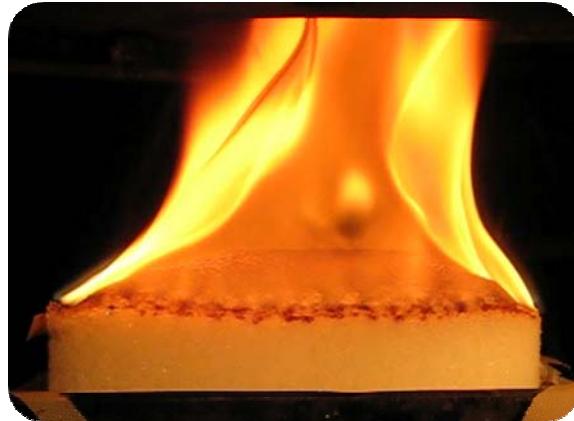


The Effect of Dimensional and Morphological Changes in Cellular Plastics during Combustion.

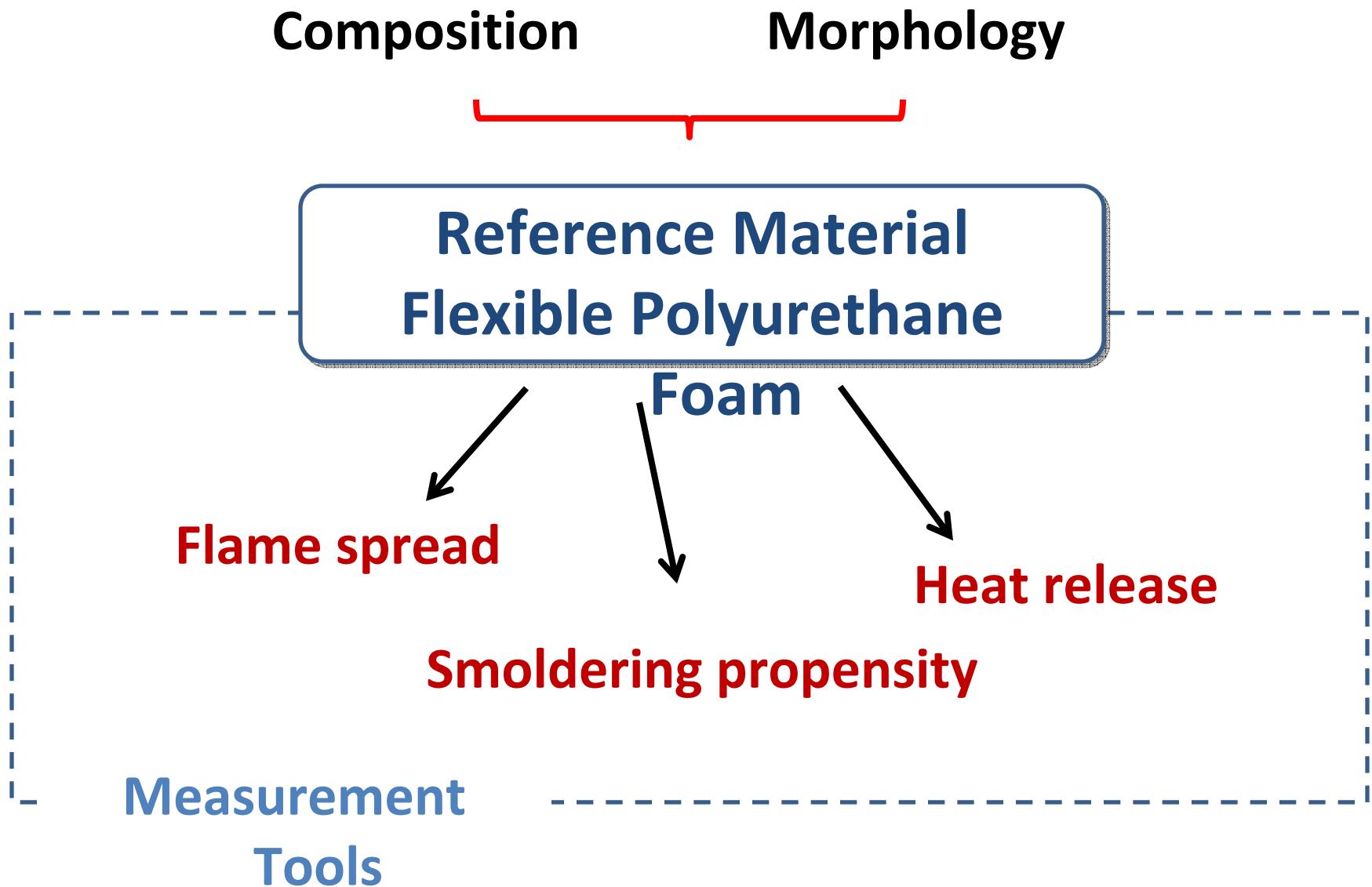
The Sixth Triennial International Aircraft Fire and Cabin Safety Research Conference, October 25-28, 2010, Atlantic City

Roland H. Krämer, Szabolcs Matko, Jeffrey W. Gilman



**National Institute of
Standards and Technology**
Fire Research Division
100 Bureau Drive
Gaithersburg-MD 20899

BACKGROUND: Feasibility study



Potential areas of application:

- Testing of smoldering propensity of furniture fabrics.
- Verification of foam flammability tests on multiple scales.
- Soot production under controlled conditions.
- Verification of numerical models of foam combustion.

Problem: Variations in commercial foam properties

Burned residues in NIST Smolder Box.

Foam I



Foam II



Foam III



Specifications:

no flame retardant

density 1.8 lb ft^{-3}

IFD 25 - 30

air flow $> 4 \text{ ft}^3 \text{ min}^{-1}$

10 cm

Challenges: Complexity of foam formulations

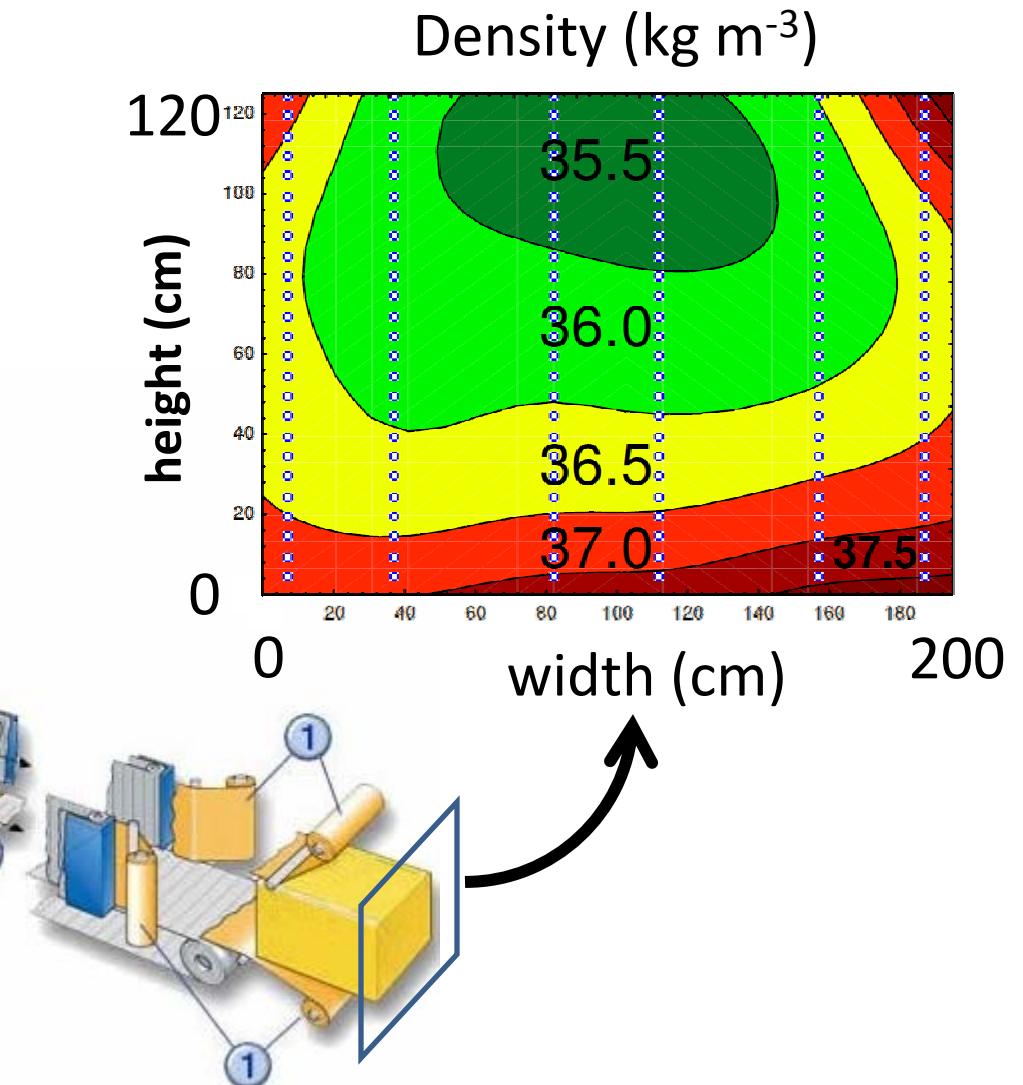
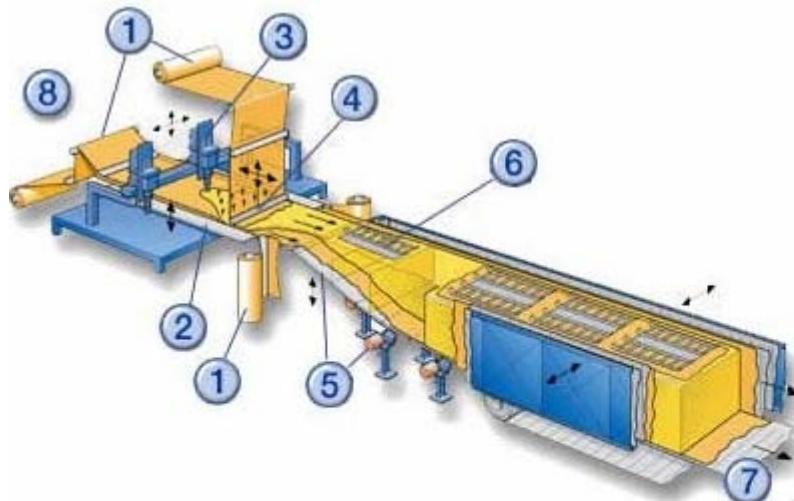
Component	Parts	mass.%
Polyether polyol ($M_w \sim 3000$, trifunctional)	100	58.8
Deionized Water	3.8	2.2
Auxiliary Blowing Agent	2.6	1.5
Amine Catalyst (blowing catalyst)	0.2	0.12
Tin Catalyst (curing and blowing)	0.23	0.14
Silicon Surfactant	1	0.59
Toluene Diisocyanate (TDI)	51.52	30.3
(Flame Retardant, optional)	10.6	6.4

+ graft polymers

+ additives (stabilizers, cell-openers...)

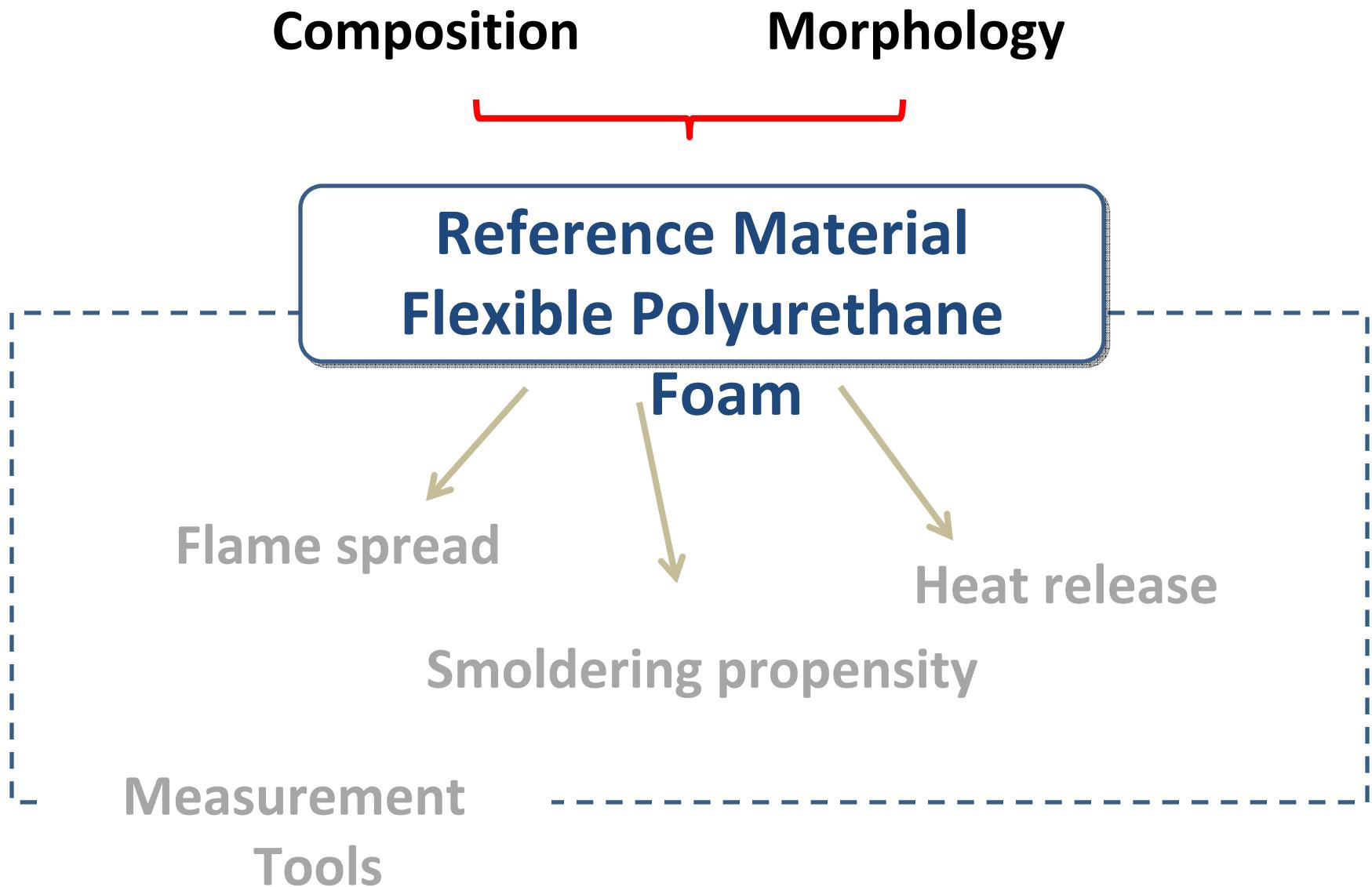
Challenges: Variability in foam quality in production

Foam production line:

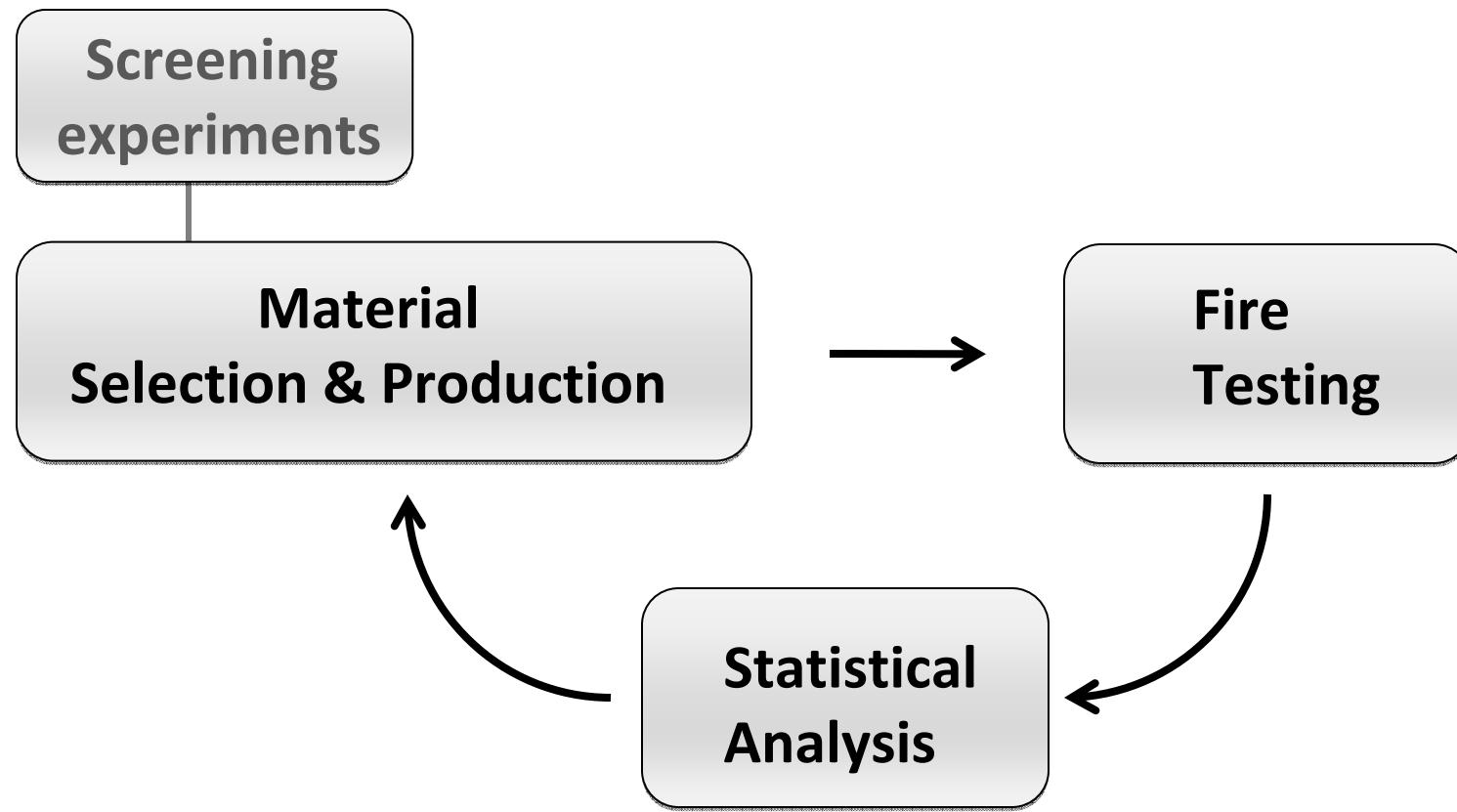


Source: Huntsman Polyurethanes, www.huntsman.com/pu/Media/2008_Utech_presentation.pdf

BACKGROUND: Feasibility study

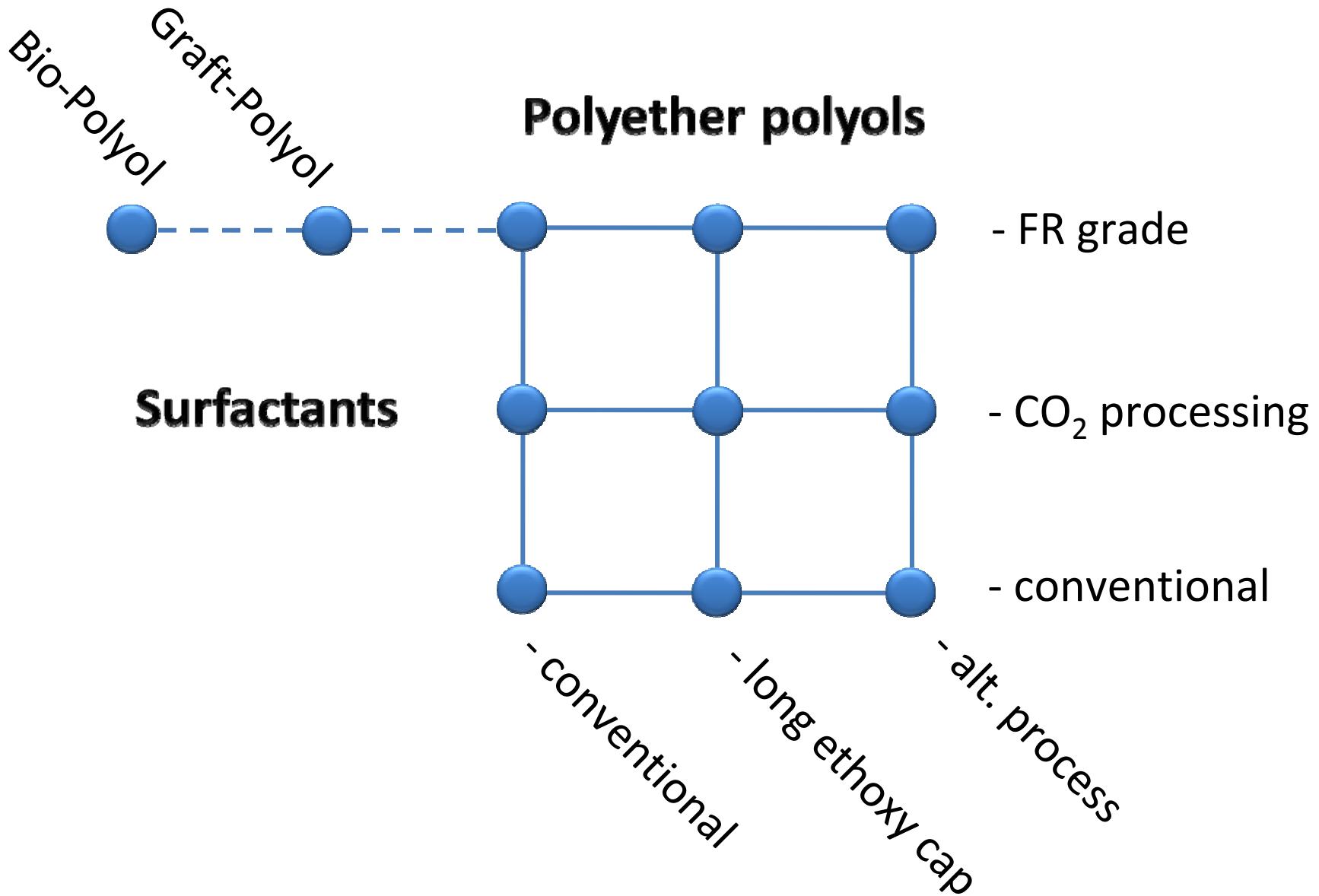


Experimental design with 3 iterations

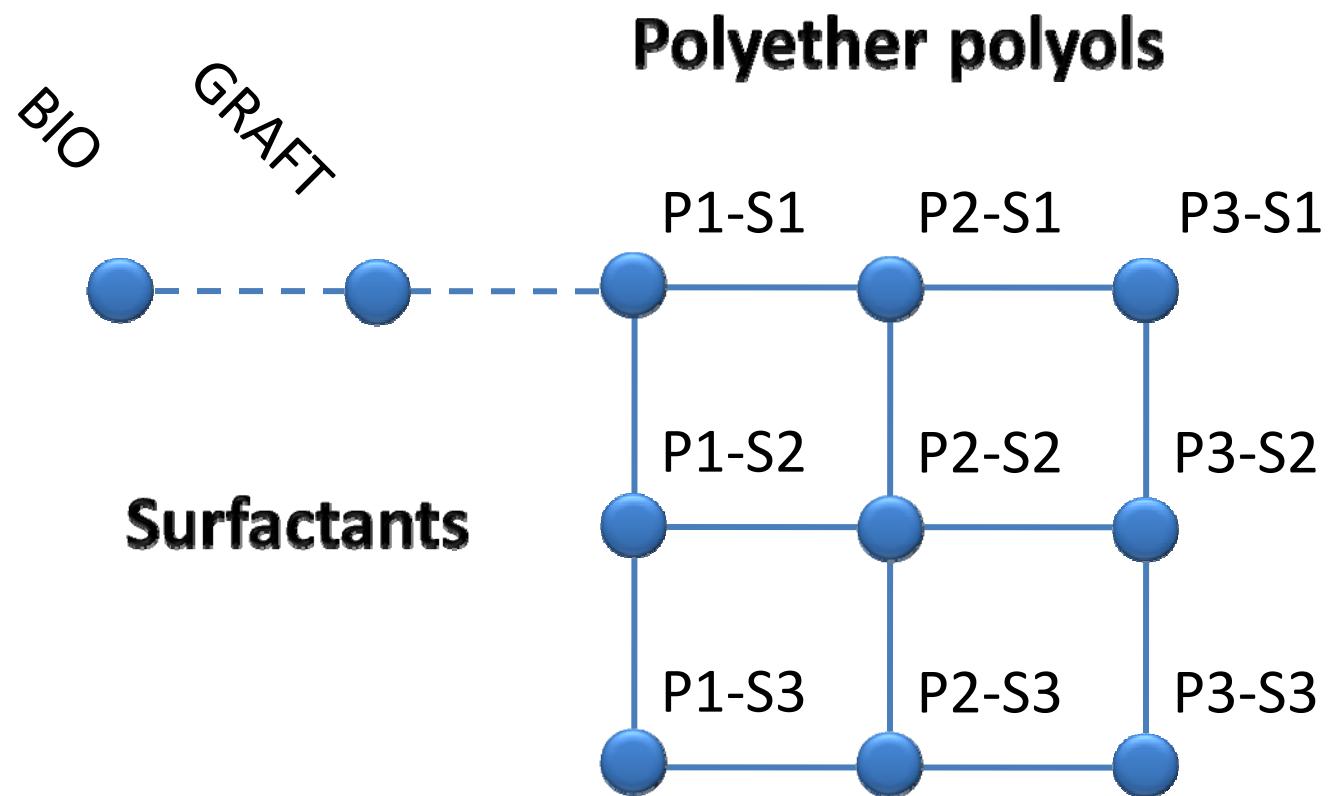


- | | |
|---------------------------------------|---------------------------|
| I Chemical composition | raw materials, impurities |
| II Morphology | air flow, density, ... |
| III Scale-Up & Correlation | (selection) |

1st Iteration: Chemical Composition

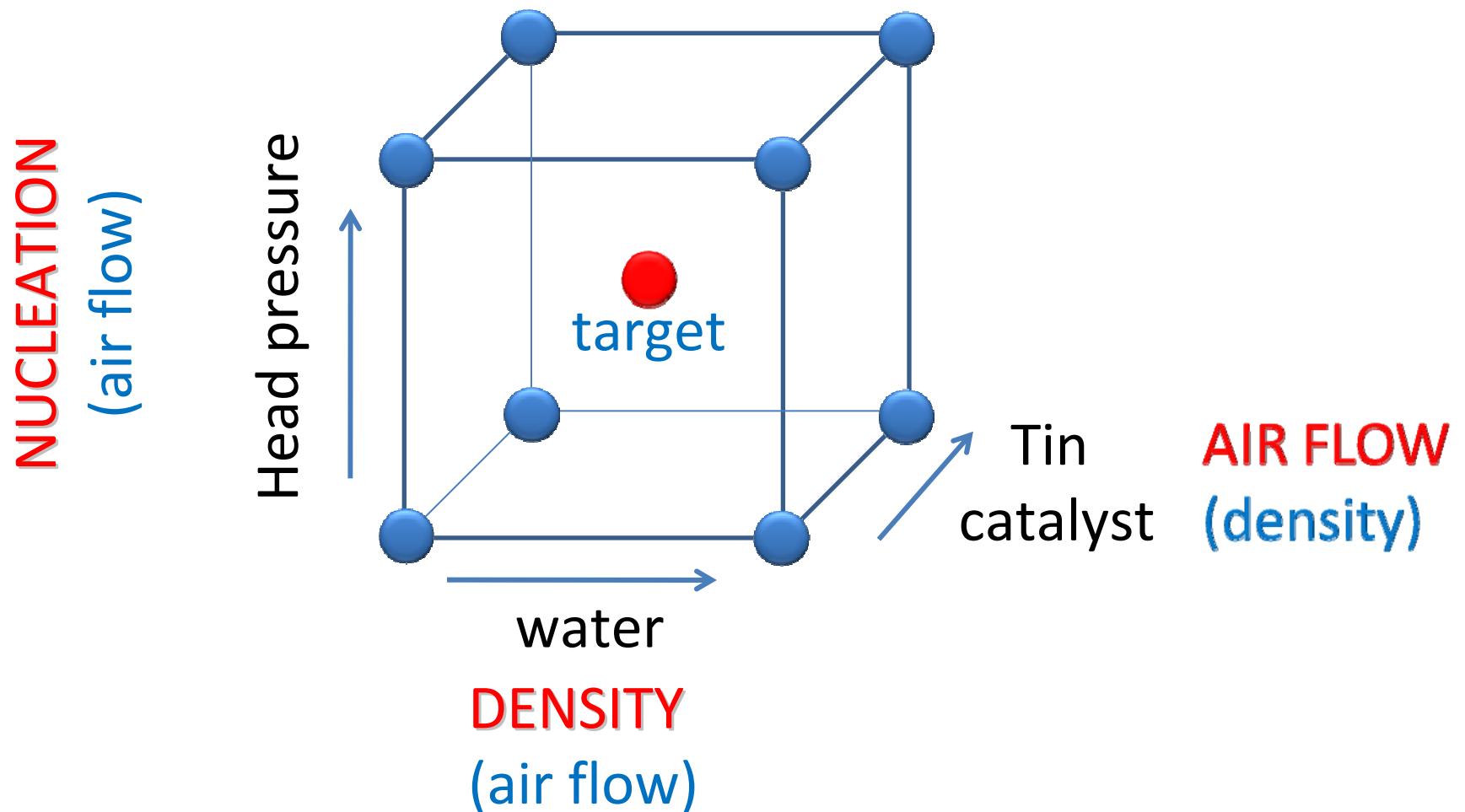


1st Iteration: Chemical Composition

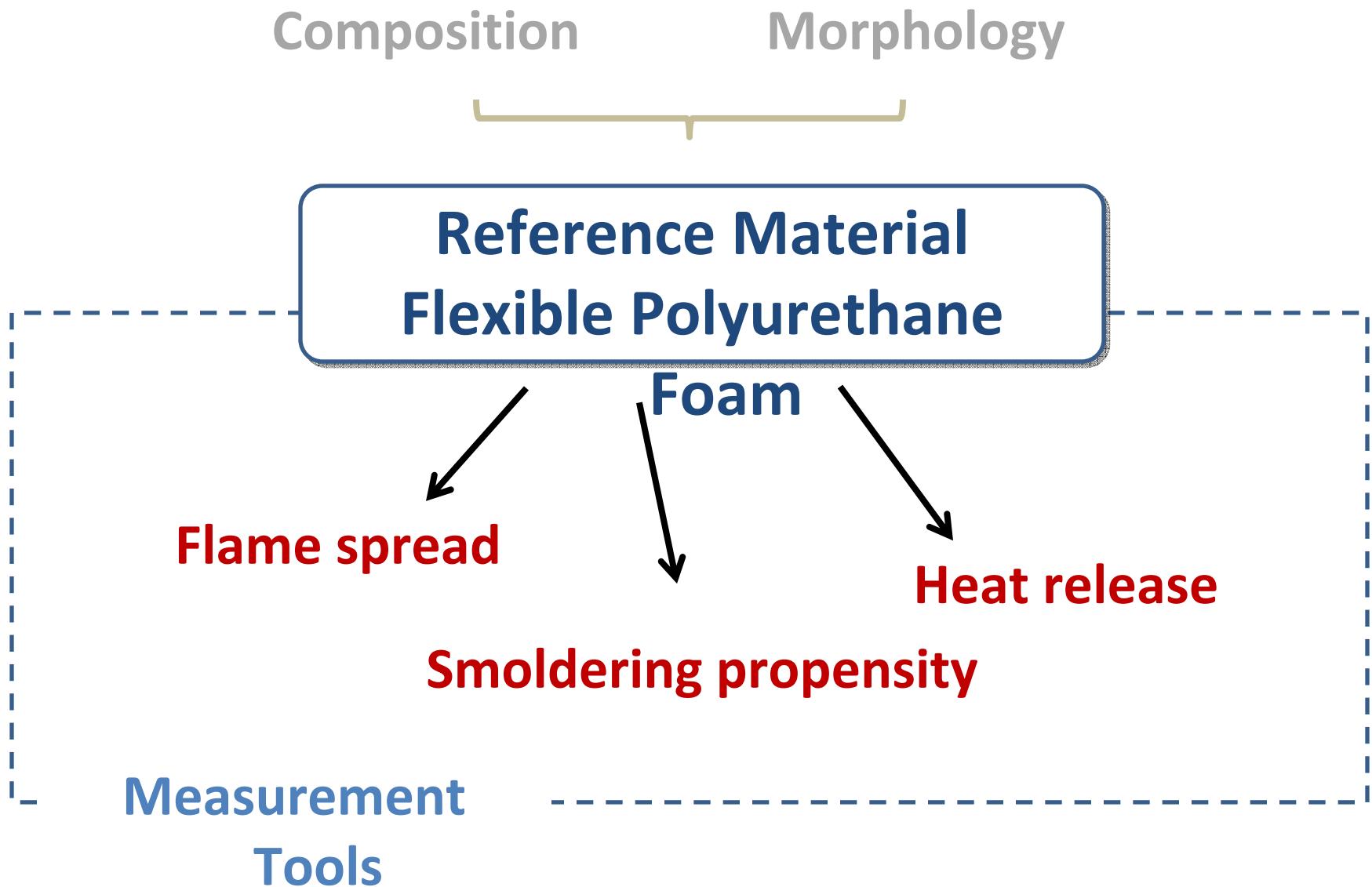


2nd Iteration:

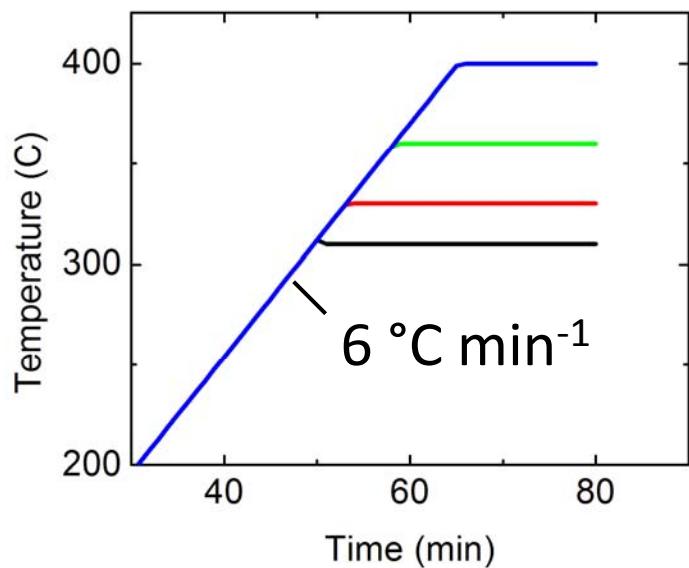
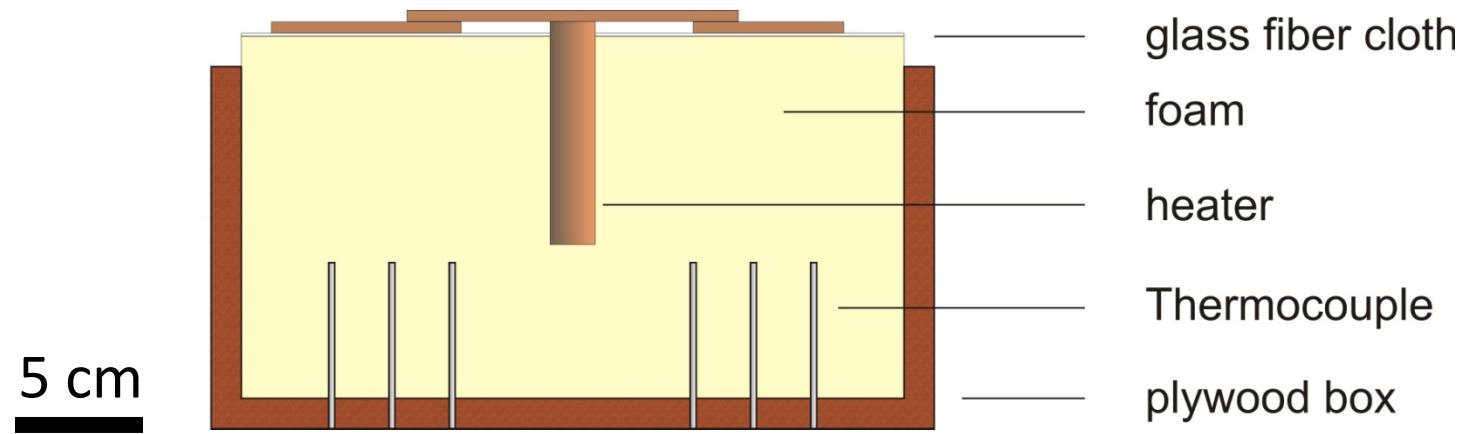
Morphology



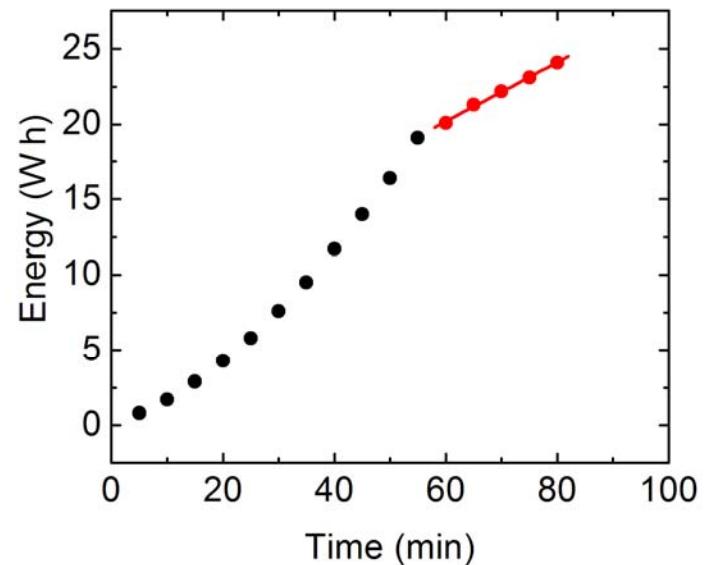
BACKGROUND: Feasibility study

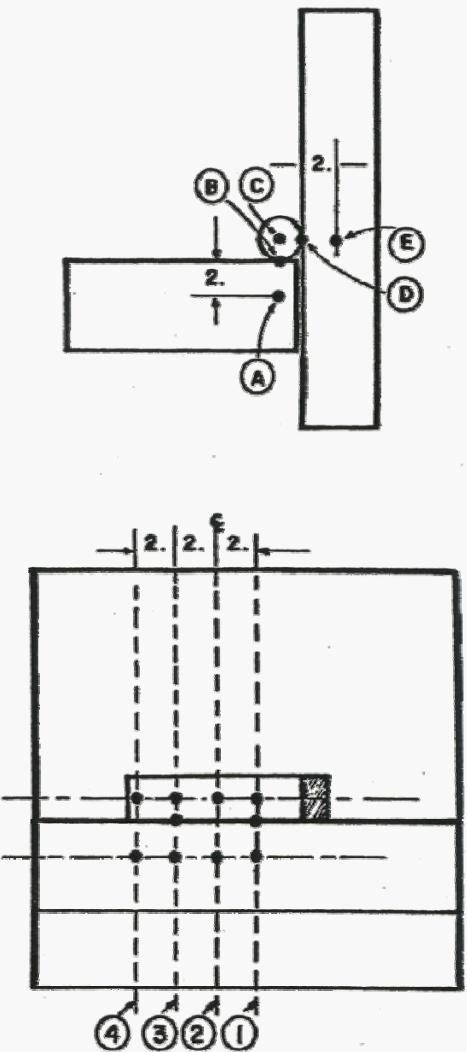


NIST Smolder Box

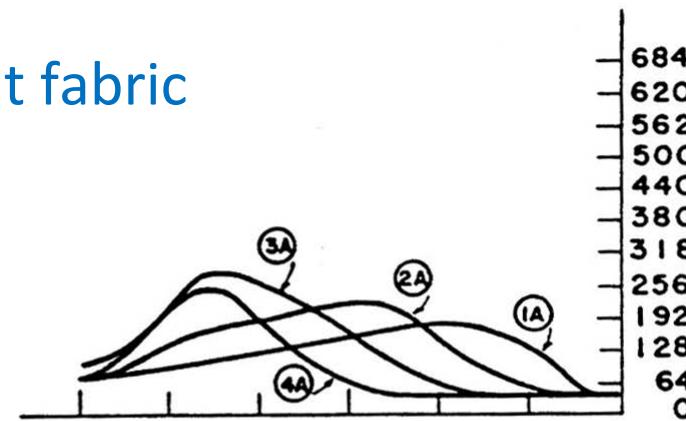


$\mathbf{T = 360\text{ }^{\circ}\text{C}}$
 $\mathbf{T = 340\text{ }^{\circ}\text{C}}$
 $\mathbf{T = 330\text{ }^{\circ}\text{C}}$
 $\mathbf{T = 320\text{ }^{\circ}\text{C}}$

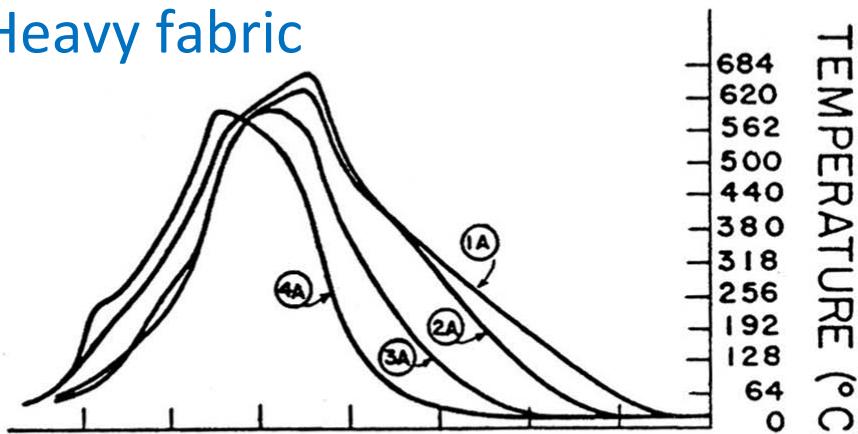




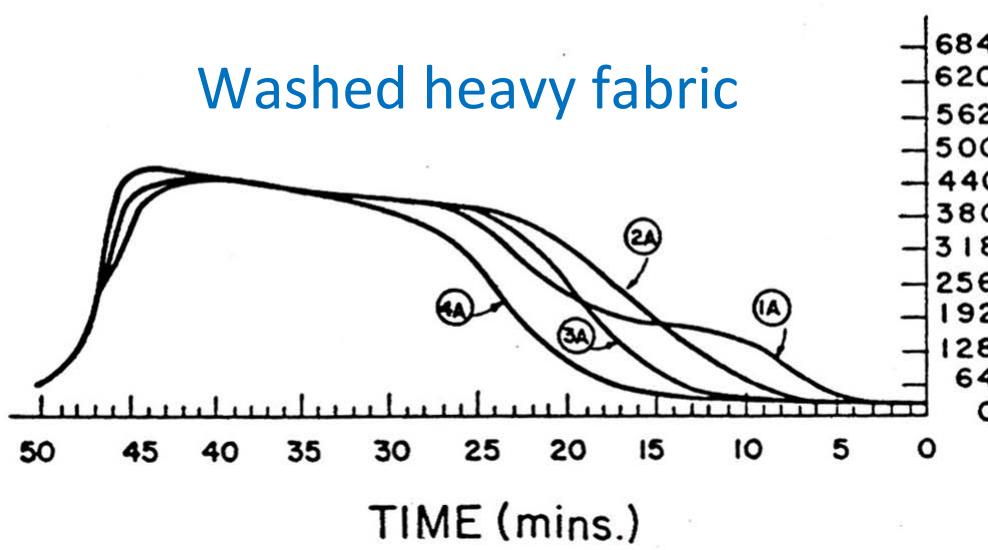
Light fabric



Heavy fabric



Washed heavy fabric



NIST Smolder Box

Test output:

- Temperature profile
- Mass loss and size of smolder zone
- Power supplied to the heater

Foam I

360 °C



— 5 cm

Foam II

360 °C

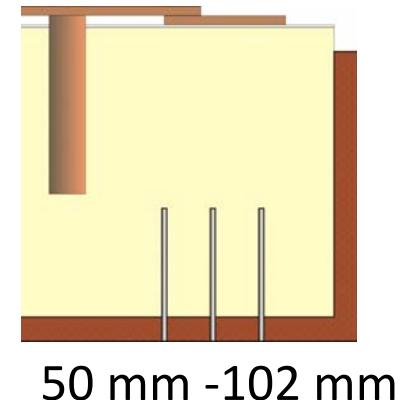


— 5 cm

NIST Smolder Box

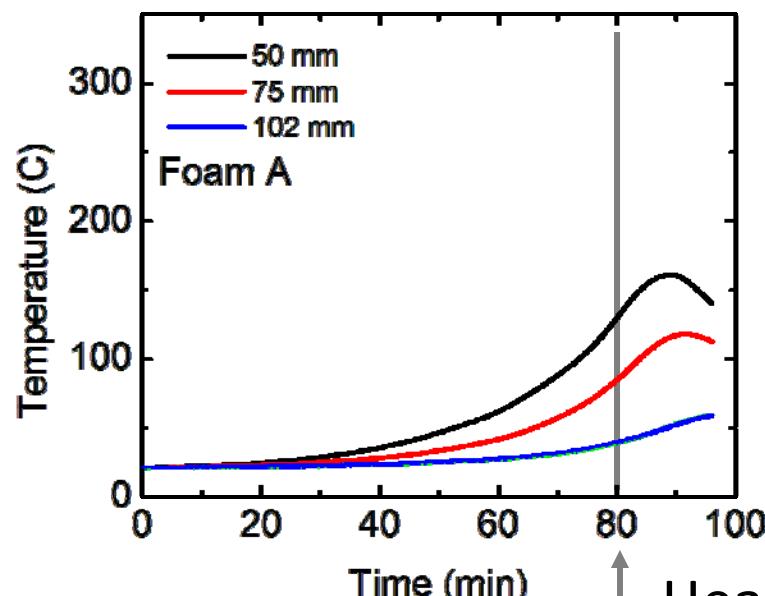
Test output:

- Temperature profile
- Mass loss
- Size of the smolder zone



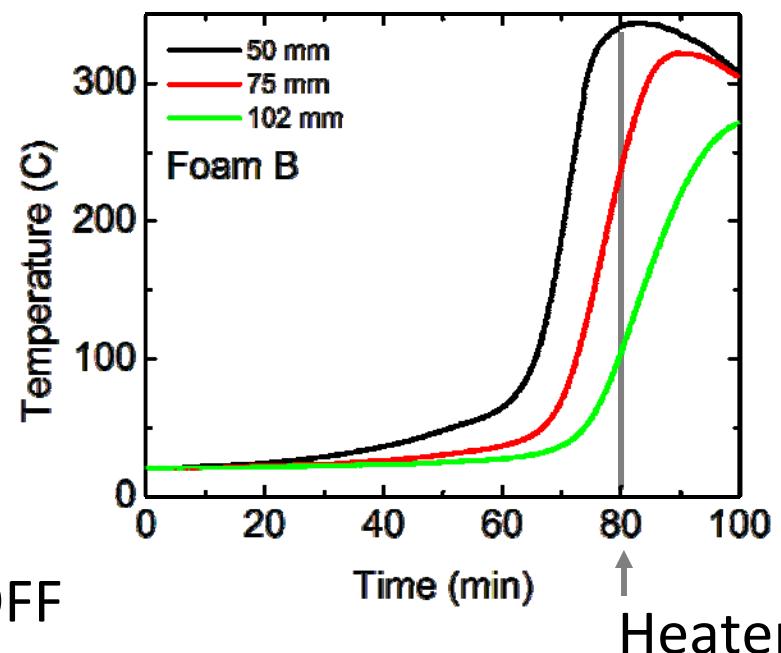
Foam I

360 °C



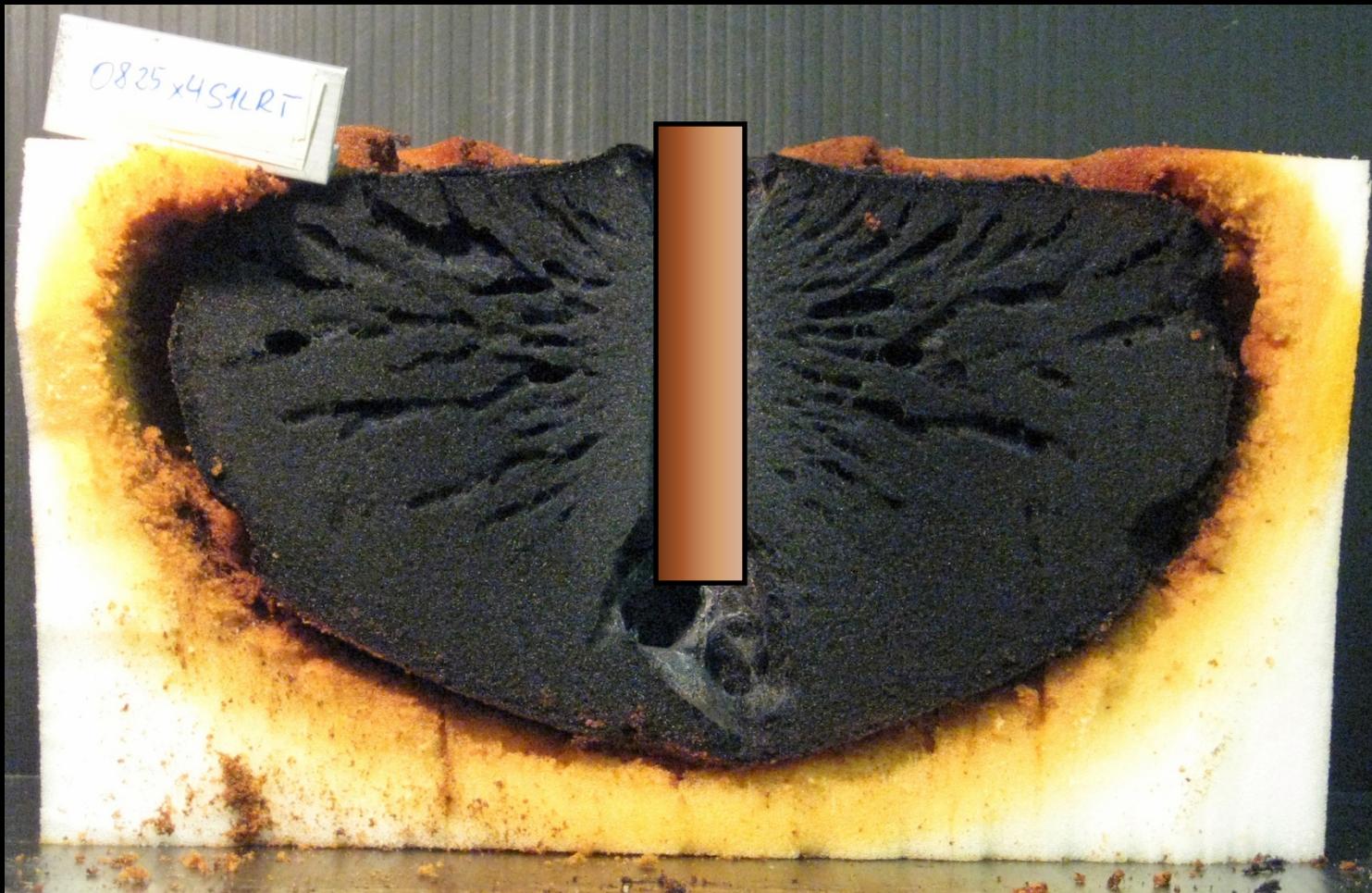
Foam II

360 °C



NIST Smolder Box – Sample residue

$T_{\text{heater}} = 340 \text{ }^{\circ}\text{C}$



— 5 cm

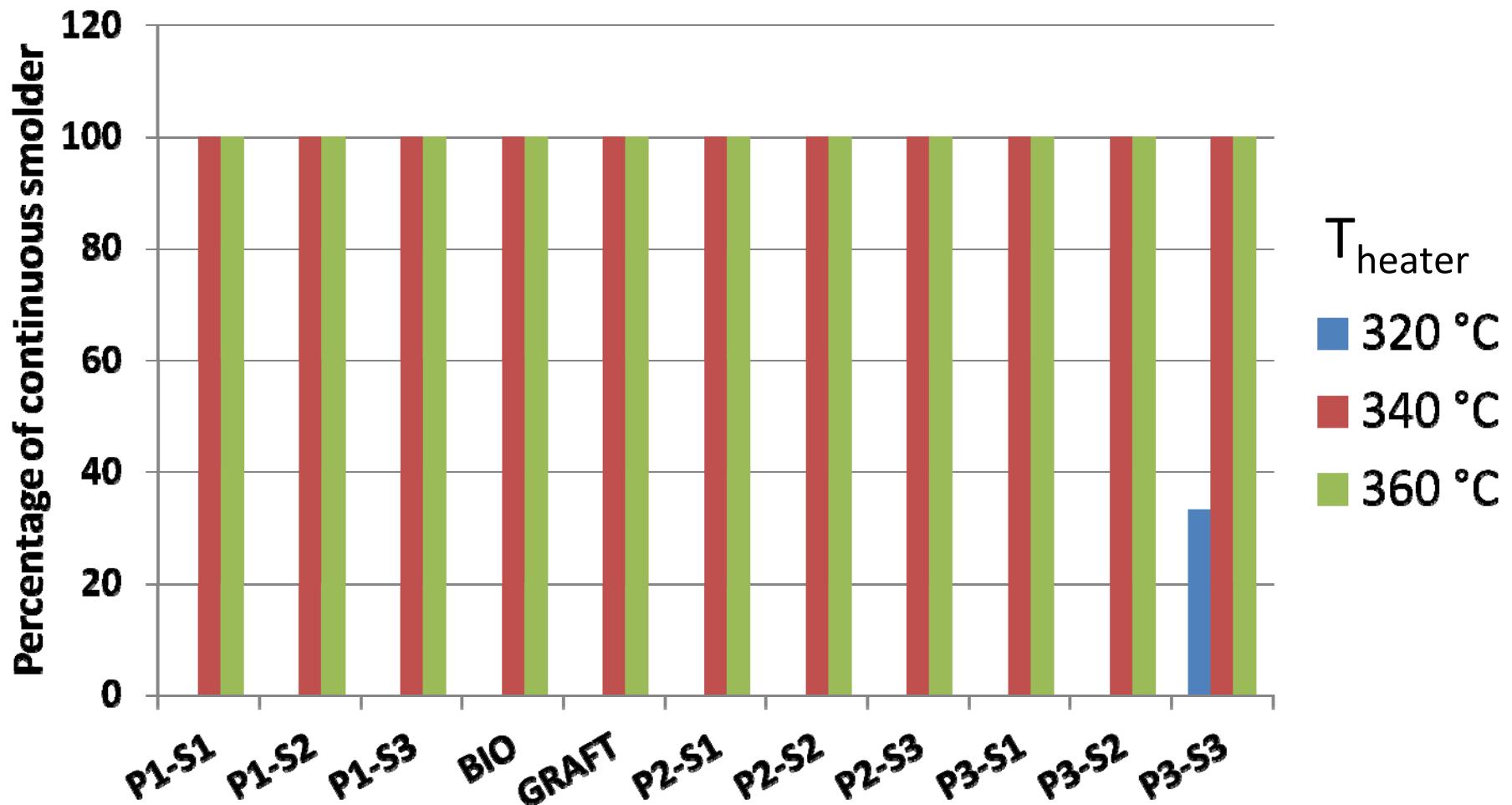
Variation of parameters and test results

$T_{heater} = 340 \text{ } ^\circ\text{C}$

Sample size: 20 runs

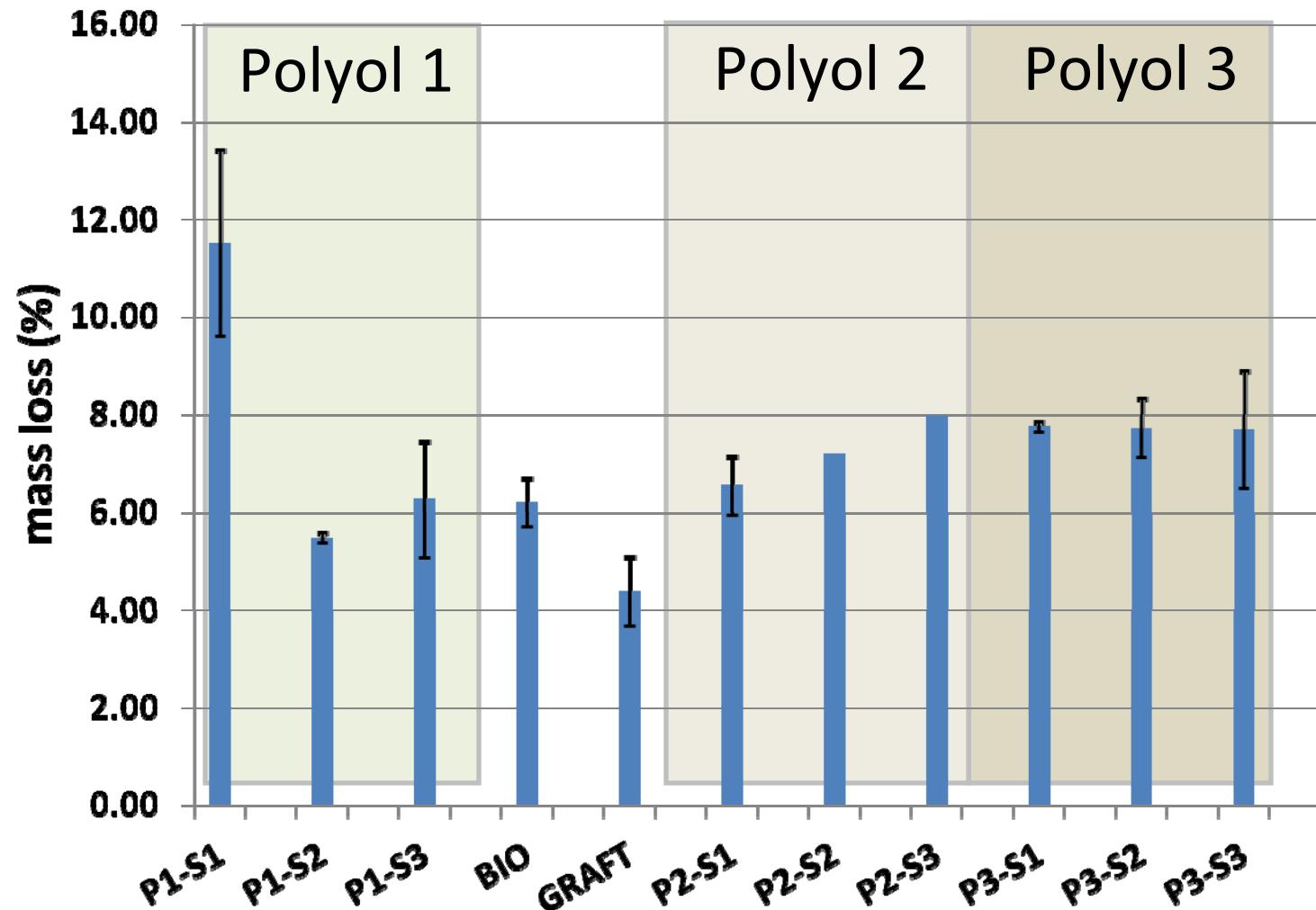
	Average	Same sample type deviation	Same sample type deviation %
Mass loss (%)	7.2	0.6	8 %
Temperature at 4 in distance ($^\circ\text{C}$)	179	24	13 %
Power to maintain Set point (W)	12.9	0.9	7 %
Energy supplied (W×h)	24.7	0.7	3 %
Heating rate ($^\circ\text{C min}^{-1}$)	5.7	0.1	2 %

Initiation of continuous smolder in box test



Smolder Box Results

$T_{\text{heater}} = 340 \text{ }^{\circ}\text{C}$

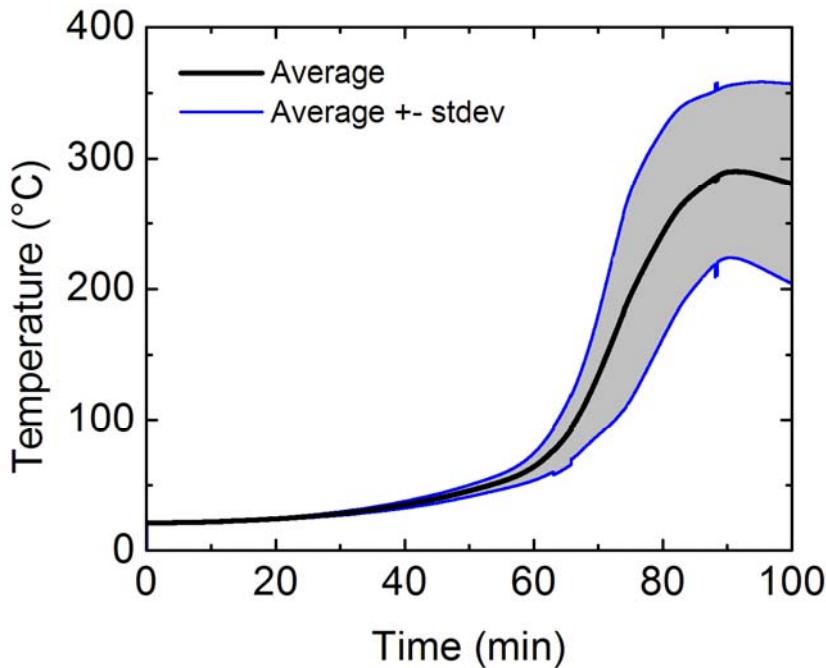


Variability of reference formulations $T_{\text{heater}} = 360 \text{ }^{\circ}\text{C}$

