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# **Effective Aircraft Seat Development for Row to Row HIC test**

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10<sup>th</sup> Triennial international aircraft fire and cabin safety research conference / Oct.17-20, 2022 / Atlantic City, NJ

# Agenda

1. Background

- 2. Goals
- 3. Setting target of seat function
- 4. Creation of simple model
- 5. Application example
- 6. Conclusion
- 7. Future work

# Current aircraft seat dynamic qualification tests use the <u>H</u>ead <u>Injury</u> <u>C</u>riteria (<u>HIC</u>) to evaluate head protection. Difficult to understand which characteristics contribute the HIC value.

- Seat supplier must satisfy HIC with overall seat system, but the parts other than those of the seat supplier may be incorporated to the seat.
- Development verified by detailed seat model as conventional manner is costly and it takes time to complete the analysis.

Clarifying the correlation of each characteristics of component items by using Model Based Development, then define target characteristics for product design.



# 1. Background

# 1. Background

### Application of Model Based Development to row to row HIC test

• Row to row HIC test (Zone C)

To confirm whether the occupant's head injury, femur load and post-test seat deformation condition within the limit or not, in case the inertia load of emergency landing occurred with multiple row layout.

#### HIC ≦ 1000

Femur compression Load  $\leq 2250$  lbf Deformation: within the limit, no harmful edge or injurious protrusion

HIC is calculated by following formula with Head Acceleration

$$HIC = \left\{ \left[ \frac{1}{(t_2 - t_1)} \cdot \int_{t_1}^{t_2} a(t) dt \right]^{2.5} (t_2 - t_1) \right\}_{max}$$

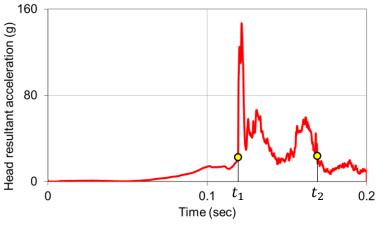
Where a(t) is the resultant acceleration of the CG position of anthropomorphic test device head in g's, and  $t_1$  and  $t_2$  are times in the response that maximize the function.

Head Acceleration element

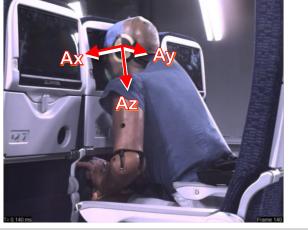
Before test

Head impact during test











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Extracted from AC 25.562-1B

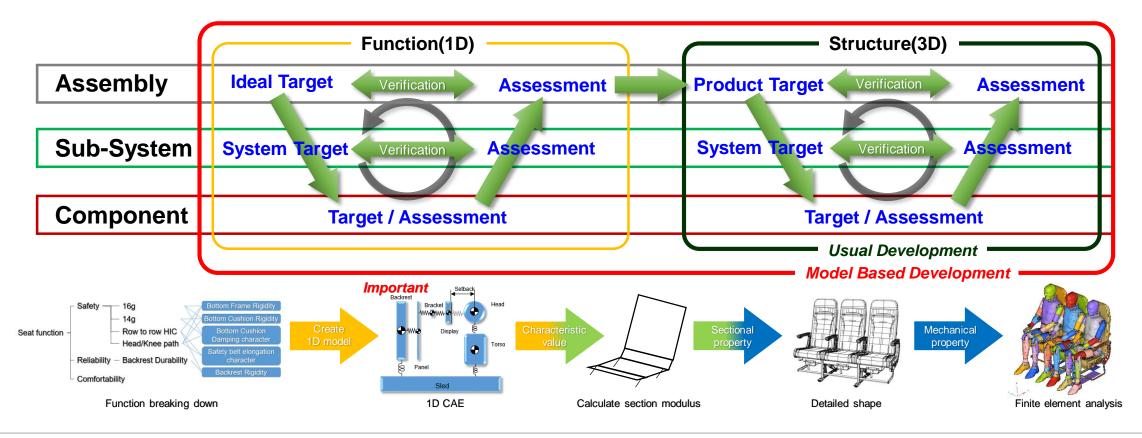


1. Background

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What's Model Based Development?

