

CRASHWORTHINESS OF COMPOSITE FUSELAGE STRUCTURES -Material Dynamic Properties



K.S. Raju
Department of Aerospace Engineering
Wichita State University

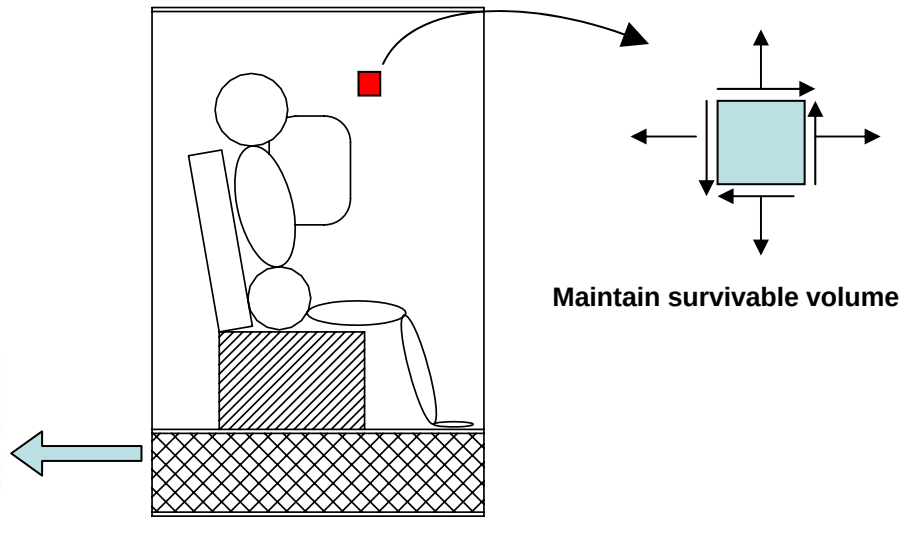
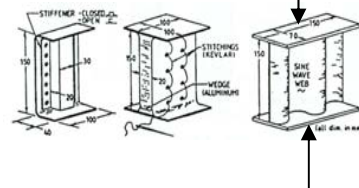
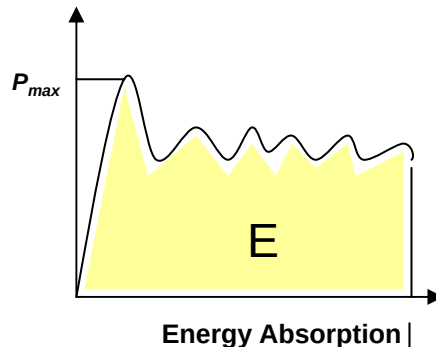
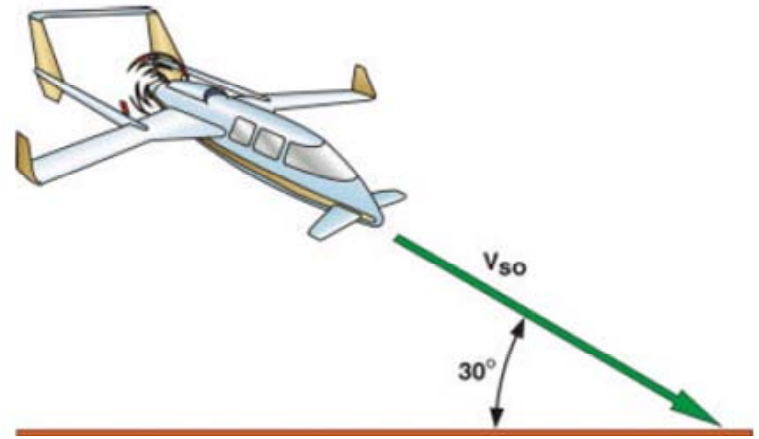


Program Monitor : Allan Abramowitz
FAA William J. Hughes Technical Center

The Fifth Triennial International Aircraft Fire and Cabin Safety Research Conference,
Oct 29- Nov1, 2007, Atlantic City, NJ

