FULL-SCALE CRASH TESTING OF CARGO CONTAINERS EXPERIMENTAL CHARACTERIZATION FOR TRANSPORT AIRPLANE CRASH APPLICATIONS

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Motivation

Influence of cargo loading on crashworthiness



Relevant characteristics of cargo loading

- Cargo mass → mass inertia forces introduced in the cargo floor structure
- Cargo rigidity → direct load path between cabin and cargo floor



Motivation Cargo loading



- Types of cargo loading (lower deck)
 - Bulk
 - Container
 - Pallets
 - Miscellaneous
- What is representative cargo?
 - Bulk

Container

No data available in literature 🗶



Representative ULD containers

Selected container types

- LD3 (IATA: AKE)
 - Lower deck of wide-body transport airplanes
- LD3-45 (IATA: AKH)
 - Lower deck of the single-aisle A320 family

Selected containers

- 13 used containers purchased by DLR: 4 AKH + 9 AKE containers
 - All airworthy, with negligible or minor damages
 - Same manufacturer (Driessen) and same series
- Conventional differential design (most representative)
 - Similar design for AKE and AKH containers, e.g. identical profile cross-sections





Building block approach

Container characterization





[1] M. Waimer, P. Schatrow: "Cargo Container Characterization for Airplane Crash Applications – Experimental Tests and Validation of Simulation Models", Aerospace Structural Impact Dynamics International Conference 2019, June 4-6, 2019 – Madrid, Spain

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Element level Container profile sections





Element level

Overview

Experiments

- 3P-bending
- Quasi-static (50 mm/min) and transient dynamic (2 m/s)
- Servo-hydraulic high-rate test machine

Effects

- Failure behavior significantly dependent on profile design
 - Plastic hinge development
 - Rupture of tensile loaded flanges
 - Flange holes as crack initiator
- → Good experimental data base for model validation!
 - Plasticity & damage, element size, flange hole modeling, etc.

profile 37158

profile 37157 profile 37820 profile 39127 profile 39128









Detail level Roof corner: Overview

Experiments

- Roof corner assembly: Cantilever bending
 - Tension & compression mode
- Quasi-static (50 mm/min) and transient dynamic (2 m/s)
- Servo-hydraulic high-rate test machine

Effects

- Tension mode
 - Failure behavior driven by the bolted joints
- Compression mode
 - Buckling of gusset, w/o bolted joint failure
- Good experimental data base for model validation!
 - Fastener model, model assembly



Detail level Base corner: Overview

Experiments

- Base corner assembly: Crushing
- Quasi-static (50 mm/min) and transient dynamic (2 m/s)
- Universal testing machine (q-s); drop tower (dyn)

Effects

- Bolted joint failure and structural disintegration
- Stanchion buckling after disintegration from container base
- Peak load driven by complex structural interaction
 - Compliance in the bolted joint and stanchion contact with base
 → Second load path in addition to bolted joints
- Good experimental data base for model validation!
 - Model assembly









Test setup

Drop test

- Temporary setup in the in-door test lab
- Free-falling impact plate (unguided)
 - Clear boundary conditions (no compliance in guidance)
 - Pyrotechnical release system
 - Elastic ropes for automatic alignment
- Test base
 - AKE / AKH identical base dimensions
 - Container embedded on 4 load cells
 - Boundary condition device

Data acquisition

- 4 load cells (Vertical force in each container base corner)
- 4 high-speed cameras (Front, rear, isometric views)
- 2 GoPros



Test setup





test sample (container) protective walls (flying debris) protective devices (free falling impact plate)

wooden plates (span field protection) test base (4 load cells on 2 steel beams) lights end position absorbers

data acquisition



Test matrix

- Container type (AKE & AKH)
- Door canvas & door diagonal ropes
 - Relevance for finite element model
- Container loading (Luggage)
 - Decision to test w/o luggage (empty containers), focus on container design parameters
 - Luggage test data available for separate validation; combination of both in the finite element model
- Impact speed: 6.7 m/s (22 ft/s)
 - Based on pre-test simulation (energy absorption) and final impact plate mass



