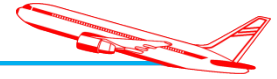


Temperature rise study on fluid in tube subjected to oil burner



Long Chen

Oct. 28, 2019

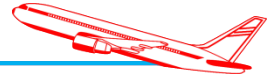


Introduction

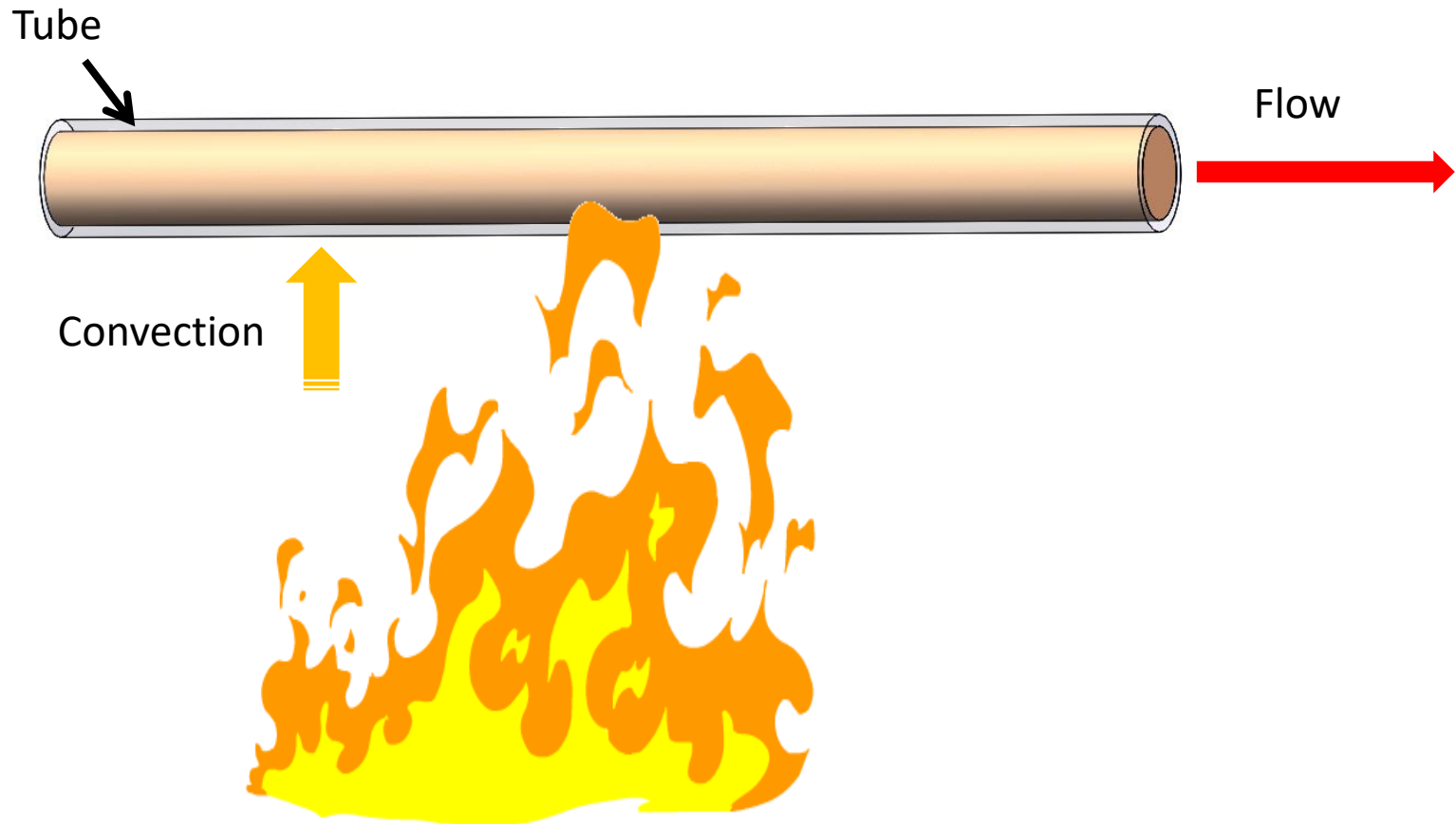
- ◆ Tubes & hose assemblies in engine nacelle of an aircraft
- ◆ Distributing fuel, hydraulic oil & lubricant
- ◆ Tested by oil burner