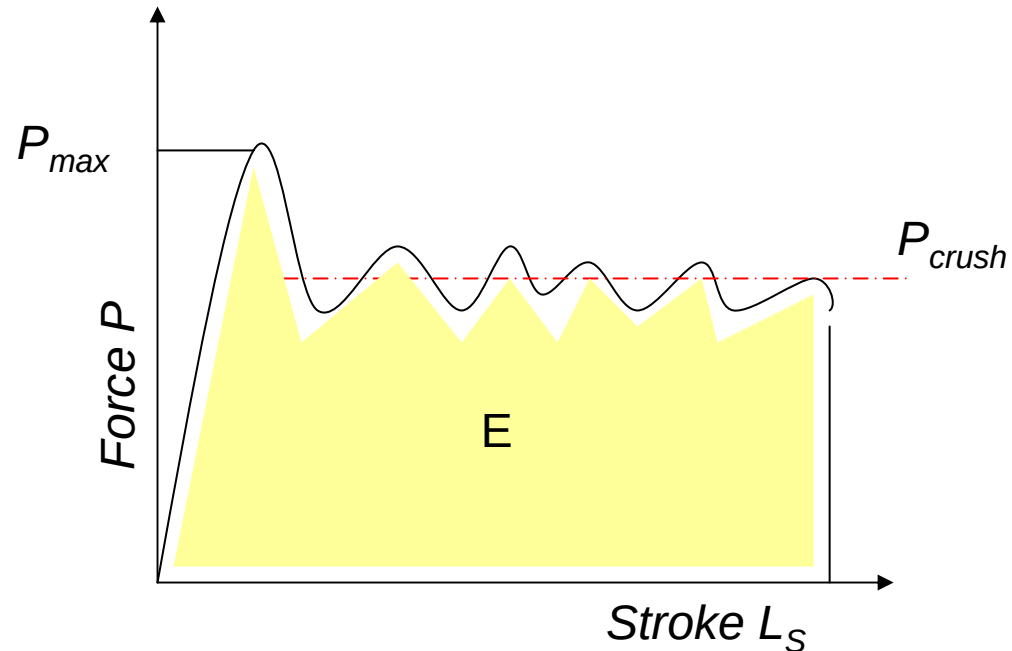
Background

- Crashworthiness
 - Maintain survivable volume
 - Alleviate occupant loads
- Energy Absorption
 - Metals – Plastic deformation
 - Composites – controlled failure modes
- Factors affecting energy absorption
 - Geometry (?)
 - **Strain rate (?)**



Energy Absorption in Composites

- Maximize energy dissipated due to formation of surfaces
 - Matrix cracks, delaminations, fiber-matrix interface failure, fiber fractures
 - Maximize the damage volume {multiple locations of damage}
- Minimize reduction /loss of load path
 - Provision for sustained stability



Maximization bounded by “*stability*” of the transmitting structure/device and availability of crush space

Maximization bounded by “*safe loads*” that can be transmitted

$$E = \int_0^{L_S} P d\delta$$

The equation shows the integral of Force P with respect to displacement δ from 0 to L_S . An arrow points from the text “Maximization bounded by ‘*stability*’...” to the upper limit L_S in the integral. Another arrow points from the text “Maximization bounded by ‘*safe loads*’...” to the integrand $P d\delta$.

Energy Absorption Devices

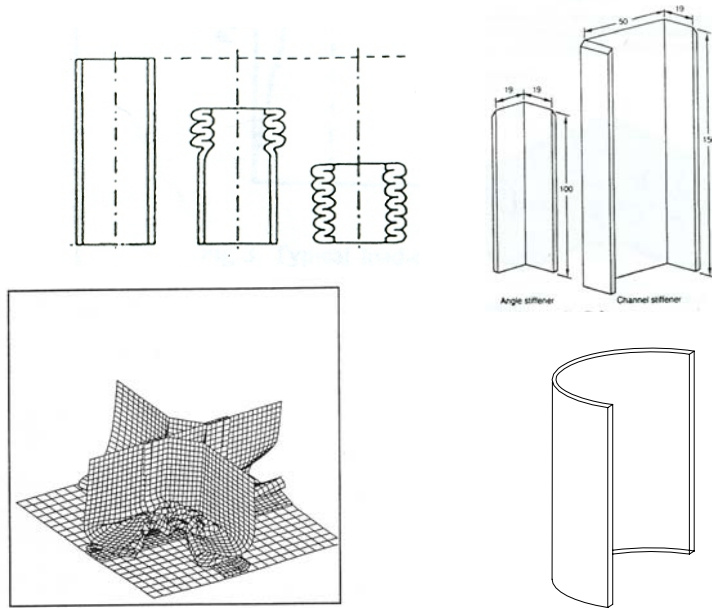


Figure 11. Finite element simulation of HTP-cruciform under impact at 10 m/s.