Commercial foams

Mass loss

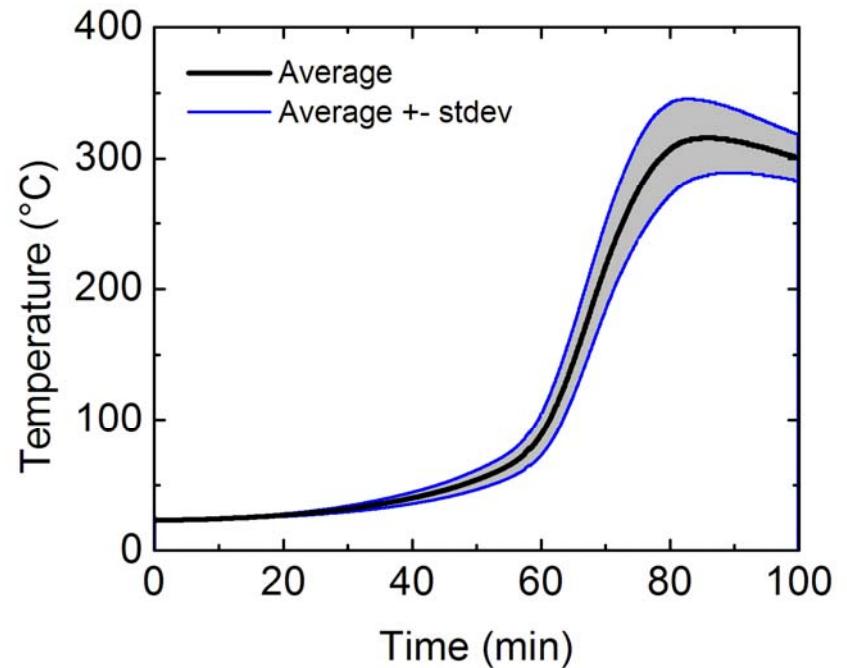
$9 \% \pm 7 \%$



SRM evaluation 3 surfactants x 3 polyols

Mass loss

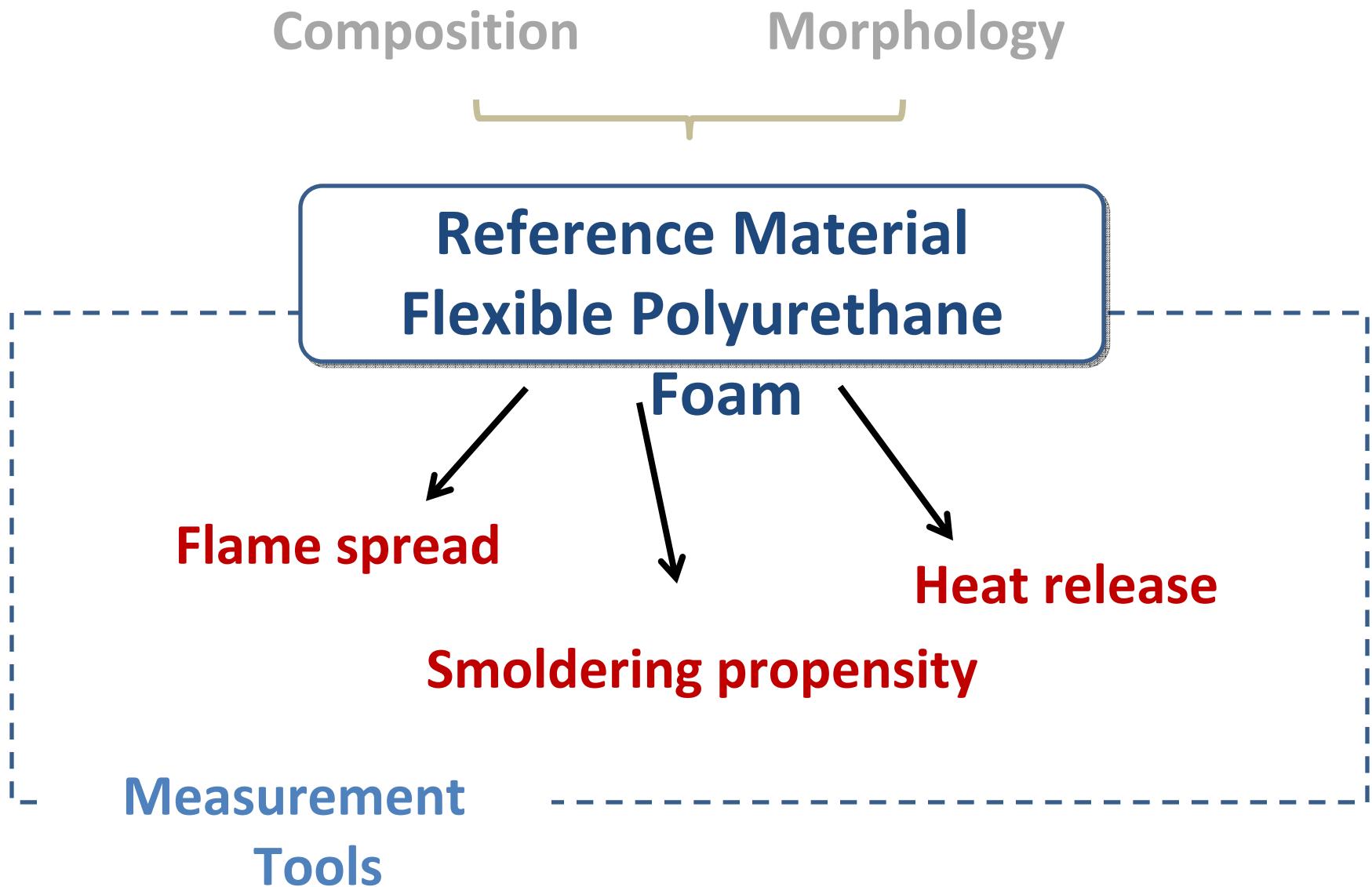
$8 \% \pm 2 \%$



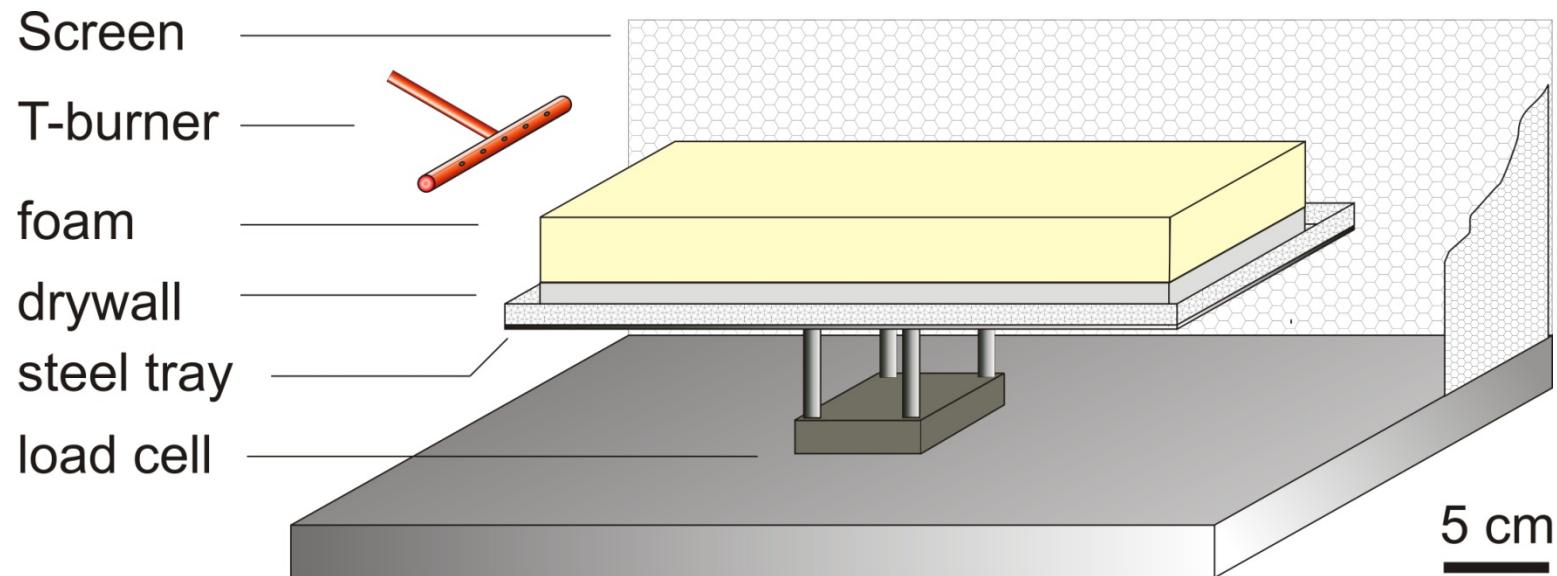
Effect of chemical composition on smoldering propensity

- The smolder box test method was continuously improved and showed a satisfactory reproducibility of results.
- An acceptable foam quality and level of control over known nuisance parameters was achieved using a pilot foam production line.
- The variability of the smolder box test results of the custom-made samples was significantly lower than that of commercial samples.
- The nature of the polyether polyols and silicone surfactants chosen for this sample set did not significantly affect the outcome of the smolder box test.