Test number	Container type	Door canvas & diagonal ropes	Test identifier (incl. series number)
1	AKE	with	8062447_FSL_AKE_DYN_1
2	AKE	with	8062445_FSL_AKE_DYN_2
3	AKE	without	8063050_FSL_AKE_DYN_3
4	AKE	without	8062915_FSL_AKE_DYN_4
5	AKH	with	8063189_FSL_AKH_DYN_5
6	AKH	with	7059356_FSL_AKH_DYN_6
7	AKH	without	7059334_FSL_AKH_DYN_7
8	AKH	without	8063217_FSL_AKH_DYN_8











AKE with door canvas/ropes (exemplarily test 02)





IET COINE MANAGEMENT

AKE 62184 LH

Rear side

Jettaine

AKE 62184LH

High-speed video records



AKE with door canvas/ropes (exemplarily test 02)









AKE with door canvas/ropes (exemplarily test 02)









AKE with door canvas/ropes (exemplarily test 02)





NE 62184 4H







Force-displacement correlation acc. to ISO18571 (CORAplus, test by test correlation, 0-100 mm)

Overall rating	Min	Max	Mean
AKE	0.594 (fair)	0.857 (good)	0.748 (fair)



Force: Butterworth, cut-off 1000 Hz (50 kHz sampling frequency) Displacement: Unfiltered (5 kHZ sampling frequency) Force: Sum of local forces (four base corners) Displacement: Mean of local displacements (four impact plate positions)









AKH with door canvas/ropes (exemplarily test 05)





High-speed video records





AKH with door canvas/ropes (exemplarily test 05)









AKH with door canvas/ropes (exemplarily test 05)







AKH with door canvas/ropes (exemplarily test 05)







Test results: AKH

Data plots (all AKH tests)



Force-displacement correlation acc. to ISO18571 (CORAplus, test by test correlation, 0-100 mm)

Overall rating	Min	Max	Mean
АКН	0.651 (fair)	0.807 (good)	0.742 (fair)



Force: Butterworth, cut-off 1000 Hz (50 kHz sampling frequency) Displacement: Unfiltered (5 kHZ sampling frequency) Force: Sum of local forces (four base corners) Displacement: Mean of local displacements (four impact plate positions)

Final outcomes





Final outcomes

Force-displacement

Crash characteristics under purely vertical impact conditions

Same general crash phases for both container types



Force-displacement correlation acc. to ISO18571

Overall rating	Min	Max	Mean
AKE	0.594 (fair)	0.857 (good)	0.748 (fair)
АКН	0.651 (fair)	0.807 (good)	0.742 (fair)





Force: Sum of local forces (four base corners), filtered data: Butterworth, cut-off 1000 Hz (50 kHz sampling frequency) Displacement: Mean of local displacements (four impact plate positions), unfiltered data (5 kHZ sampling frequency)

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Final outcomes

Crash characteristics under purely vertical impact conditions

Energy-displacement

Total absorbed energies in the same range for both container types







Container type (AKE vs. AKH)

- Identical general crash phases for both container types
- Initial force peak in the same range (Reasonable: Design similarities for both container types)
- Second force peak different for AKE and AKH (AKH: Stanchion disintegration during initial force peak)
- Post-peak domain different for AKE and AKH (different design: stanchion length and number of balconies)
- Total absorbed energies in the same range

Door canvas & diagonal ropes

- Test results indicate no noticeable influence of door canvas and diagonal ropes
- Tests in the same force-displacement range
- No effects identified by high-speed video records or post-test inspections

Outlook



Finalization of research program

 Post-test simulations and final model validation of AKE and AKH simulation models

Application of container finite element models

 Simulation driven investigations on the effect of container loading under real-world crash conditions







Thank you for your attention!

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Appendix AKE vs. AKH design





Appendix Secondary crash effects in the balcony structure (post-peak domain)