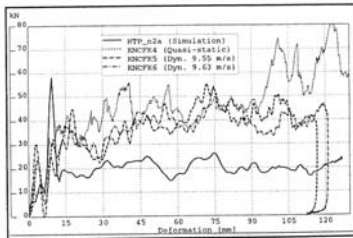


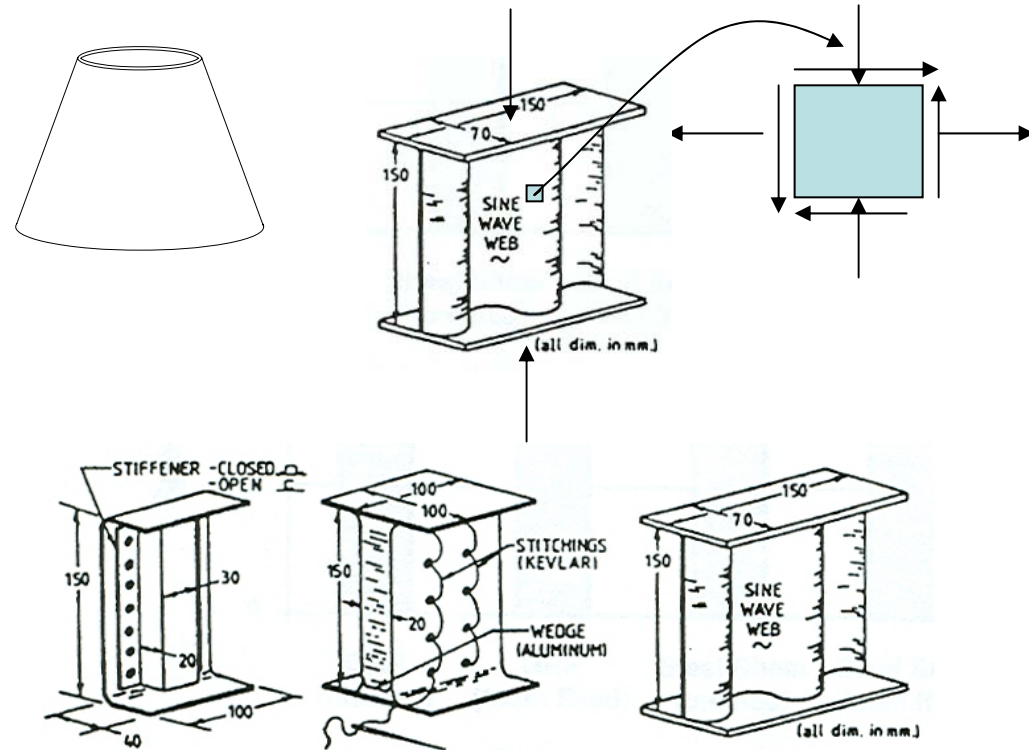
Figure 12. Load-deflection response of HTP-cruciforms under impact-comparison of finite element simulation and test data.

Hull D (1991) *Comp. Sci Tech*, 40.

Bannerman & Kindervater (1984) in *Structural Impact and Crashworthiness*

Bolukbasi & Laananen (1995) *Composites*, 26.

Carruthers, Kettle & Robinson (1998) *Appl Mech Rev*, 51.