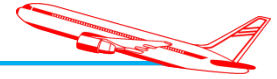
ISO 2685-1998

Aircraft Materials Fire Test Handbook

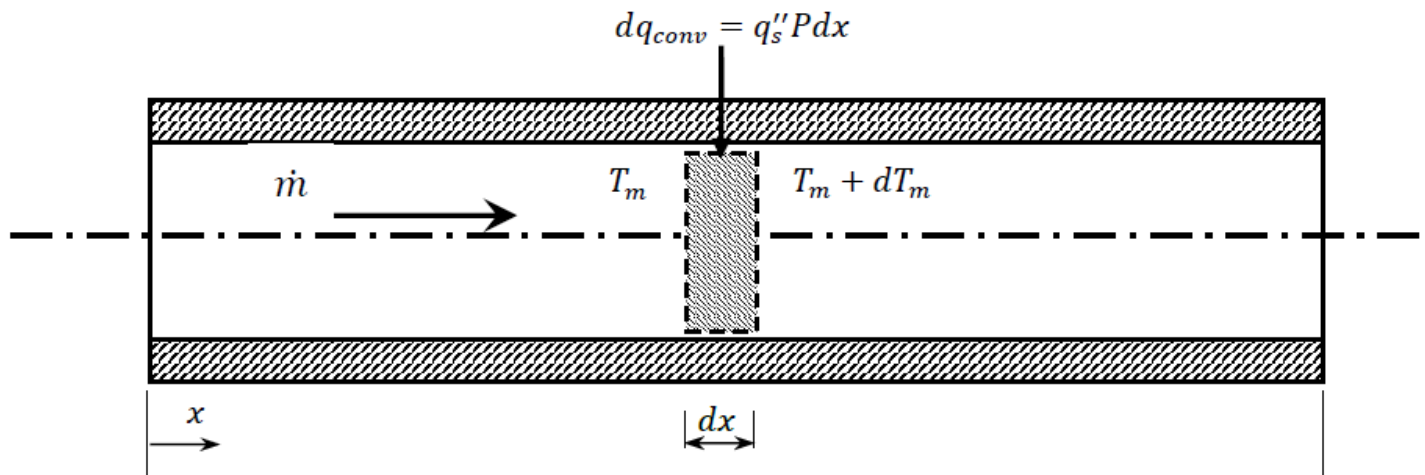


Heat transfer process





Heat transfer process

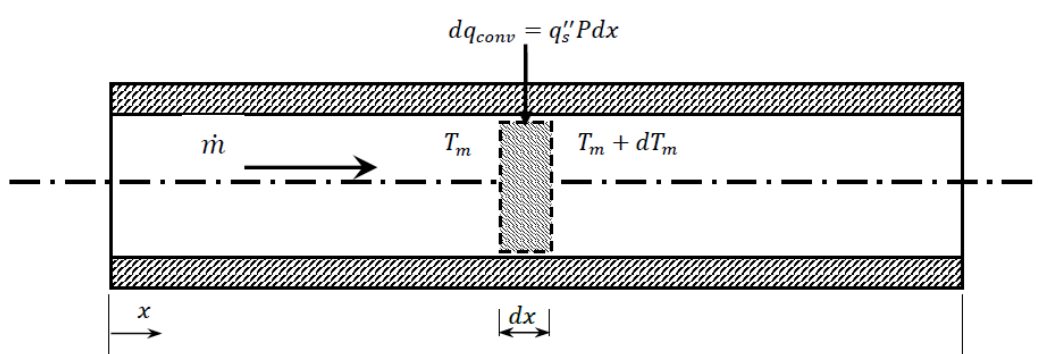


$$dq_{conv} = \dot{m} C_p [(T_m + dT_m) - T_m] = q_s'' P dx = q_s'' \pi D dx$$



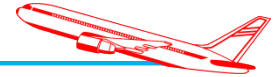
Assumptions

- The temperature of position x can be represented by average temperature of this cross section, ignoring the radial temperature gradient
- As metallic tube has a relatively **low heat capacity** and a relatively **high heat conductivity**, the conventional heat absorbed by oil is approximately equal to total heat transfer of the outer surface, the flame.



