, and venting mass rate as functions of the cell temperature and the cell SOC*.
- The fire events in the experiments and the modeling results will be compared in both *single and multiple cell* levels. After the model is comprehensively validated, it will be used to study fire *propagation* between cells, and to understand the *scalability* of battery fire.