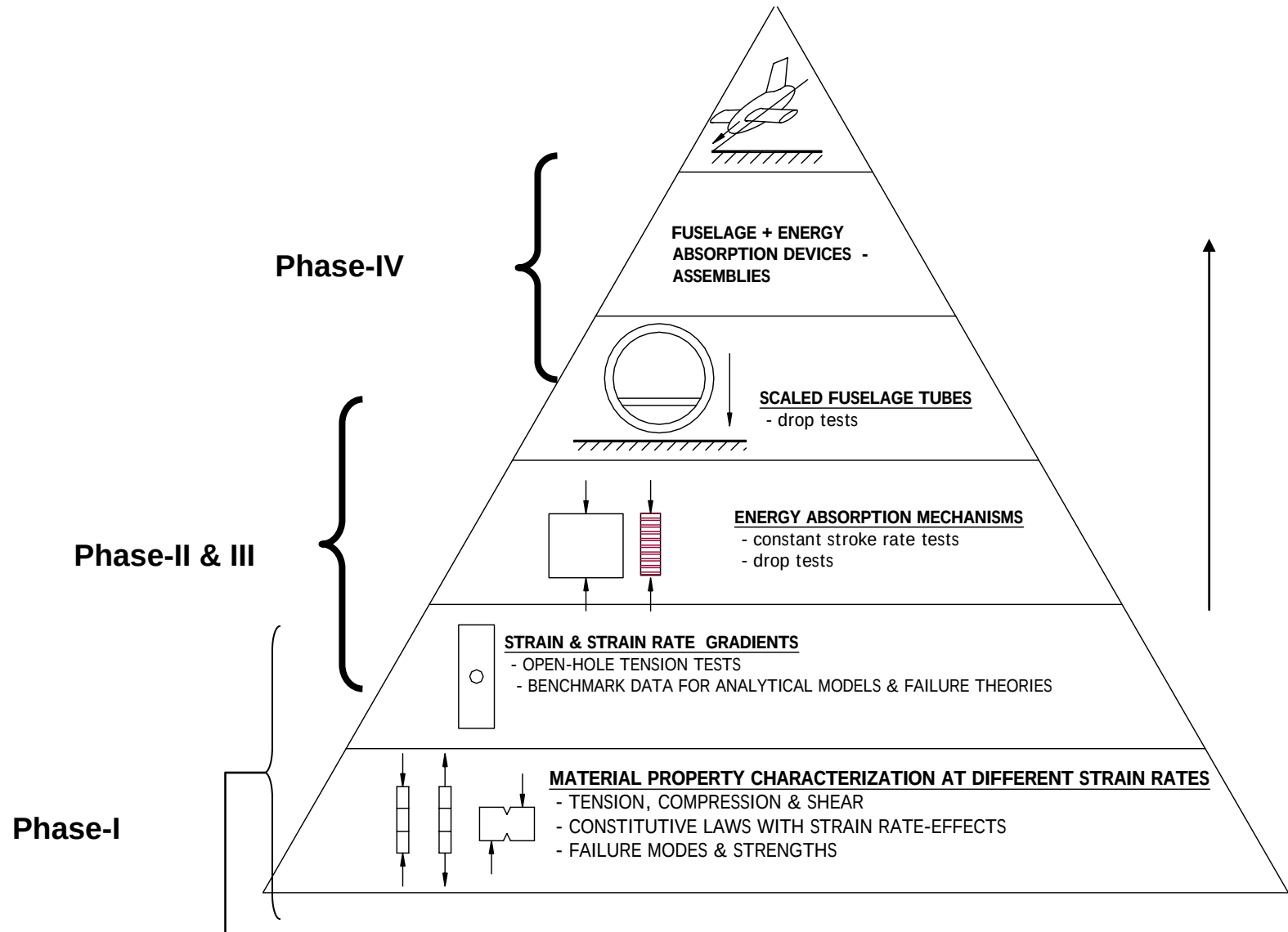


-Rate effects are evident (+ or -) but in terms of stroke rate

-Strain rates not reported /measured (?)

-Strain rate not proportional to stroke rate due to complexity of localized deformation & Strain gradients

APPROACH



Tasks..