$$dT_m = \frac{q_s'' \pi D dx}{\dot{m} C_p}$$

$$T_o - T_i = \frac{q_s'' L \pi D}{\dot{m} C_p}$$



Experiment configuration

◆ Hose assembly

Fuel & lubricant, 12mm I.D., 500mm long stainless steel tube, 50 to 200 L/hr

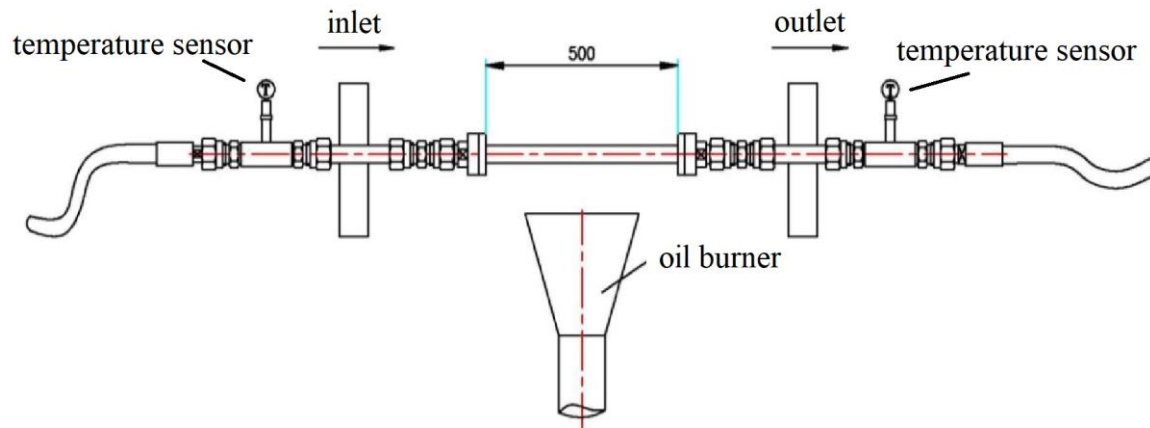
◆ BTU Heat Transfer Device

Water, 12mm I.D., 380mm long cooper tube, 2.6 to 3.8L/min(156 to 228 L/hr)



Hose assembly

- No.3 Jet Fuel(Jet A-1) and RIPP 4050 are utilized
- Carlin CRD200 burner
- Air velocity: 2300 FPM
- Fuel flow rate: 2.1GPH





Hose assembly

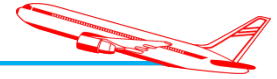
- The flame of the burner is not evenly distributed
- Temperature rise has a linear relationship with heat flux density $\longrightarrow q_s'' \approx \overline{q_s''}$
- Heat flux density of 11 horizontal points with the same distance from the burner tip is measured by Garden Gauge