To develop a product from functional perspective in prior to structural verification phase.



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• What's 1D CAE?

Backrest

1. Background

Representing the entire target product on function basis without omission and evaluating them. It is possible to design overall appropriately at the upstream stage of product development.

#### Physical Model (1D CAE model)

Head

Neck

Chest

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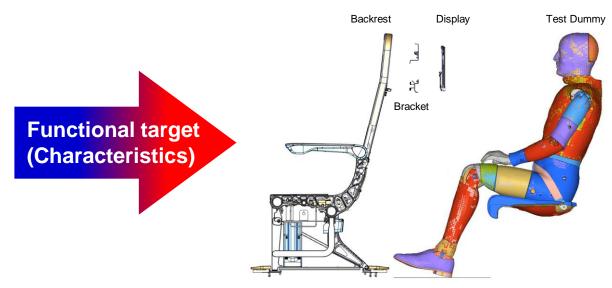
Represent physical phenomenon as simple model (can be replaced by mathematical formula), then verify the functional target

-WW Translational rigidity - Rotational rigidity

Sled

Design the shape of structure that satisfies the functional target





# 1. Background

• Procedure of model based development

### <u>1. Consider the ideal performance of seat</u> (Value design/conceptual design/statement) Determine what kind of seat to design and where to put the value into.

# 2. Generate function tree and clarify the interaction among each characteristics.

Breaking down overall target into types of functions. Make what the target consists of visible.

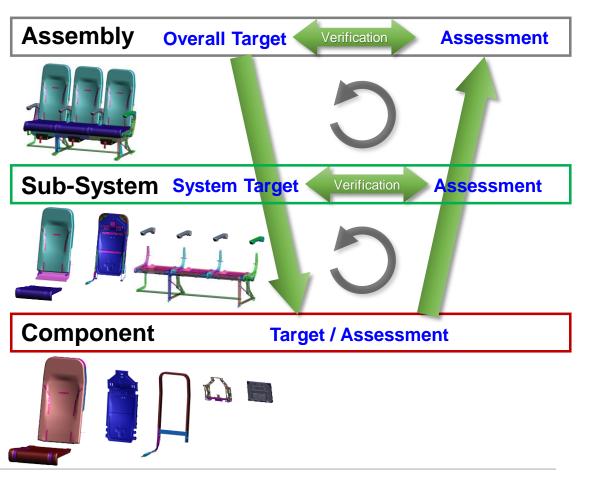
#### 3. Generate function model

Make simple function model and understand the behavior. Generate function model at necessary fineness level, then confirm the sensitivity.

#### 4. Allocate functional target

Set target value of component part and predict performance.

#### Development



Frame durability

Cushion hardness

Sitting comfort

Reliability

Pressure distribution

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From partial optimization to overall optimization ullet

Constitution of parts

Layout

Optimization of overall seat function

1. Background

Frame rigidity

Comfortability

Fatigability

Safety • Fabric property Appearance performance target. Clarify the relationship and Outer shape allocate functional target ٠ **Operation** load Usability Operability

Characteristics have relationship beyond the type of function

- Seat function have many categories such as "Safety", "Reliability", "Comfortability" etc. And various component characteristics are closely related to their
- To achieve goals with overall seat in a well-balanced manner, it is necessary to clarify the relationships between each function and characteristics, then optimize and allocate the functional target.

# 1. Background

# Advantage of 1D CAE

### 1. Front loading of development

Required characteristics can be drafted when shape is not determined yet, and the discussion can be conducted dynamically about the allocation of functional target. Achievement scenario may be found by creating model based on physical principle.

#### 2. Optimization of multiple functions

Overall non-defective condition can be found by confirming the interaction between multiple functions. Easy to conduct verification with varied characteristics, and it may arrive to the new achievement scenario.