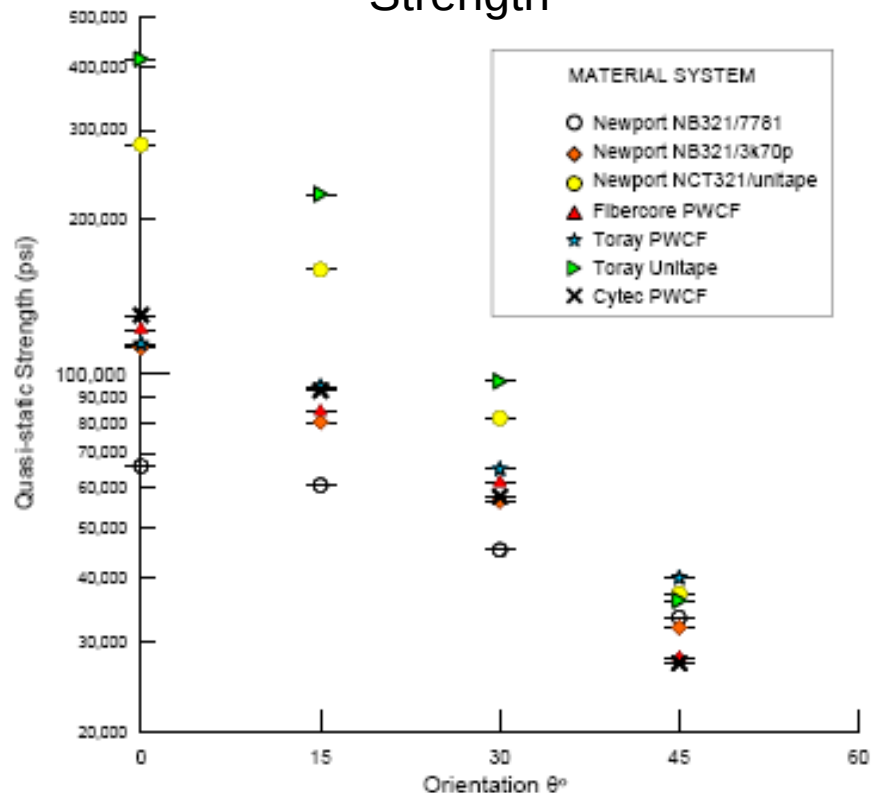
- Phase-I
 - In-Plane Tensile Properties (Strength & Modulus)
 - $[0^\circ]_n$, $[\pm 15^\circ]_{ns}$, $[\pm 30^\circ]_{ns}$, $[\pm 45^\circ]_{ns}$
 - In-Plane Compressive Properties (Strength & Modulus)
 - $[0^\circ]_n$, $[\pm 15^\circ]_{ns}$, $[\pm 30^\circ]_{ns}$, $[\pm 45^\circ]_{ns}$
 - In-Plane Shear Properties (Strength & Modulus)
 - $[0^\circ/90^\circ]_{ns}$
- PHASE-II
 - Open- Hole Tension
 - Pin Bearing
 - Interlaminar Shear
 - Flexure
 - Scaled Fuselage sections
- PHASE-III
 - Fracture Toughness
- PHASE-IV
 - EA device

Material Systems

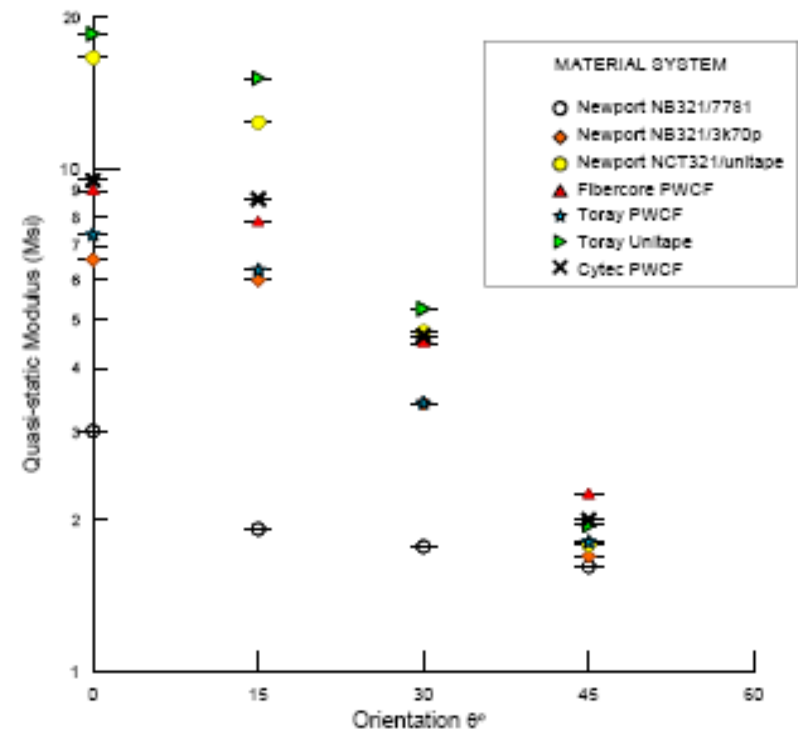
- Material systems selected by FAA/industry participants
 - State of Kansas (`NIAR.INDUSTRY.STATE`) funding
 - Boeing, Spirit Aerosystems, Hawker BeechCraft (Raytheon), Cessna
 - FAA personnel involved
 - Allan Abramowitz, Curtis Davies, J. Zvanya
 - Wide range of materials
- Material Systems
 - Newport NB321/3k70P
 - Newport NB321/7781 Fiberglass*
 - Newport NCT321/G150 Unitape
 - Toray T800S/3900-2B[P2352W-19] BMS8-276 Rev-H- Unitape*
 - Toray T700G-12K-50C/3900-2 Plain Weave Carbon Fabric*
 - Fibercote E-765/PW Carbon Fabric /Epoxy
 - Cytec PWC T300 3KNT Plain Weave Carbon Fabric*
- Material systems for phase-II and beyond limited to Newport & Toray systems