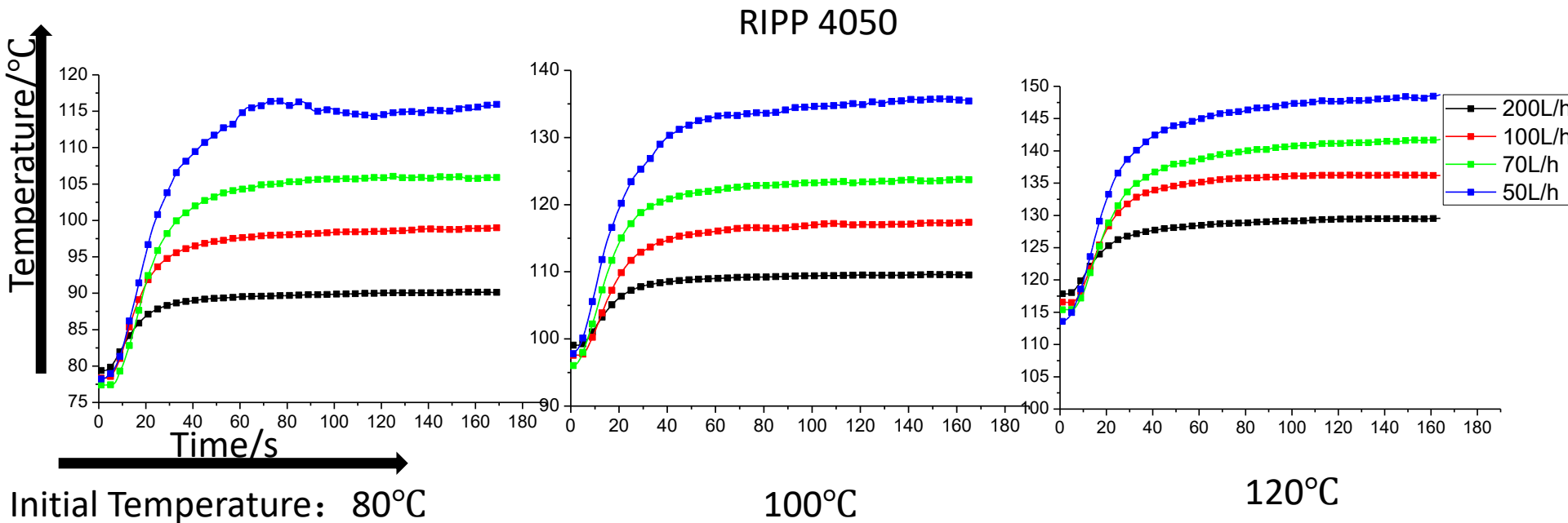
Hose assembly tests

Position[mm]	0	50	100	150	200	250	300	350	400	450	500
Heat flux Density [W/cm ²]	2.8	4.7	7.4	8.0	12.0	12.2	10.8	6.0	5.3	2.9	1.7

- The position presents distance from the inlet of the tube.
- The average value $\overline{q_s''}$ is 6.445 W/cm².



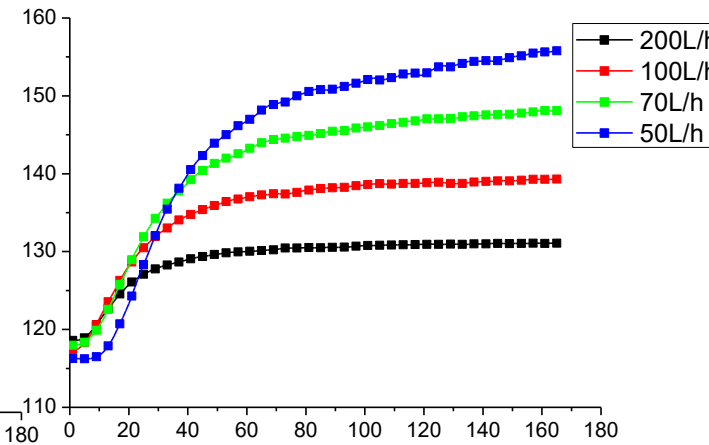
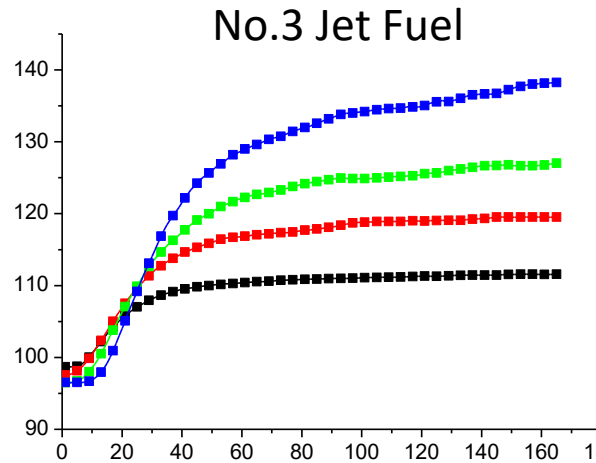
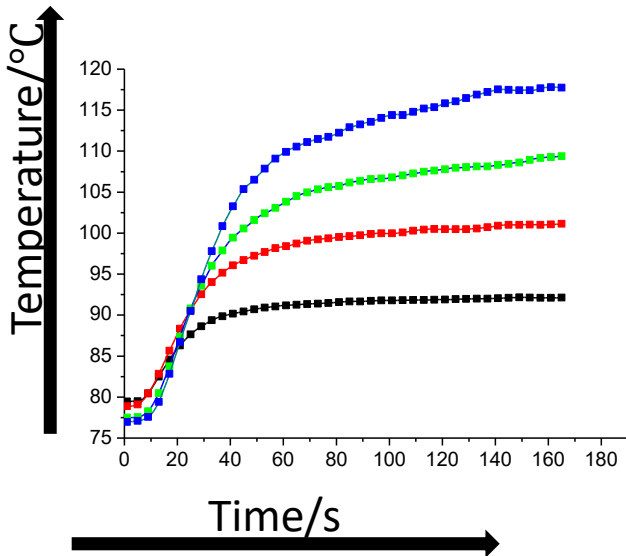
Test Results