#### 3. Shorten development duration

Compared with 3D CAE, calculation duration is short, so many variations of characteristic can be verified in a short period. In addition to this, the completed model can be utilized continuously by improving and updating.

# 2. Goals

- Goals of this report
  - Construct a simple model that can confirm the behavior of each characteristic value with respect to HIC in row to row HIC test.
  - Find the better function allocation (amount of influence and sensitivity) among them by using created 1D CAE model.

# 3. Setting target of seat function

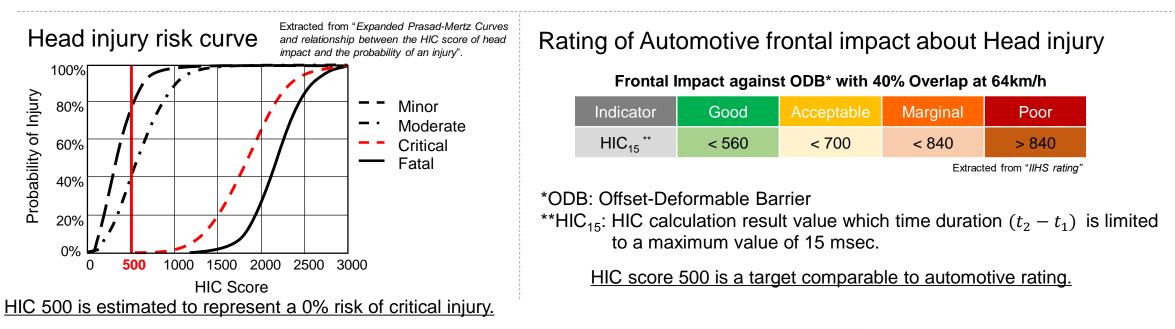
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## Setting target Value of HIC

#### Which conditions are better?

Ideal  $\cdot$  No Head impact to front seat  $\rightarrow$  Increase seat pitch upto enough space (Unrealistic in economy class)

Target  $\cdot$  Reduce head injury probability level  $\rightarrow$  Make "critical" probability to 0% in Head injury risk curve



From the above, the target value of HIC is set at 500 or less.

# 3. Setting target of seat function

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## Relationship between HIC value and Head acceleration

Acceleration

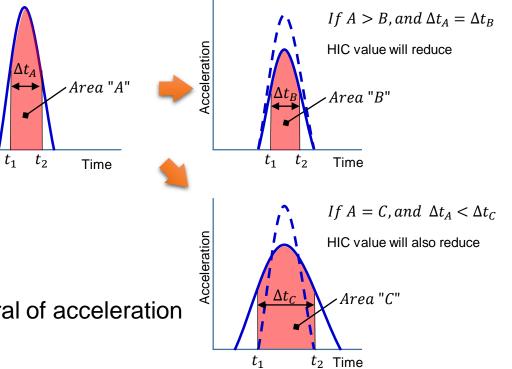
**Condition:** If pulse shape of head acceleration of 1<sup>st</sup> collision is comparatively large, HIC value may be determined by 1<sup>st</sup> collision pulse magnitude only. In such case, HIC value may be reduced by changing pulse shape of head acceleration as below.

Expanding the HIC calculation formula for clarify, we get

$$HIC = \left\{ \frac{1}{(t_2 - t_1)^{1.5}} \cdot \left[ \int_{t_1}^{t_2} a(t) dt \right]^{2.5} \right\}_{max}$$

HIC value will be decreased if  $\Delta t (t_2 - t_1)$  increased or integral of acceleration (i.e. area) is decreased.

**Our approach:** <u>Verify the response against each characteristics by using 1D</u> <u>CAE</u>, because  $\Delta t$  is variable which is determined from the pulse shape of acceleration.