Tensile Properties ... Quasi-Static Loading

Strength



Modulus



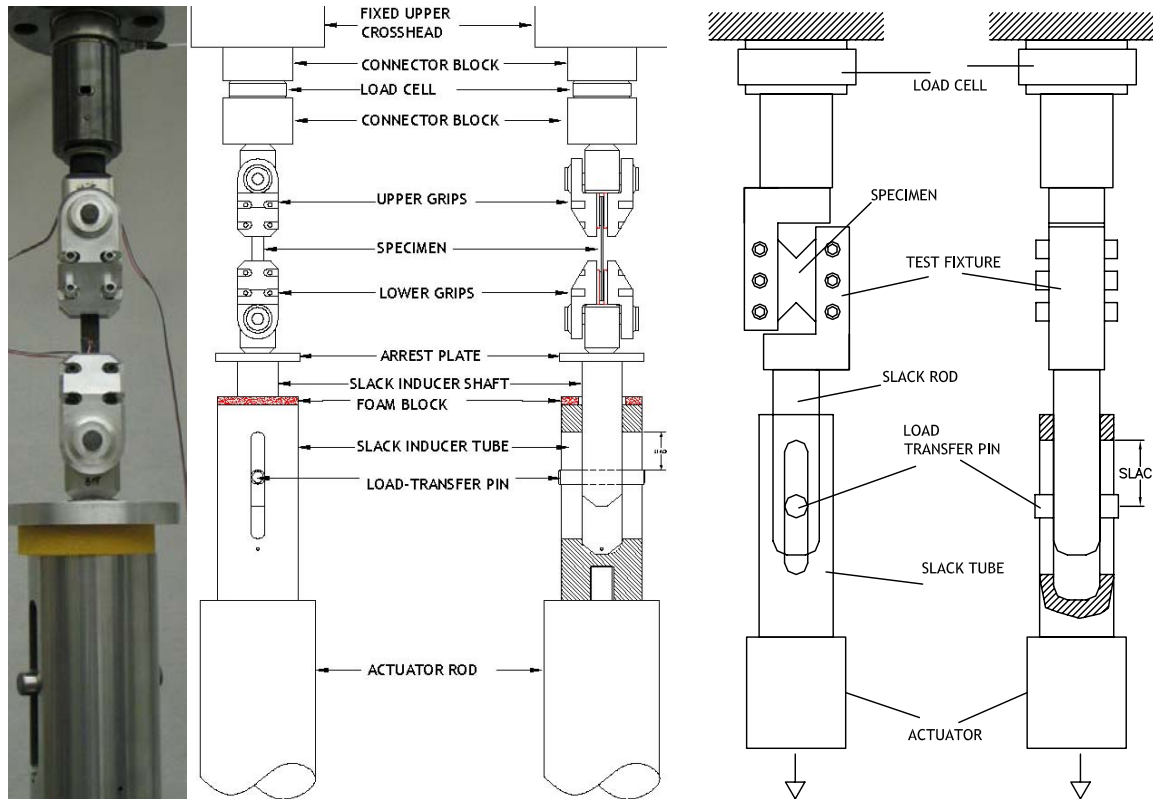
TEST APPARATUS

- TENSION MODE TESTING
 - Tension, shear and flexure tests
- MTS High Stroke Rate System (MTS-HSRS)
 - Stroke rate ~ 500 in/sec
 - +/- 7 inches stroke
 - Load capacity
 - 5 kips @ rated speed
 - 9 kips maximum
 - Load measurement
 - Piezoelectric load cells
 - +/- 0.5kip, +/- 1kip, +/- 10kips
 - National Instruments PCI 6110 DAQ
 - 4 Channels
 - 5 MHz (simultaneous sampling)
 - 12 bits resolution
 - Test control
 - MTS MultipurposeTestware computer program