BACKGROUND: Feasibility study



Flame spread test

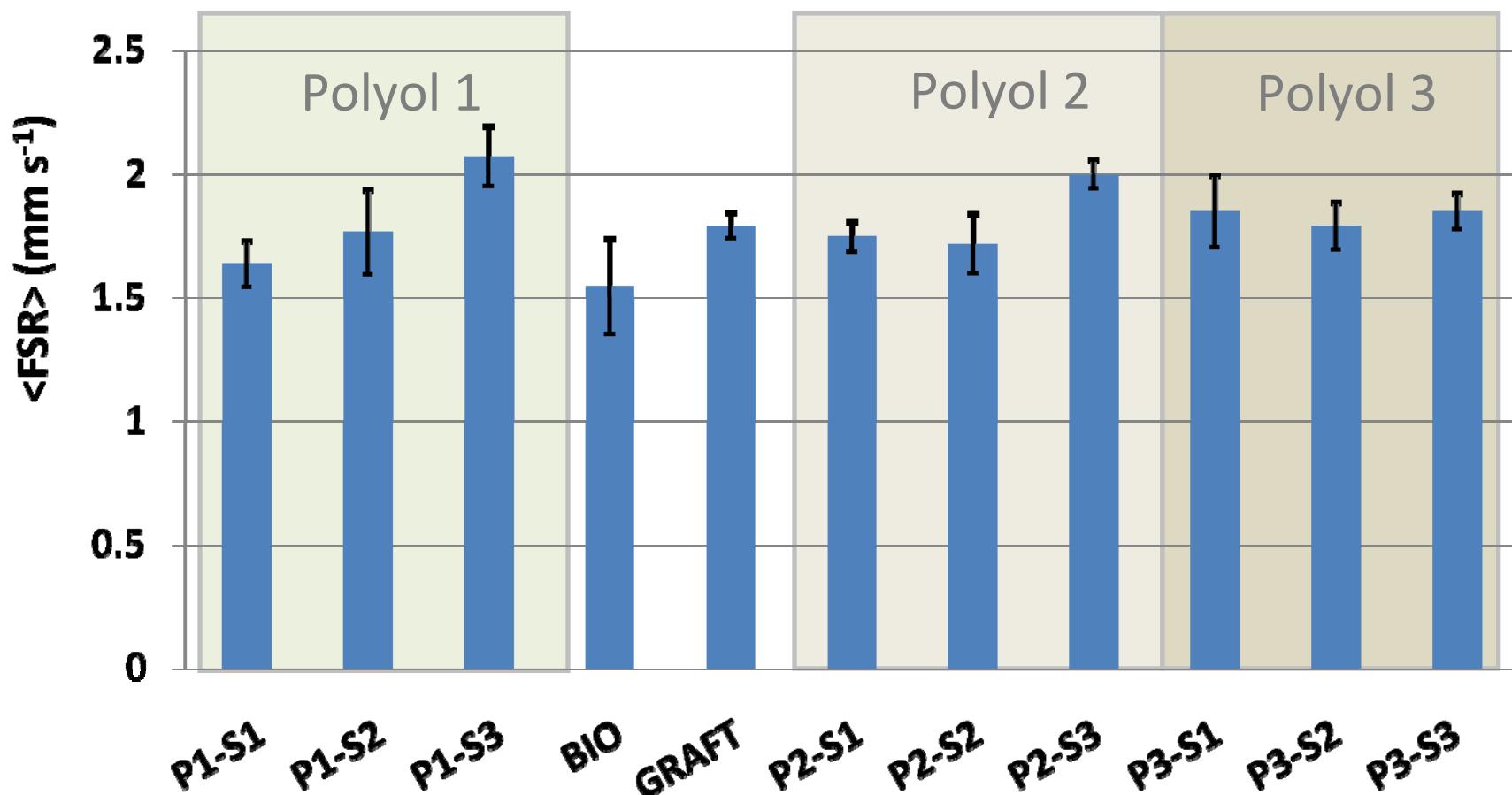


Sample size: 28 cm × 7.5 cm × 3 cm

Flame application: 20 s

Flame spread test

Flame spread rate

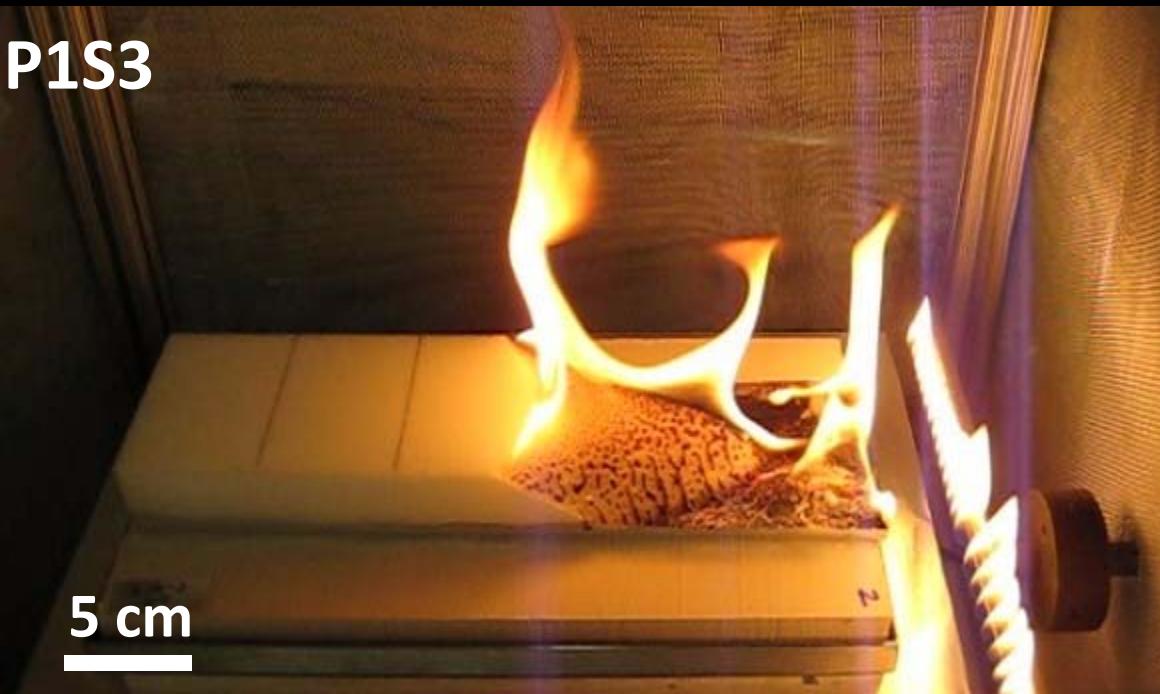


P1S2



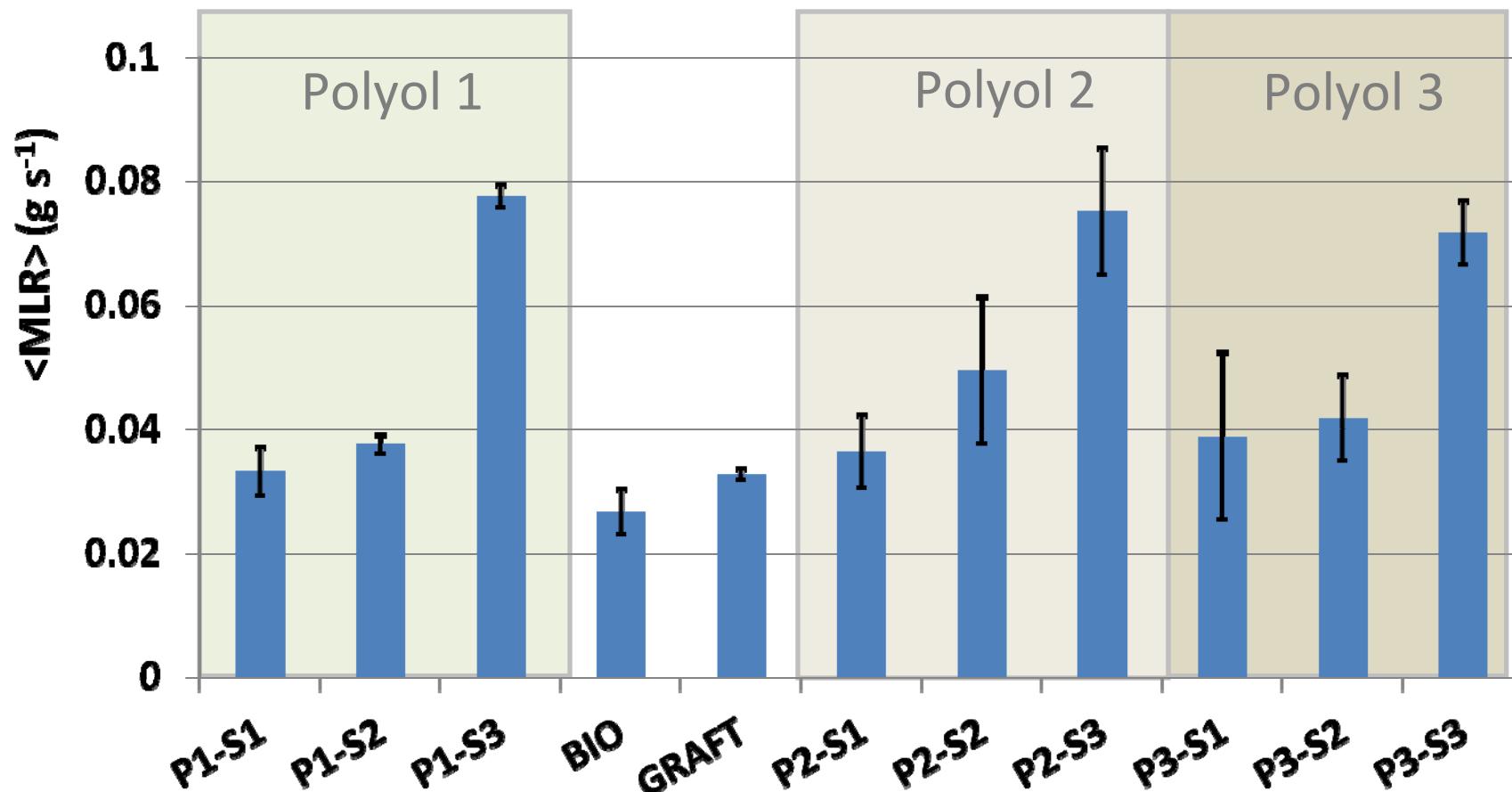
No or partial
pool fire

P1S3

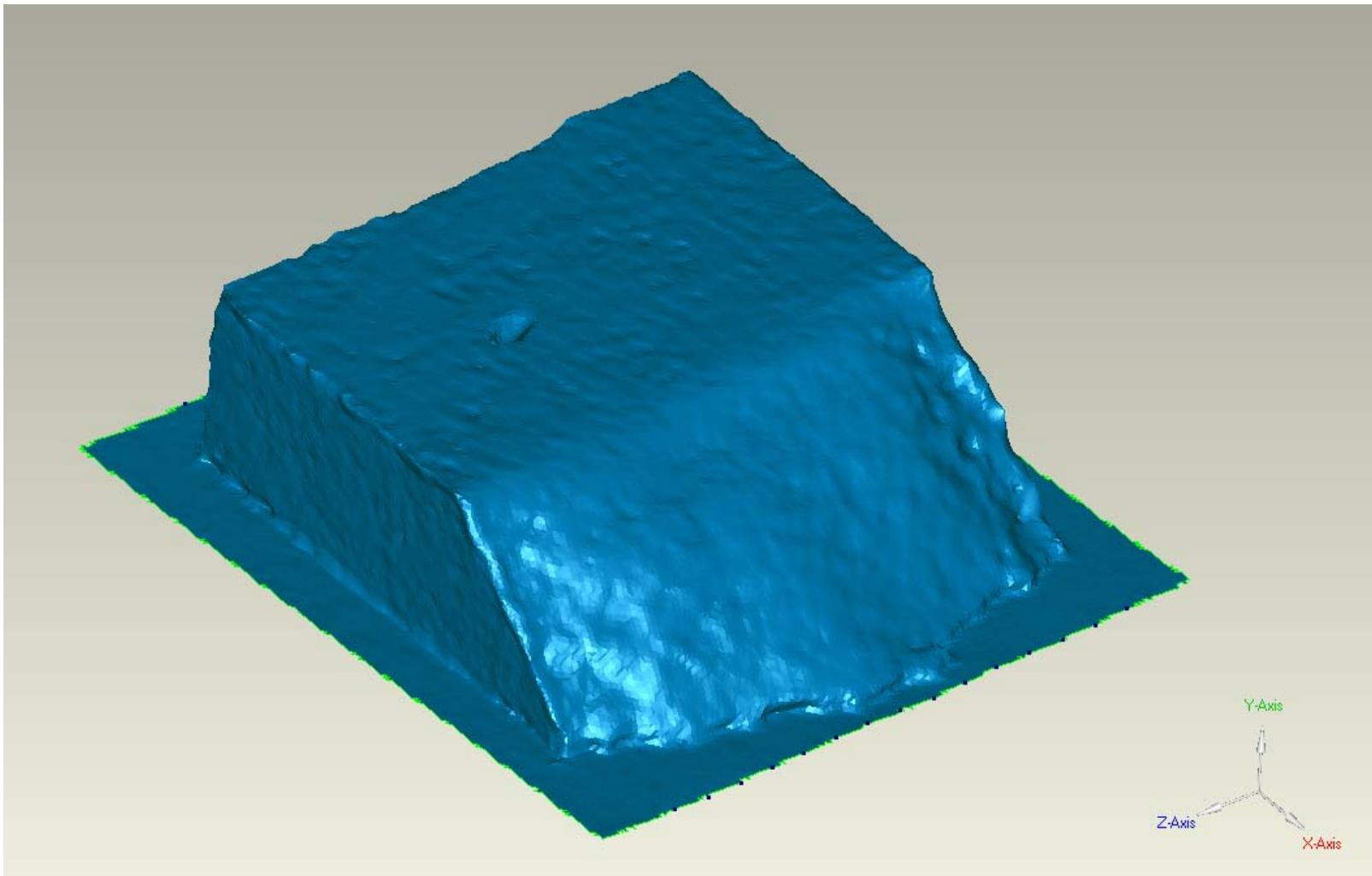


Pool fire
from the start

Mass loss rate during flame spread

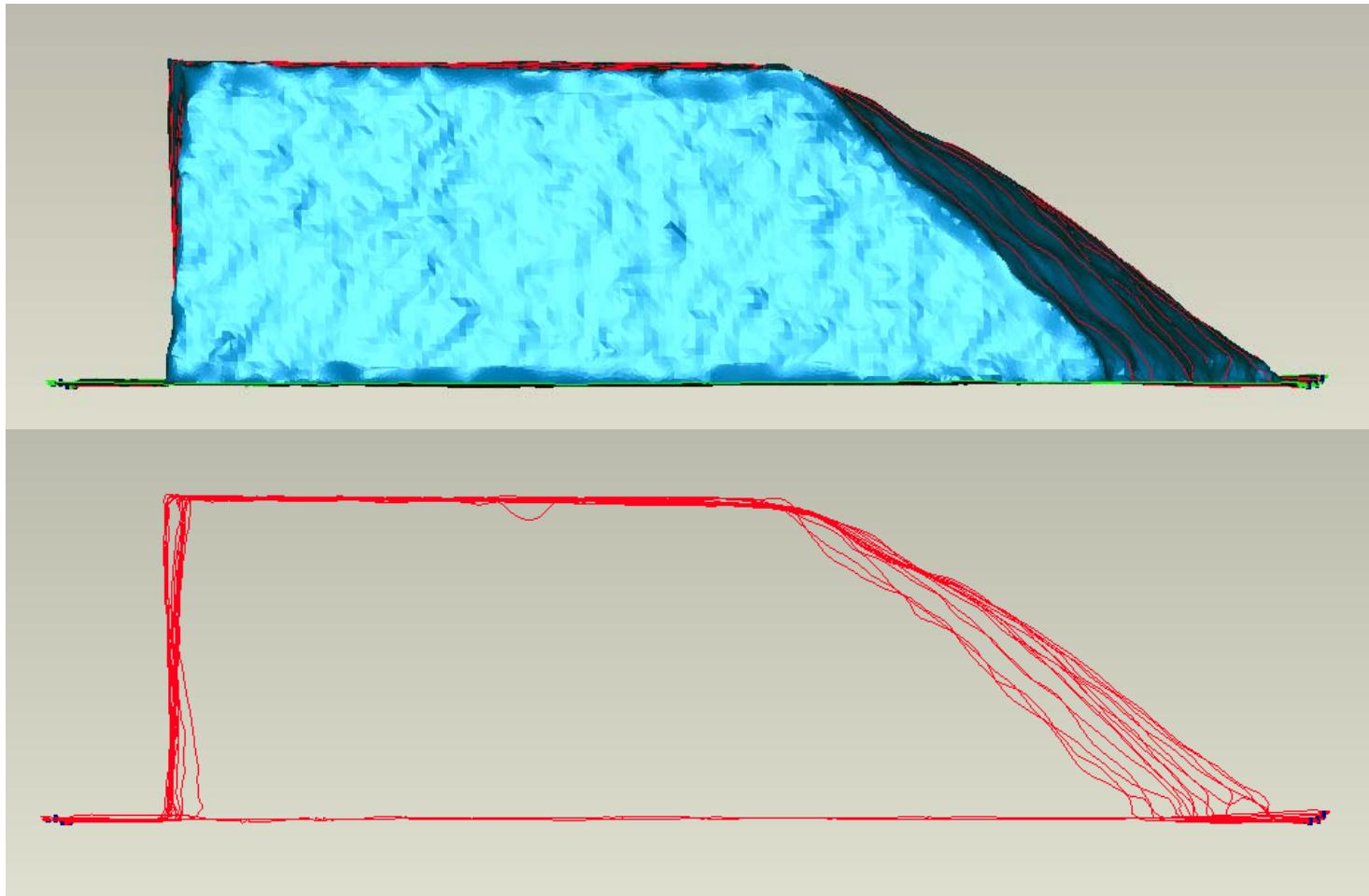


Flame spread test – Shape change of foam



2 cm

Flame spread test – Shape change of foam

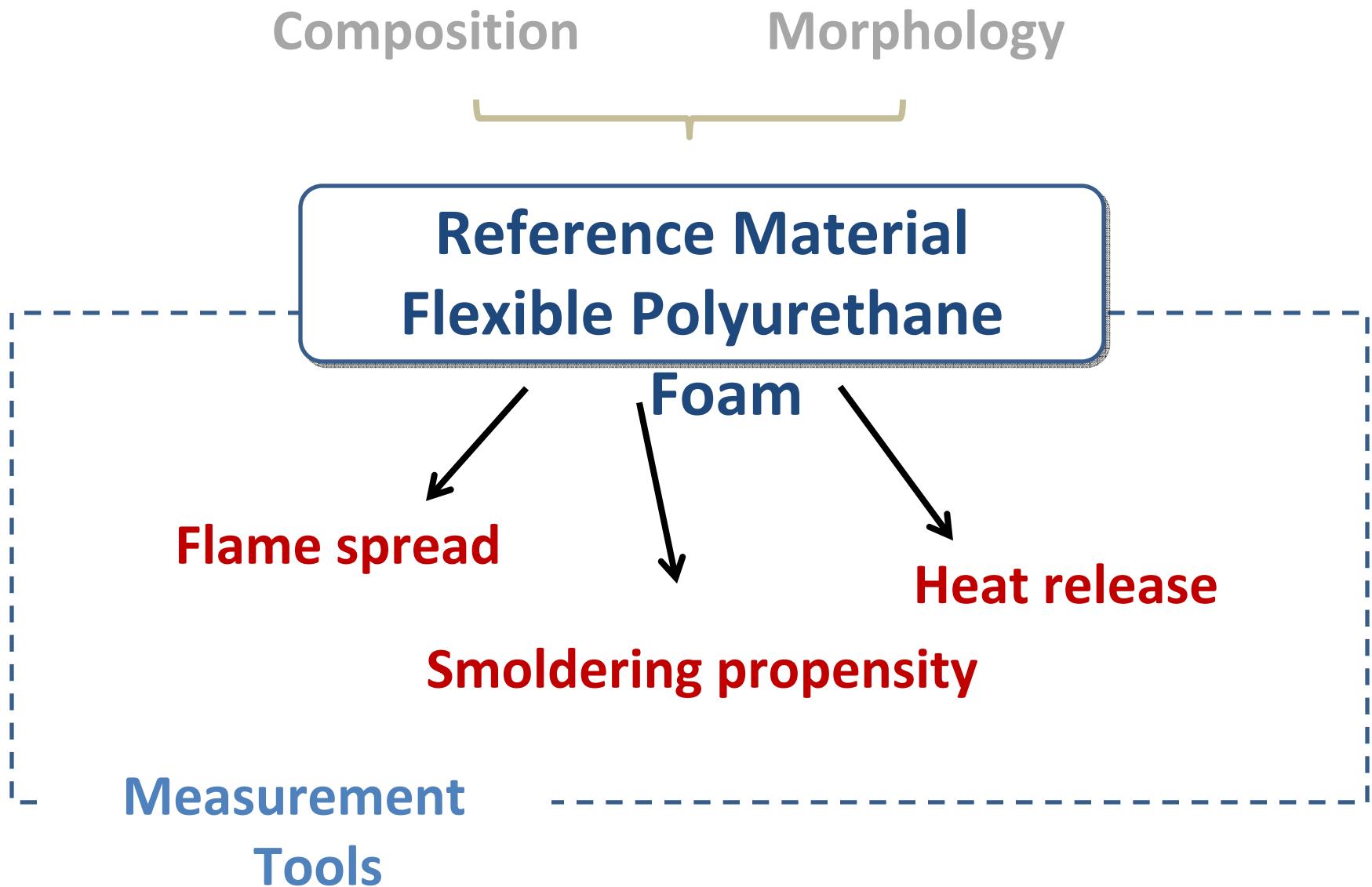


2 cm

Effect of chemical composition on flame spread behavior

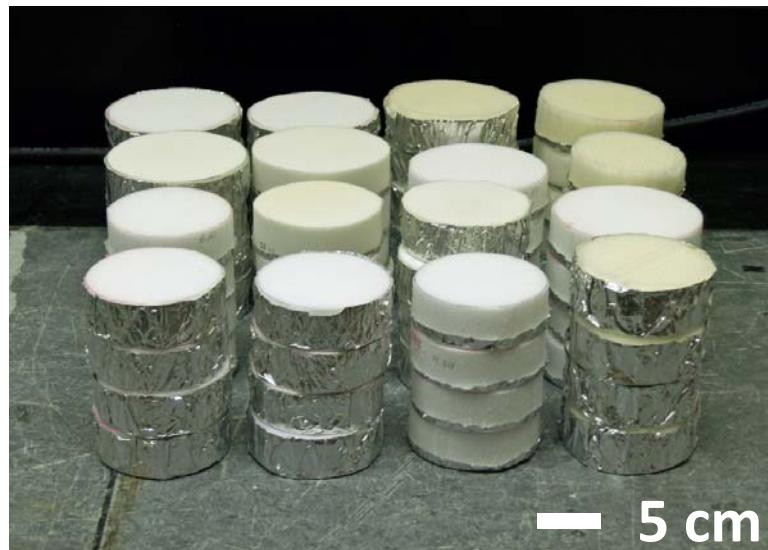
- The nature of the polyether polyols tested did not significantly affect the outcome of the flame spread test.
- The type of silicone surfactant had a strong impact on the burning rate of the pool of degraded material formed during the collapse of the foam following the initial flame spread over the sample surface.
- The flame spread rate in the given test configuration showed little variation for the foam formulations tested. The formation of pool fires led to a small increase in the flame spread rate.