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# **Condition:** There are cases when $\Lambda t$ will become

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Acceleration

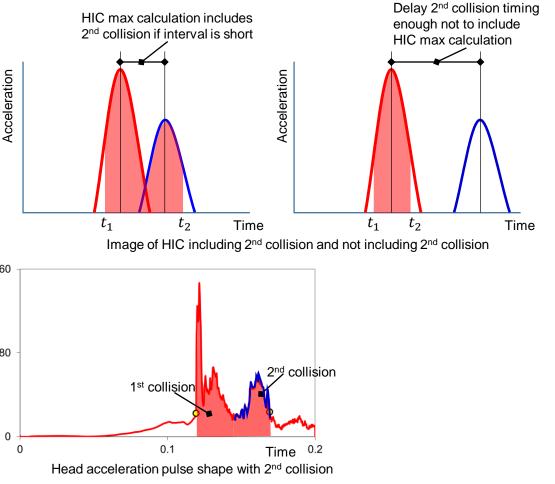
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long and include the acceleration of 2<sup>nd</sup> collision to HIC value calculation, because  $\Delta t (t_2 - t_1)$  is determined so as to maximize the HIC value. In such case, HIC value may be reduced if the time interval of collisions can be increased.

Our approach: It is also verified by using 1D CAE how the response against each characteristics indicate.

# 3. Setting target of seat function

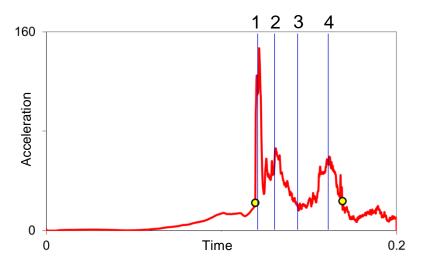
Relationship between HIC value and Head acceleration



# 4. Creation of simple model

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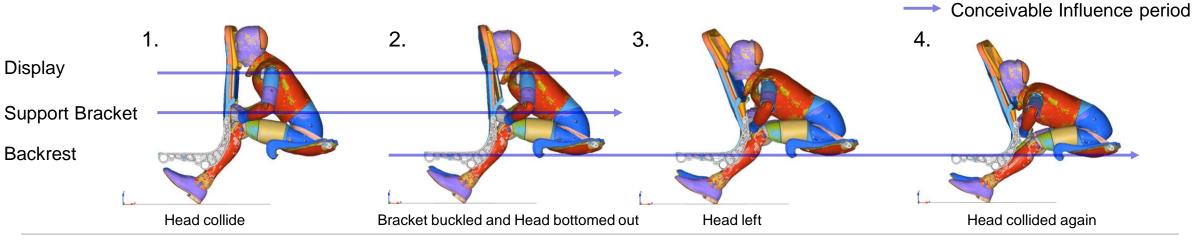
### Confirmation of Head Acceleration occurrence mechanism



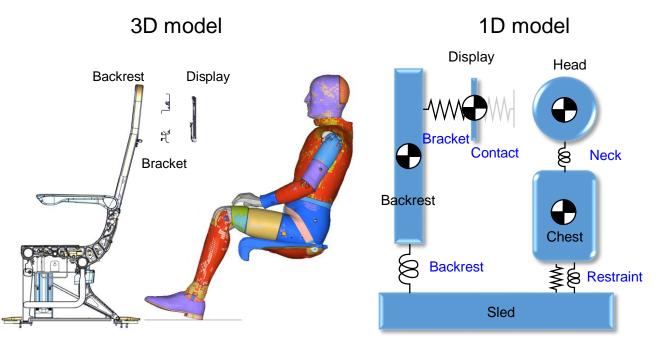
By observing the behavior during the test, the collision phenomena 1 to 4 can be confirmed, and extract the items that are thought to affect the head acceleration in each state.

- 1. Head collide with display and head acceleration have highly raised.
- 2. Display support bracket have buckled and bottomed out, then head acceleration have raised again.
- 3. Backrest have leaned forward and head left backrest.
- 4. Backrest have leaned rearward and head collide with backrest again.

From the above, at least the head, display and backrest must be represented as mass points, and the collision rigidity between head and display, the rigidity of bracket that support display, and rotational rigidity of backrest are necessary.



### Summary of simple 1D model



Use "Simulation X", a physical modeling software developed by ESI ITI, for creating and analyze 1D CAE model.