TEST APPARATUS

- TENSION MODE TESING
 - Tension, shear and flexure tests



- **SLACK INDUCER MECHANISM**

- Allows actuator acceleration to desired speed prior to loading the specimen

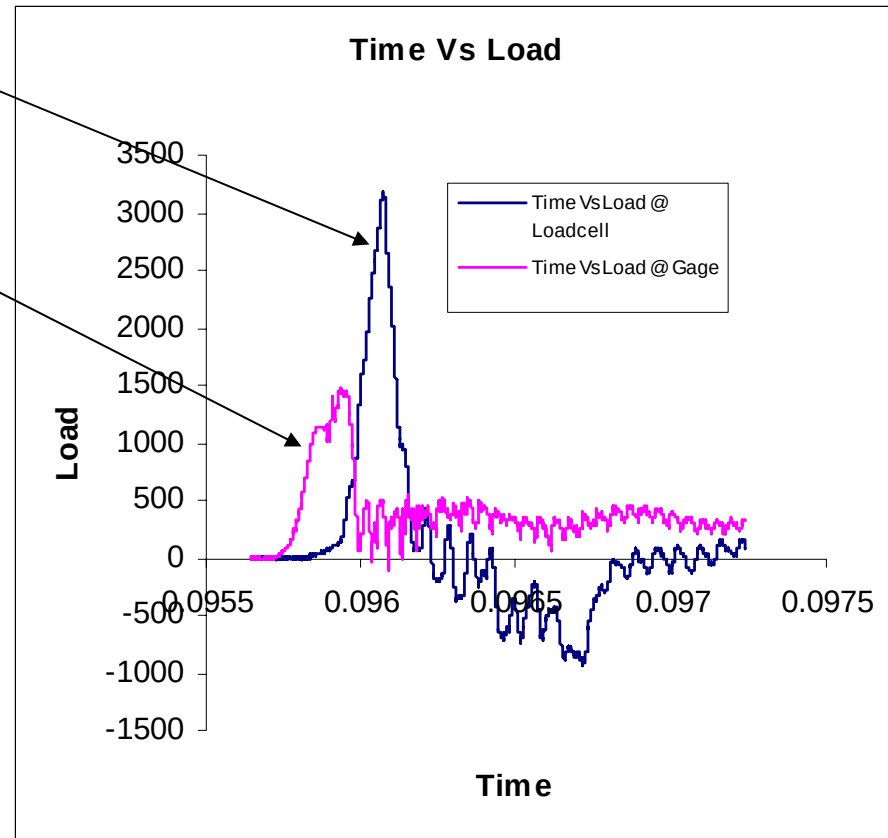
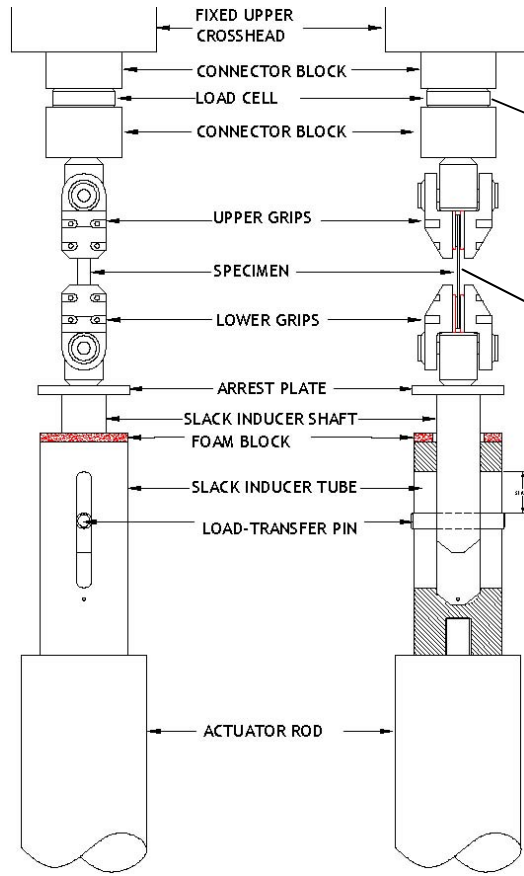
- **LOW-MASS GRIPS**

- mechanical wedge grips
 - 2.4 lbs
 - 15 kip capacity

Davis, E.A., Trans. ASME, 60, 1938
Elam, C.F., Proc. Roy. Soc. Lond., A, 165, 1938
ManJoine, M.J., Trans. ASME, 66, 1944 A-21
Milkowitz, J., Trans. ASME, 69, 1947 A-21
Morrison, J.L., Engineer, Lond., 158, 1934