BACKGROUND: Feasibility study



Cone calorimeter - Combinatorial Evaluation

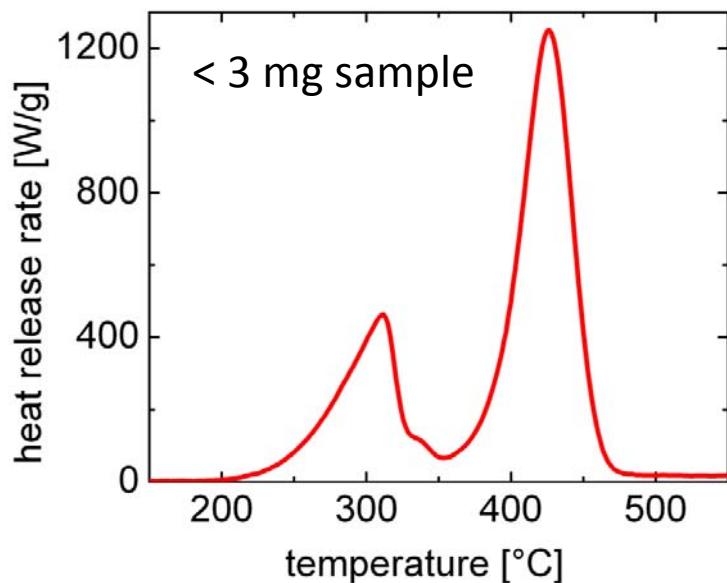
foam types – PUR-29, LDPE-29, LDPE-39, PA6-58
 2^3 full factorial experimental design



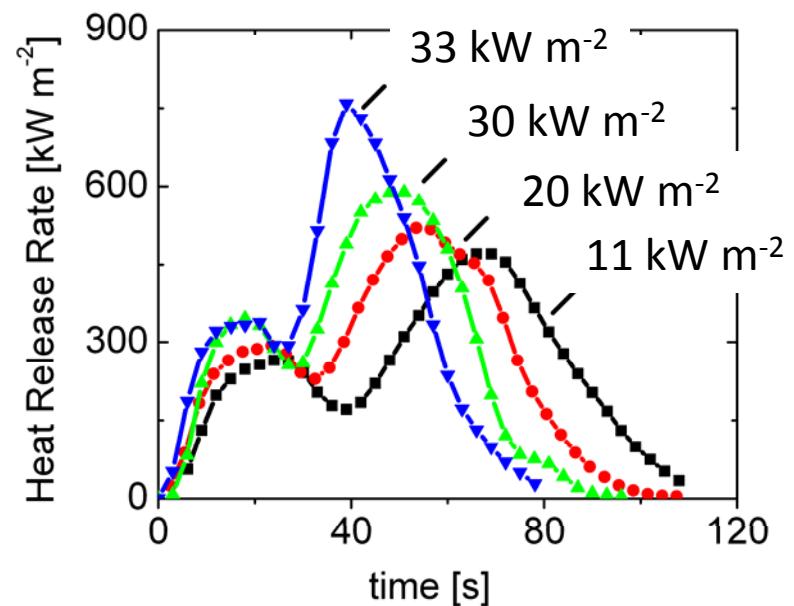
Diameter	86 mm	/	100 mm
Edge	5 mm	/	30 mm
Heat flux	10 kW m^{-2}	/	30 kW m^{-2}

Two-stage foam burning – example Polyurethane foam

Micro-Combustion Calorimeter



Cone Calorimeter

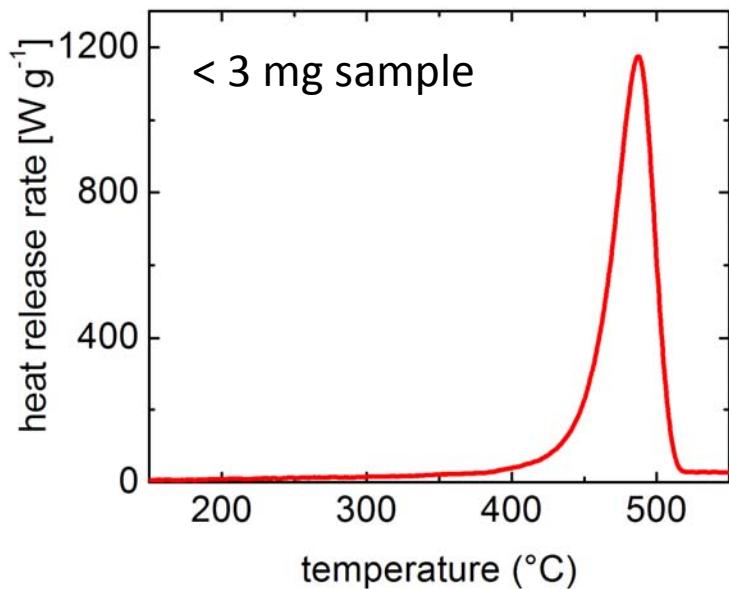


mm

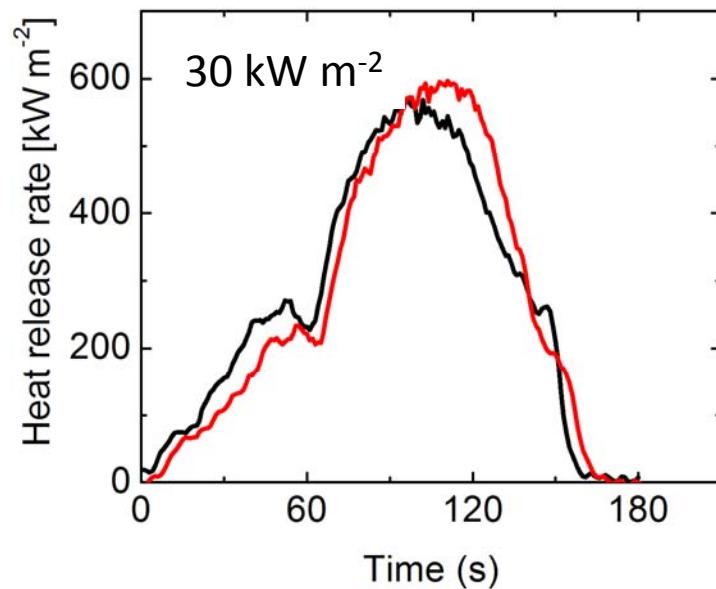
cm

Two-stage foam burning – example LDPE foam

Microcombustion calorimeter



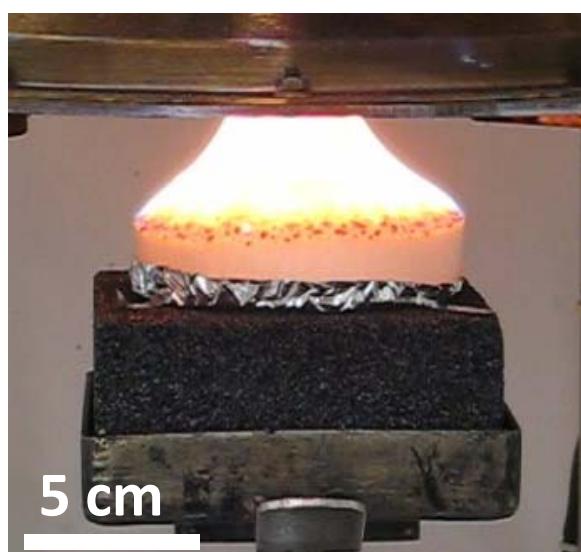
Cone calorimeter



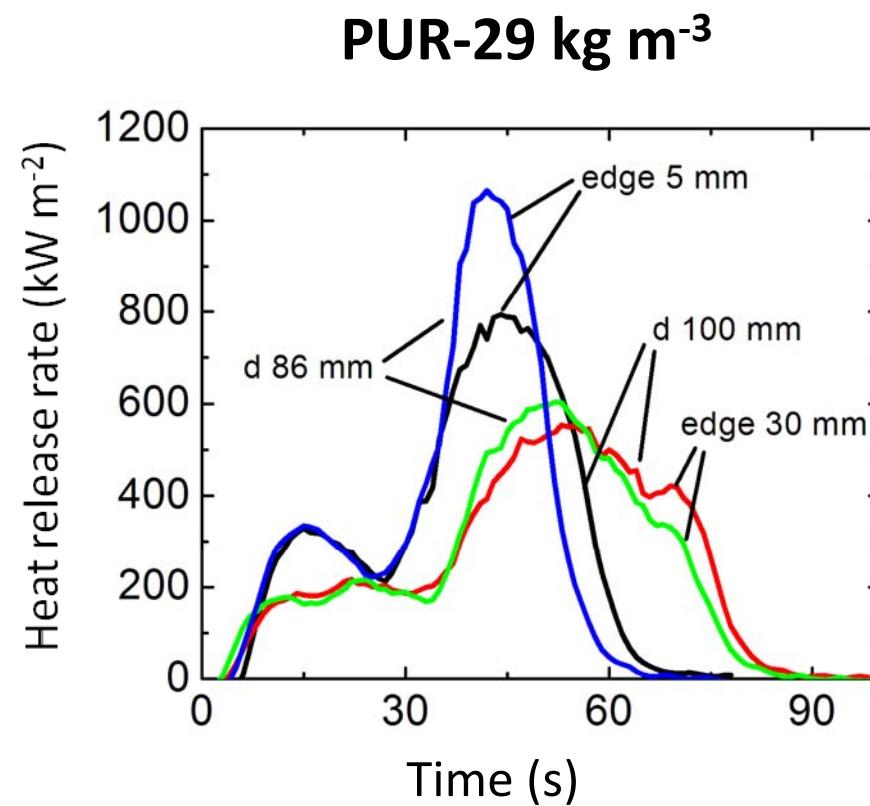
mm

cm

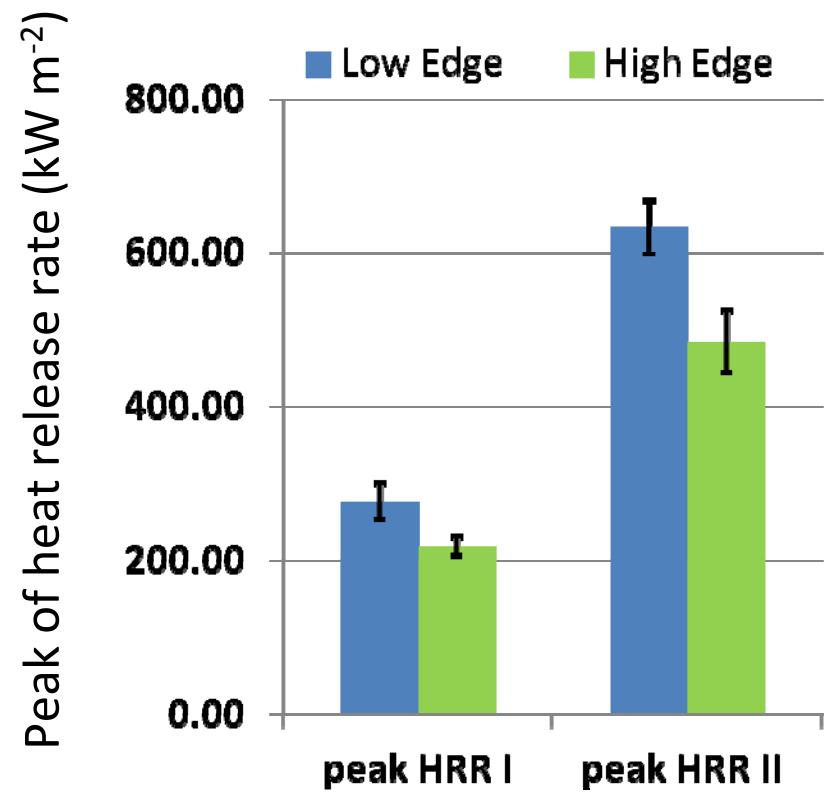
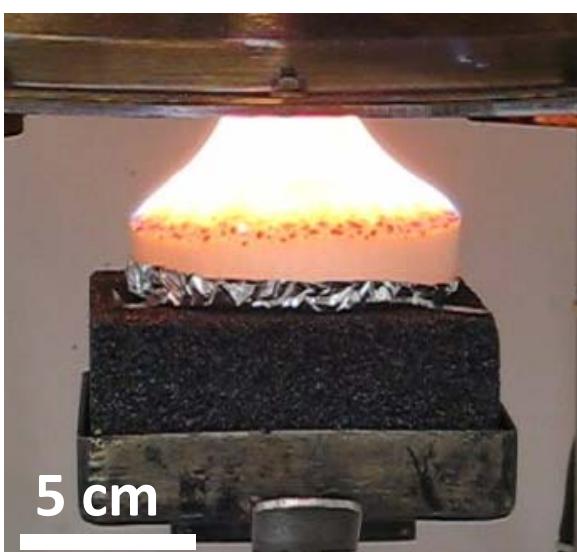
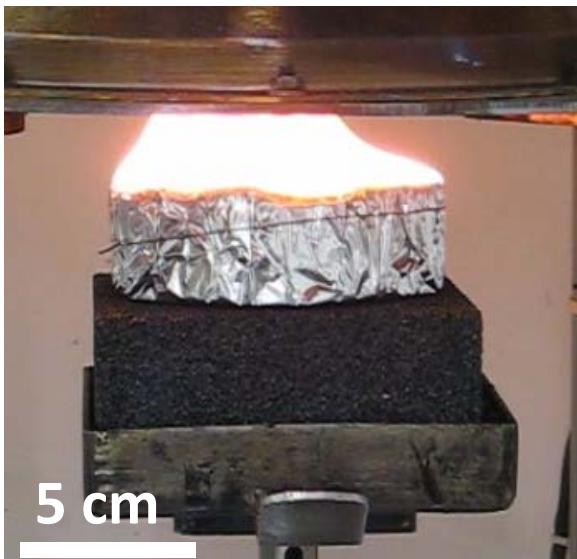
Effect of edge condition on burning rate



Incident heat flux 30 kW m^{-2}



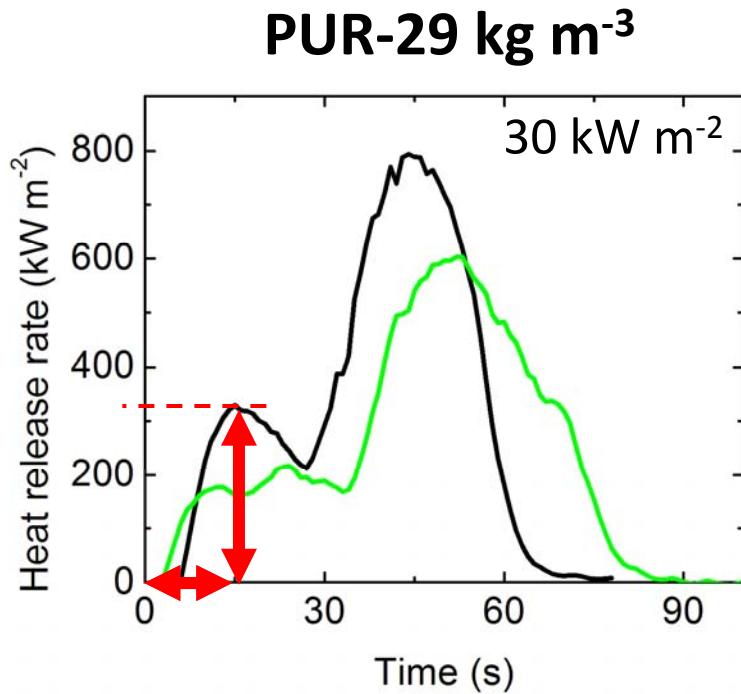
Effect of edge condition on burning rate