Create simple model with Backrest, Display and Head as mass points.

Since the head trajectory is not a translational motion but a rotational motion, the chest mass point have been also incorporated. The each rigidity values between each mass points have been also incorporated.

Each characteristic value and position are acquired from existing seat parts and test dummy in order to increase reproducibility.

#### Input parameter:

Item	Mass	Inertia moment	Location	Rigidity	Acceleration from sled
Hinge	-	-	Х	-	Х
Backrest	Х	Х	Х	Rotate	-
Bracket	-	-	-	Translation	-
Display	Х	Х	Х	-	-
Contact	-	-	-	Translation	-
Head	Х	Х	Х	-	-
Neck	-	-	-	Rotate	-
Chest	Х	Х	Х	-	-
Restraint	-	-	Х	Translation & Rotate	Х

# 4. Creation of simple model

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Validation of Display linear rigidity



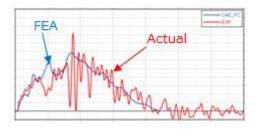




Actual test

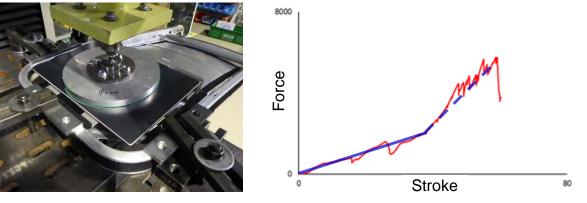


FEA model



Identify the equivalent display stiffness by reproducing the test with FEA model Validation of Display support bracket linear rigidity

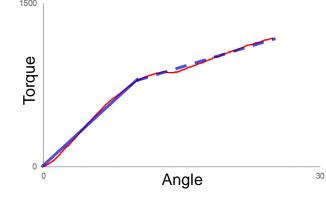
Obtain Force-Stroke graph with component configuration



# Validation of Backrest rotational rigidity

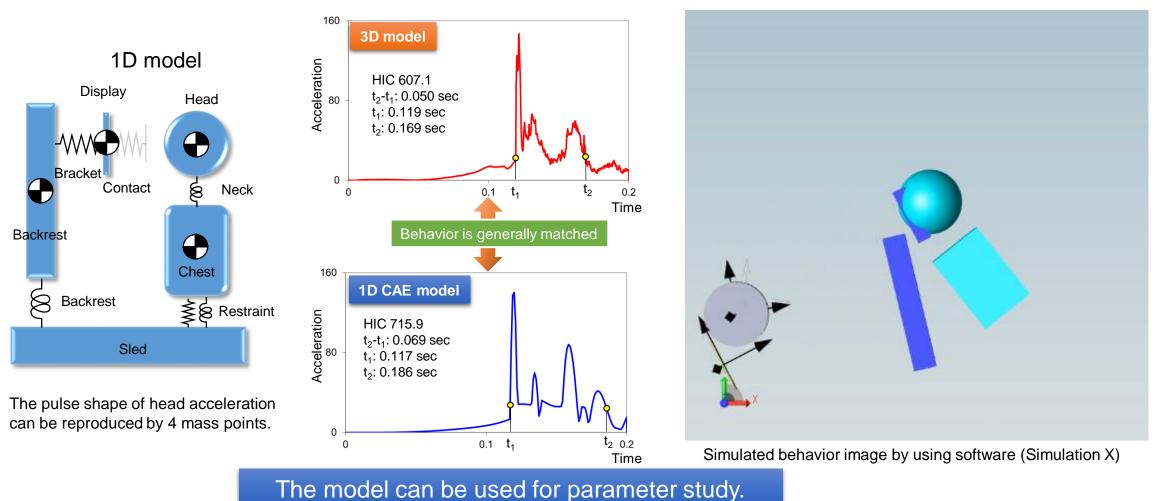
Obtain Torque-Angle graph with component configuration