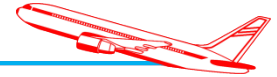
Higher fluid flow rate refers to smaller temperature rise



Test Results



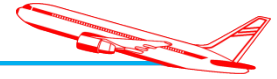
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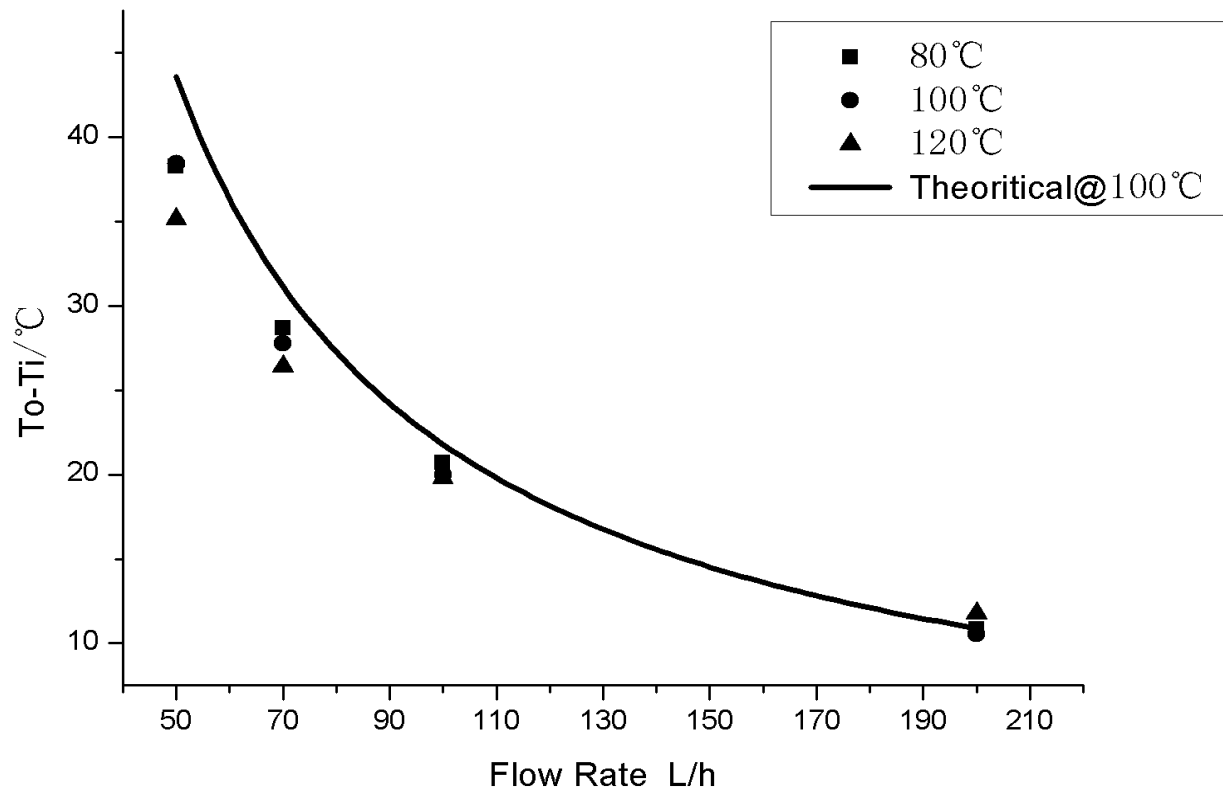
Hose assembly tests