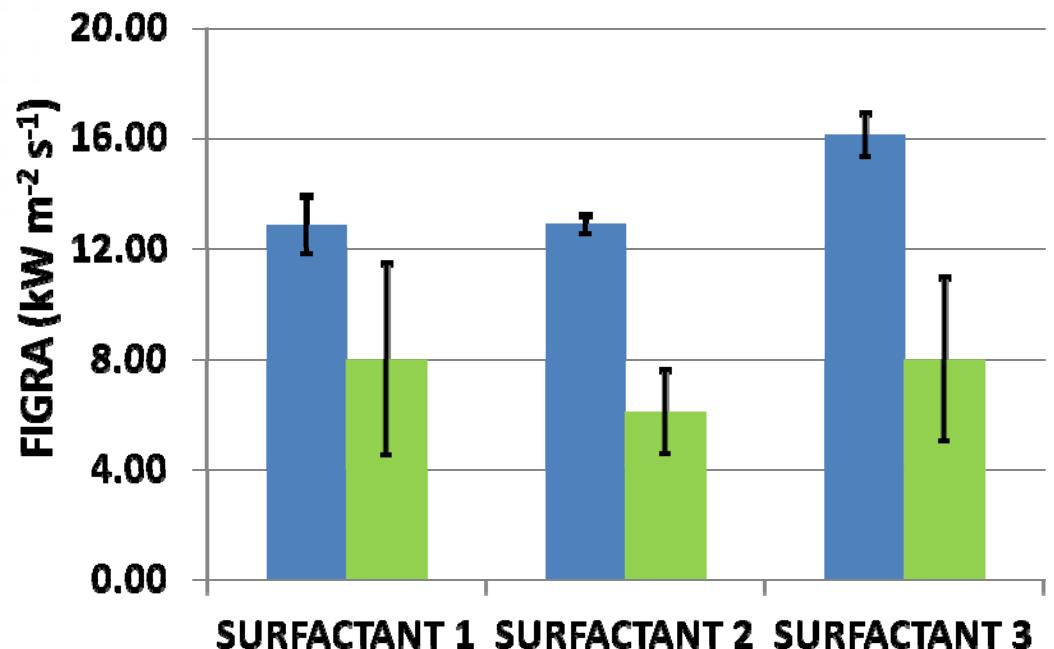
Incident heat flux: 30 kW m^{-2}
32 runs, 8 formulations

Sample to sample variation
Low edge $\pm 4\%$
High edge $\pm 10\%$

Effect of edge condition on test results

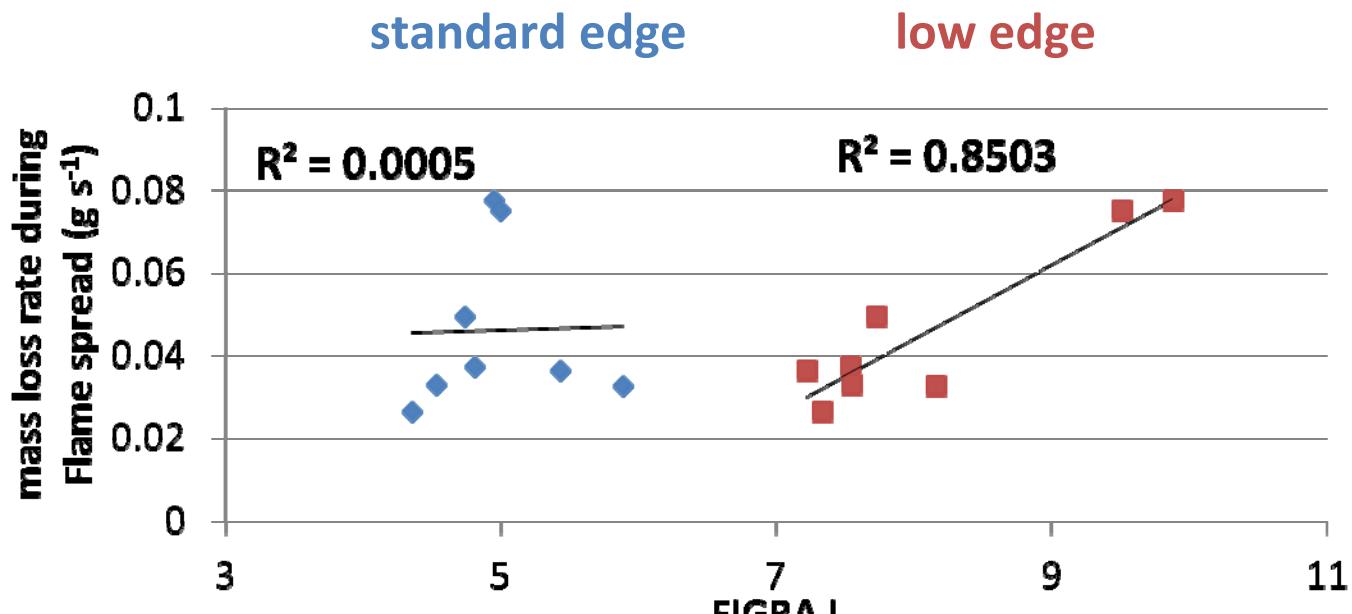


FIGRA = Peak of heat release rate
time to peak

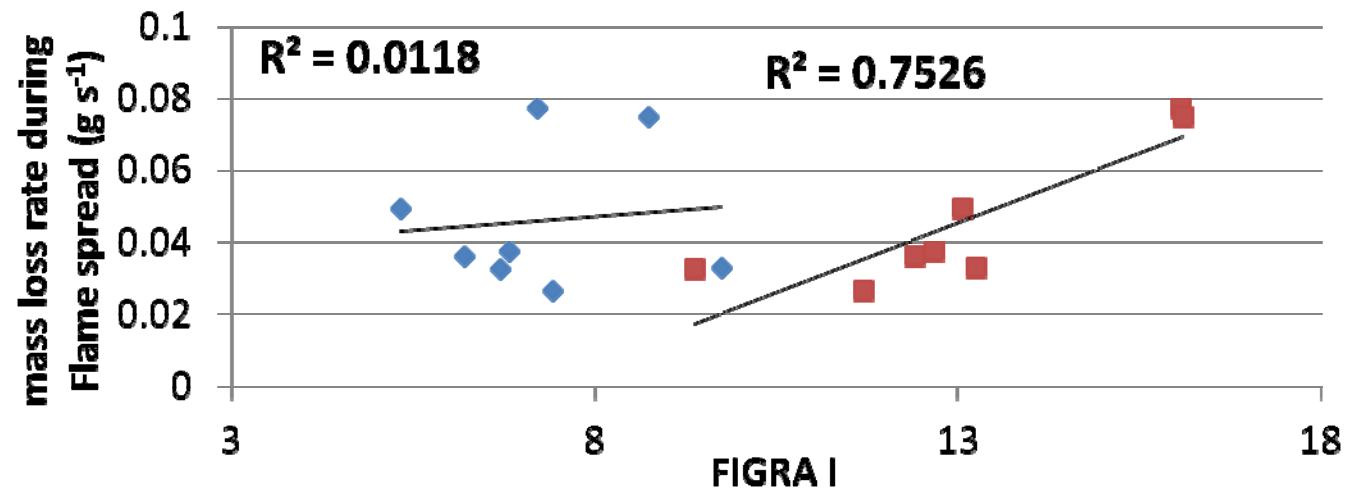


Comparison: cone calorimeter vs. flame spread test

Incid. Heat flux
 15 kW m^{-2}



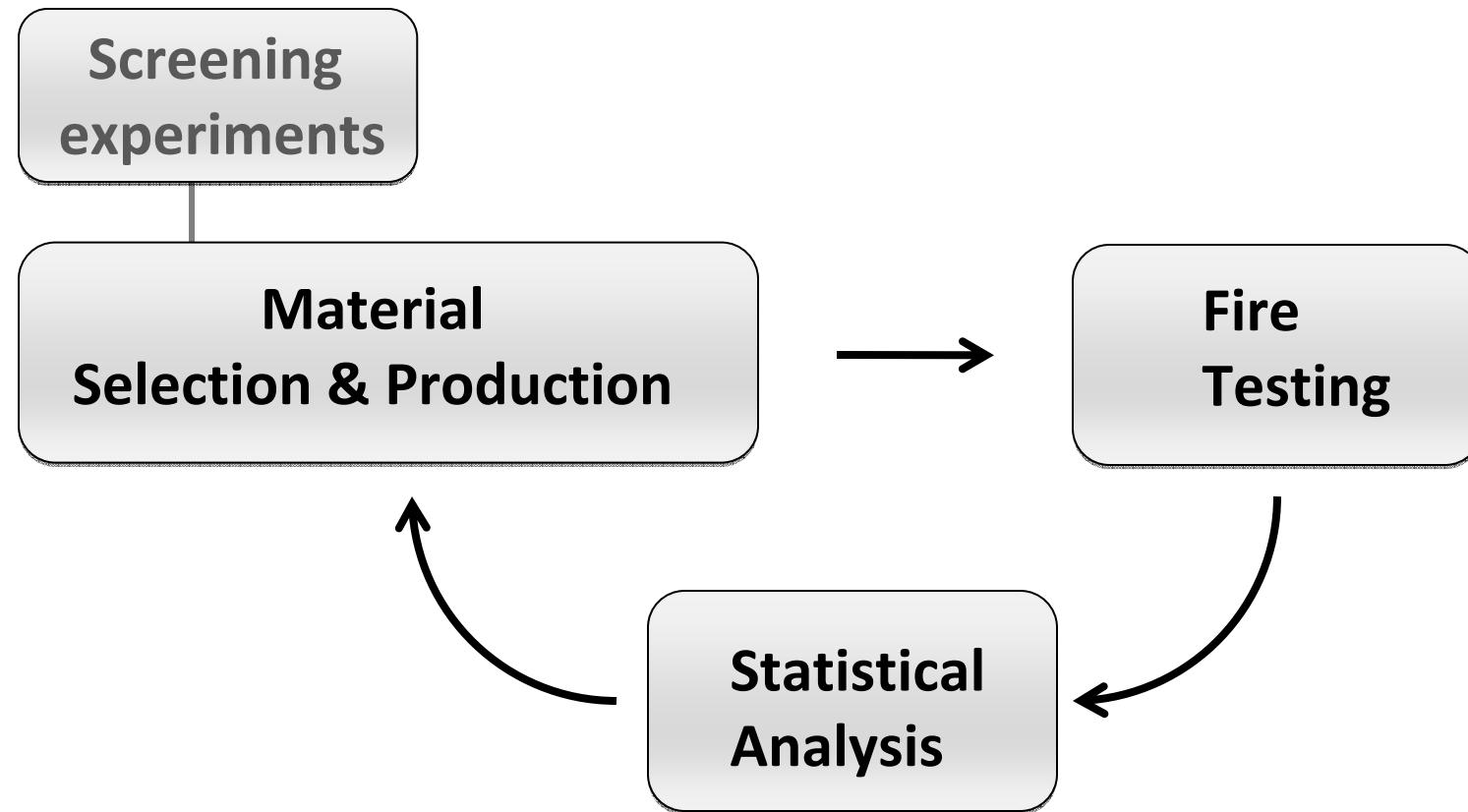
Incid. Heat flux
 30 kW m^{-2}



Summary – cone calorimeter tests

- The test conditions severely affect the shape of the heat release rate curve and measured parameters.
- Under well-control conditions, very well-reproducible results can be achieved to compare different foam formulations.
- Eight foam formulations (3 surfactants, 2 polyols, graft- and bio-polyol) did not show significant differences in standard cone calorimeter test with a covered edge.
- Testing samples with an exposed edge allows to capture the physical behavior of the foam, which affected the ease of pool fire formation in the flame spread tests.

Experimental design with 3 iterations



I **Chemical composition**

raw materials, impurities

II **Morphology**

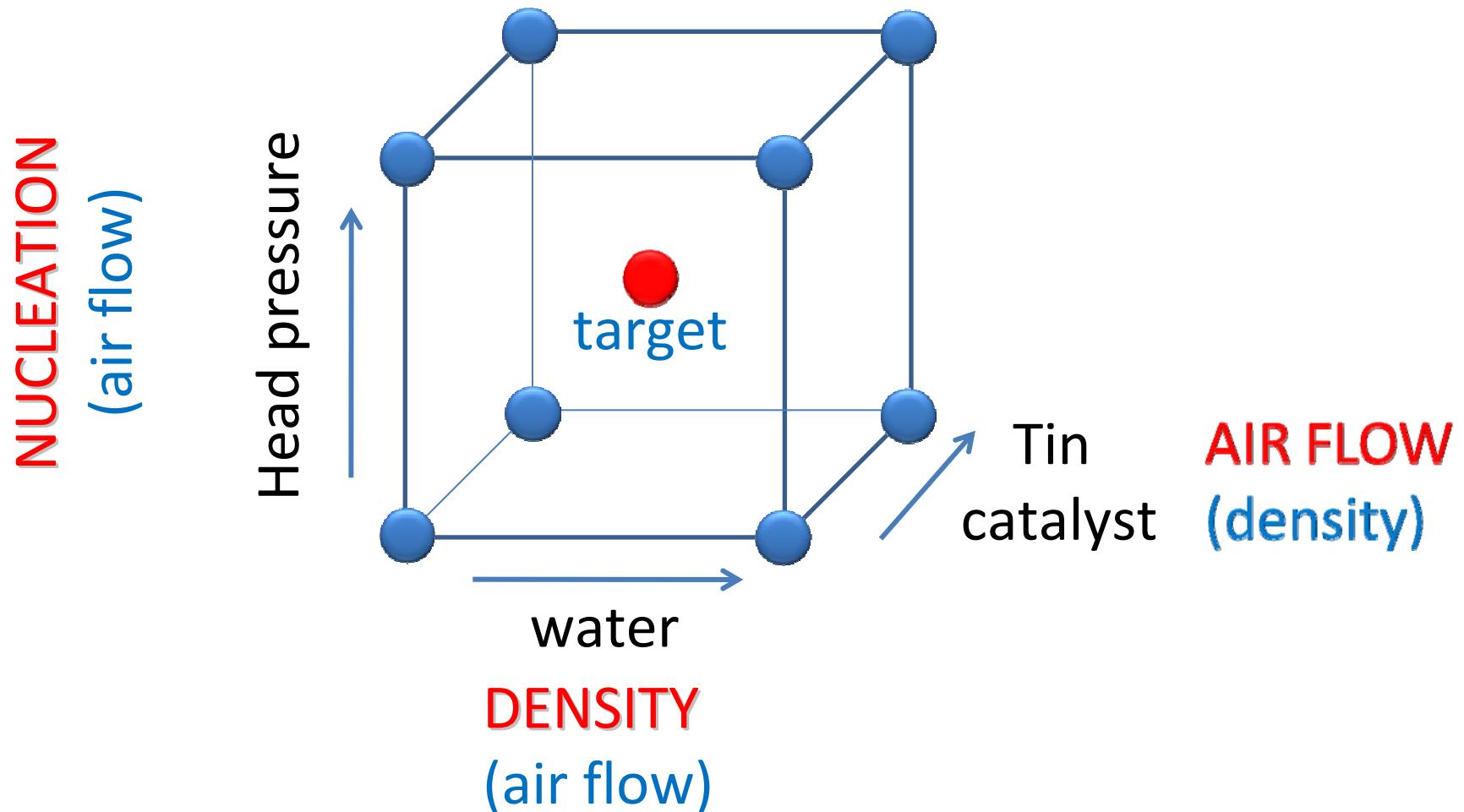
air flow, density, ...

III **Scale-Up & Correlation**

(selection)

2nd Iteration:

Morphology



THANK YOU!

Acknowledgements

**Szabolcs Matko, Jeffrey W. Gilman, Thomas J.
Ohlemiller, Richard G. Gann, Michael Smith, Mauro
Zammarano, John R. Shields, Rick Davis**

NIST Engineering Laboratory, Fire Research Division

Neil Witten
Zotefoams PLC, UK

THANK YOU!