# 4. Creation of simple model

## Confirmation of reproducibility



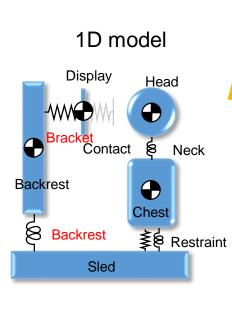
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### Verification of changes in characteristics values

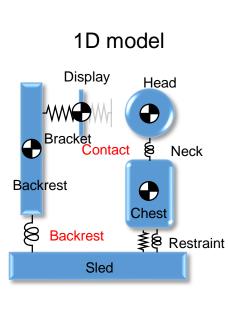
		Bracket Rigidity							
		50%	60%	70%	80%	90%	100%	150%	200%
	50%	609.0	512.7	503.6	500.9	503.2	503.1	528.9	537.9
	60%	717.8	645.1	622.3	598.5	575.3	557.9	565.5	577.1
iditv	70%	809.2	767.0	730.9	718.9	696.1	655.5	615.7	622.3
Rig	80%	847.9	824.0	818.5	776.2	726.3	682.7	610.5	632.6
ckrest	90%	903.6	855.7	813.3	783.7	729.6	703.8	604.8	615.3
Back	100%	929.1	873.2	813.6	774.8	731.5	715.9	582.2	600.1
	150%	946.5	942.9	814.8	788.5	728.4	654.3	607.0	595.0
	200%	1290.3	1013.7	837.0	794.9	785.4	768.7	672.6	643.4



### Verification of changes in characteristics values

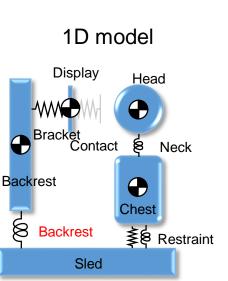
		Contact Rigidity								
		50%	60%	70%	80%	90%	100%	150%	200%	
	50%	330.9	325.9	369.4	413.2	455.3	503.1	712.8	911.9	
	60%	367.3	395.4	436.3	477.2	521.0	557.9	800.1	1013.9	
idity	70%	416.3	472.0	522.9	571.4	612.9	655.5	879.5	1147.6	
Rig	80%	451.1	503.1	559.4	602.9	657.3	682.7	889.1	1101.4	
krest	90%	459.2	518.2	570.2	621.7	661.4	703.8	953.2	1169.1	
Back	100%	460.3	515.6	558.2	613.8	649.5	715.9	954.4	1262.8	
	150%	436.4	491.1	541.0	599.0	630.9	654.3	1030.9	1333.2	
	200%	422.6	489.2	558.8	615.8	692.0	768.7	1070.7	1268.2	

The lower the rigidity, the lower the HIC Value

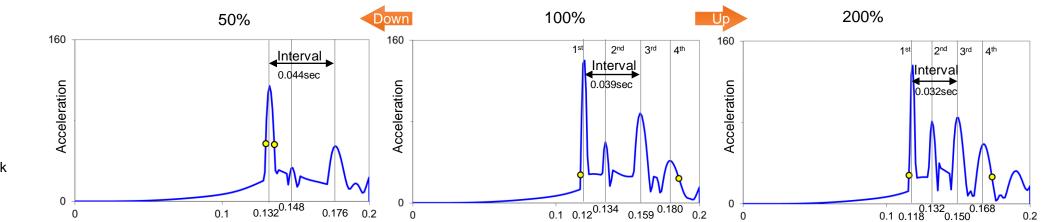


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### Verification of changes in characteristics values



### Backrest rigidity



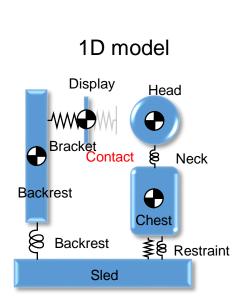
Backrest rigidity affects the first collision timing and time interval of collisions. This is because the natural frequency was changed as a result of rigidity change.

A natural frequency is obtained by a calculation formula  $f = \frac{1}{2\pi} \sqrt{\frac{k}{m}}$ .