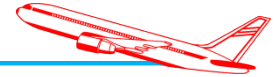
- The density of RIPP 4050 is 0.9687kg/L@100°C
Considered to be constant to simplify the calculation
- Heat capacity $C_p=2.07\text{kJ/kg}\cdot\text{K}$, $L=0.5\text{m}$, $D=0.012\text{m}$

$$T_o - T_i = \frac{q_s'' L \pi D}{\dot{m} C_p} \quad \Rightarrow \quad (\dot{V} \Delta T)_{\text{Lubricant}} = 2180 ,$$



Hose assembly tests





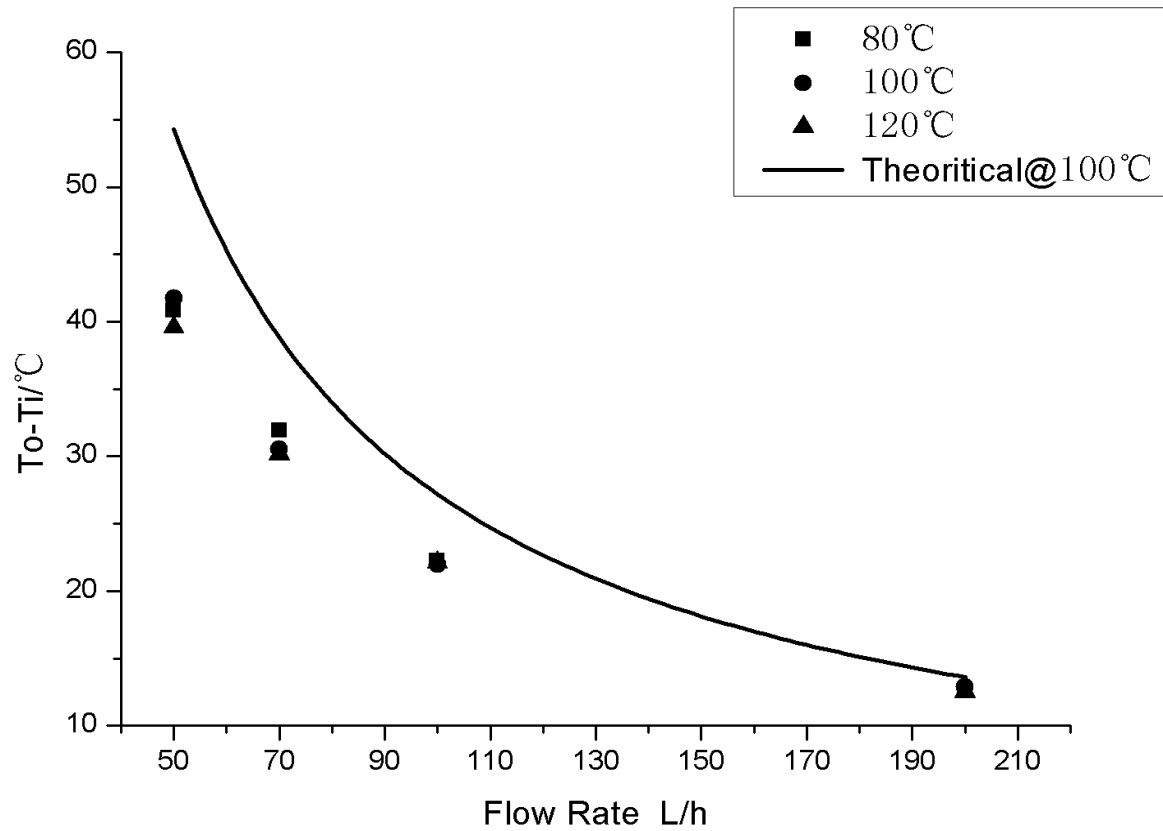
Hose assembly tests

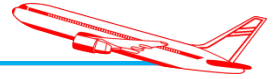
- The density of No.3 Jet Fuel is 0.73kg/L@100°C
Considered to be constant to simplify the calculation
- Heat capacity $C_p=2.35\text{kJ/kg}\cdot\text{K}$, $L=0.5\text{m}$, $D=0.012\text{m}$

$$T_o - T_i = \frac{q_s'' L \pi D}{\dot{m} C_p} \quad \Rightarrow \quad (\dot{V} \Delta T)_{Fuel} = 2716 ,$$