This behavior matches the theoretical formula, and it can be seen that it is able to be changed by rigidity and mass.

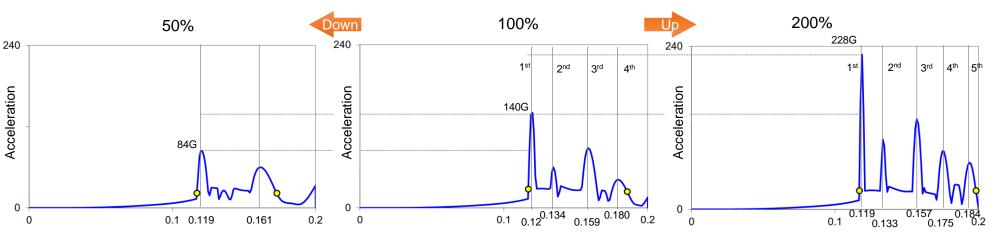
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### Verification of changes in characteristics values



### **Contact rigidity**

Acceleration



Contact rigidity strongly affects the peak of collision acceleration.

According to equation of motion ma + kx = 0, the peak of acceleration was changed as rigidity change.

The time interval between collisions is linked to the natural frequency, just like Backrest case.

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### Verification of changes in characteristics values

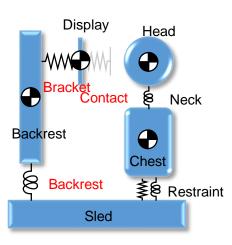
#### Summary of the confirmation results

 Image: Figure 1
 Image: Figure 2
 Image: Fig

Legend - XX: Strong correlation, X: Correlation, —: No correlation

HIC value can be reduced mainly by the rigidity of Backrest and Contact. Backrest rigidity contributes the time interval between collisions. Contact rigidity contributes the peak value of Head acceleration.

1D model



### Verification result

$\square$		Bracket Rigidity									
	$\searrow$	50%	60%	70%	80%	90%	100%	150%	200%		
	50%	609.0	512.7	503.6	500.9	503.2	503.1	528.9	537.9		
	60%	717.8	645.1	622.3	598.5	575.3	557.9	565.5	577.1		
Rigidity	70%	809.2	767.0	730.9	718.9	696.1	655.5	615.7	622.3		
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Bac	100%	929.1	873.2	813.6	774.8	731.5	715.9	582.2	600.1		
	150%	946.5	942.9	814.8	788.5	728.4	654.3	607.0	595.0		
	200%	1290.3	1013.7	837.0	794.9	785.4	768.7	672.6	643.4		
$\square$	<u> </u>	Contact Rigidity									
	$\geq$	50%	60%	70%	80%	90%	100%	150%	200%		
	50%	330.9	325.9	369.4	413.2	455.3	503.1	712.8	911.9		
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#### **Combination of Backrest and Bracket rigidity**

No combination of parameter satisfying the target of HIC 500 or less could be found. To satisfy HIC 500 or less, reduction by other characteristic value is required.

#### **Combination of Backrest and Contact rigidity**

Multiple combinations satisfying HIC 500 or less were found, but all of them require reduction of contact rigidity. (Area surrounded by red frame) Each parameter must be verified by the other related functions.

# 6. Conclusion

Summarizing this activity as follows:

- The simple model which can confirm the behavior of characteristics about row to row HIC test could be generated.
- The combination of characteristics which satisfy with the target HIC value could be found by 1D CAE.
- The hypothesis verification cycle by using 1D CAE is fast, so countermeasures can be verified in a short period.
- It is possible to know the amount of influence of characteristic value changes in the absence of actual components.
- 1D CAE is suitable for verification of changes in physical quantities (rigidity, mass, arrangement)
- Function models (1D model) are useful for checking the behavior of characteristic values. Also useful for understanding the interaction between component items.

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7. Future work

Summarizing future works as follows:

- Plan to create 1D CAE model about the other test items and subsystems for increasing functions that can be optimized.
- Utilize this 1D CAE model for proposing required characteristics to the new design seat.

# Thank you



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