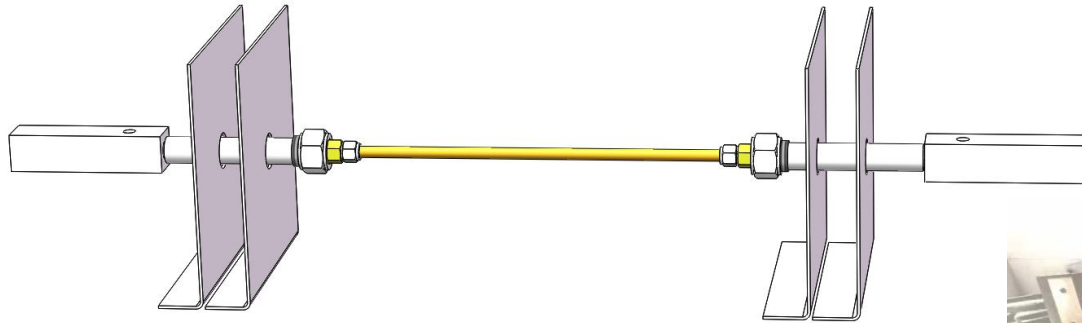


Hose assembly tests





BTU Heat Transfer Device

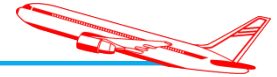




BTU Heat Transfer Device

Position[mm]	0	50	100	150	200	250	300	350	400	450	500
Heat flux Density [W/cm ²]	2.8	4.7	7.4	8.0	12.0	12.2	10.8	6.0	5.3	2.9	1.7

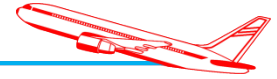
The average value $\overline{q_s''}$ within 400mm range is 8.66 W/cm².



BTU Heat Transfer Device

- The density of water is 1.0kg/L@25°C
- Heat capacity $C_p=4.185\text{kJ/kg}\cdot\text{K}$, $L=0.380\text{m}$, $D=0.012\text{m}$
- The temperature of inlet water is 21°C

$$T_o - T_i = \frac{q_s'' L \pi D}{\dot{m} C_p} \quad \Rightarrow \quad (\dot{V} \Delta T)_{\text{water}} = 1067,$$

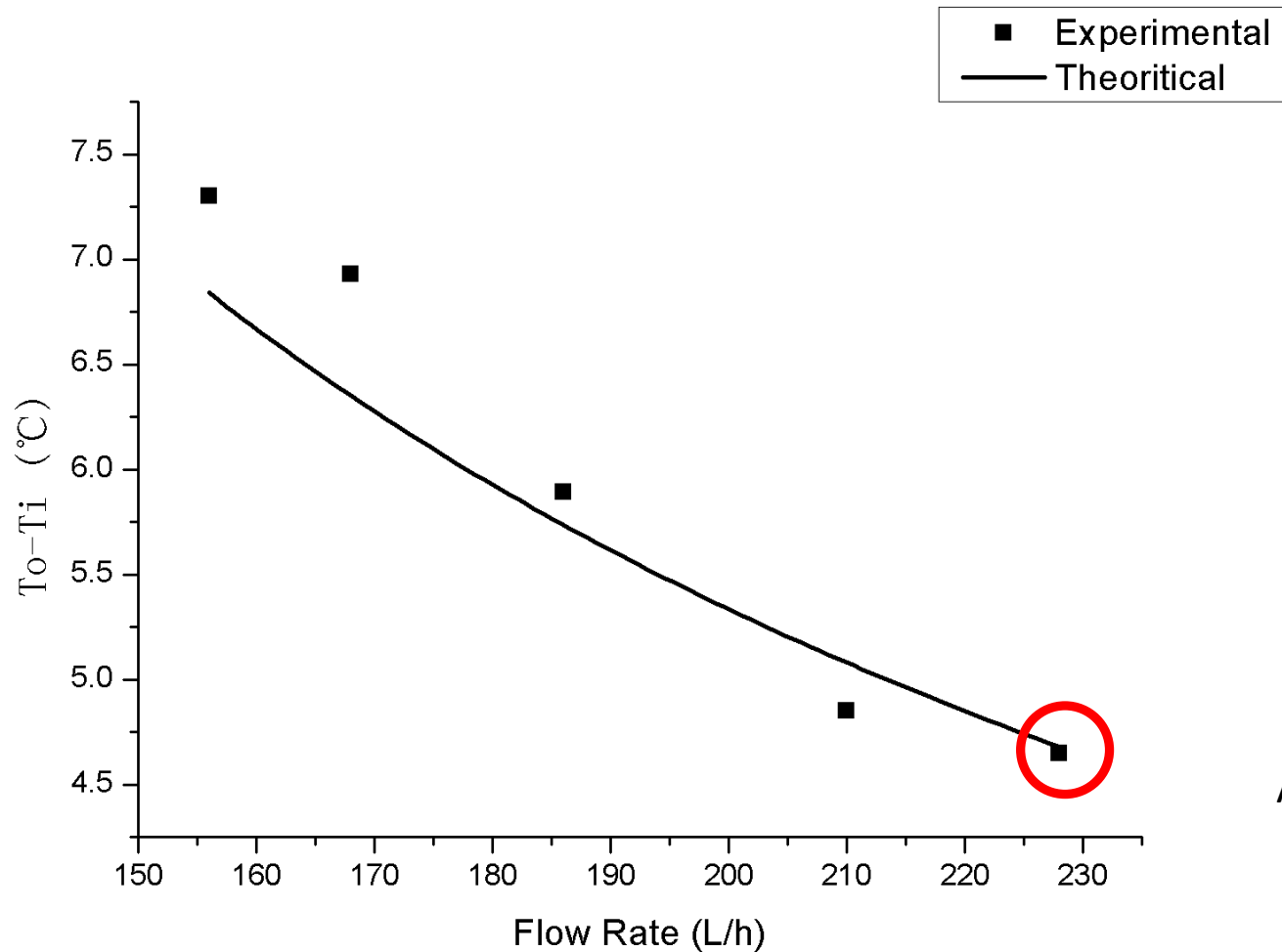


BTU Heat Transfer Device

Flow Rate L/h	156	168	186	210	228
Delta Temp. Measured °C	7.3	6.93	5.89	4.85	4.65
Delta Temp. Calculated °C	6.84	6.35	5.74	5.08	4.68



BTU Heat Transfer Device



A little lower?



BTU Heat Transfer Device

Aircraft Materials Fire Test Handbook Chapter 11 P11 & Chapter 12 P4

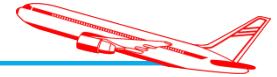
12.6.5.2.3 After the warmup period, record the inlet and outlet temperatures every 30 seconds for a 3-minute period. Determine the rate of Btu increase of the water as follows:

$$\begin{array}{lcl} 1314\text{W} & = & \overset{263}{\cancel{146}} \times 5^{\circ}\text{C} \text{ watts (for Celsius)} \\ 4500 \text{ Btu/hr} & = & 500 \times 9^{\circ}\text{F} \text{ Btu/hr (for Fahrenheit)} \end{array}$$

where: T_o = temperature ($^{\circ}\text{C}$ or $^{\circ}\text{F}$) at outlet

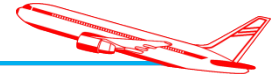
T_i = temperature ($^{\circ}\text{C}$ or $^{\circ}\text{F}$) at inlet

12.6.5.2.4 The heat transfer rate output, as determined by the equation shown in section 12.6.5.2.3, will be a minimum of 4,500 Btu/hr (1,314 W). If the heat output from the burner is not above the minimum, make adjustments to the burner and repeat sections 12.6.1 through 12.6.5.2.3.



Conclusions

- For tube carrying fluid and subjected to oil burner, relationship between flow rate and temperature rise was studied and can be expressed as $T_o - T_i = \frac{q_s'' L \pi D}{\dot{m} C_p}$
- Experimental corresponds with the theoretical calculations very well.
- For Btu heat transfer device, the delta temperature seems to be a little lower than requirement in handbook, in both ways. Does it denote that the flame calibrated by Garden Gauge may not meet the requirement of Btu heat transfer device?



QUESTIONS ?

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