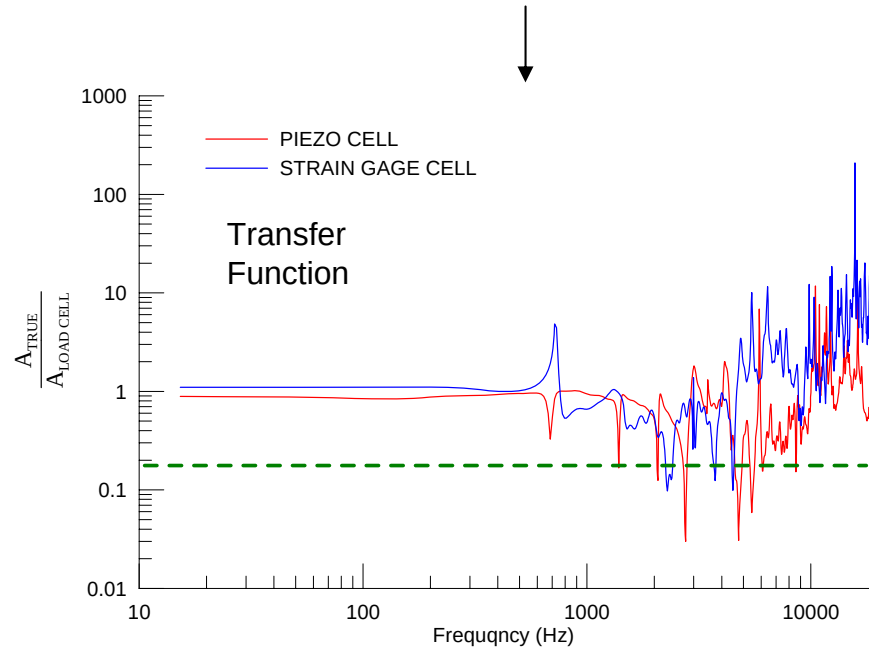
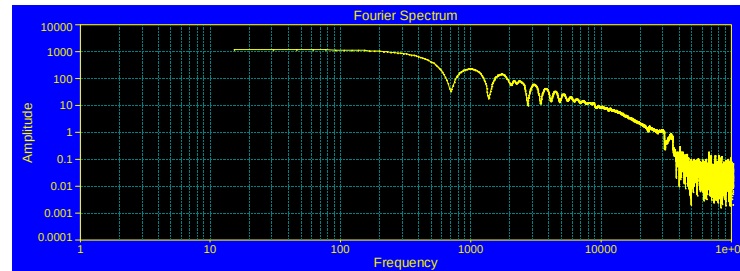
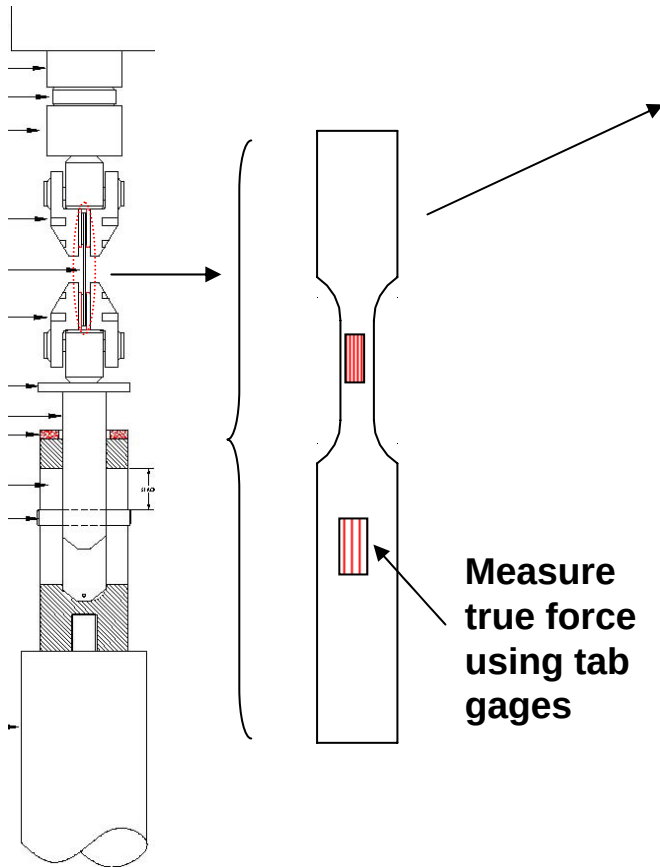
TENSION TEST APPARATUS

- Signal Modulation



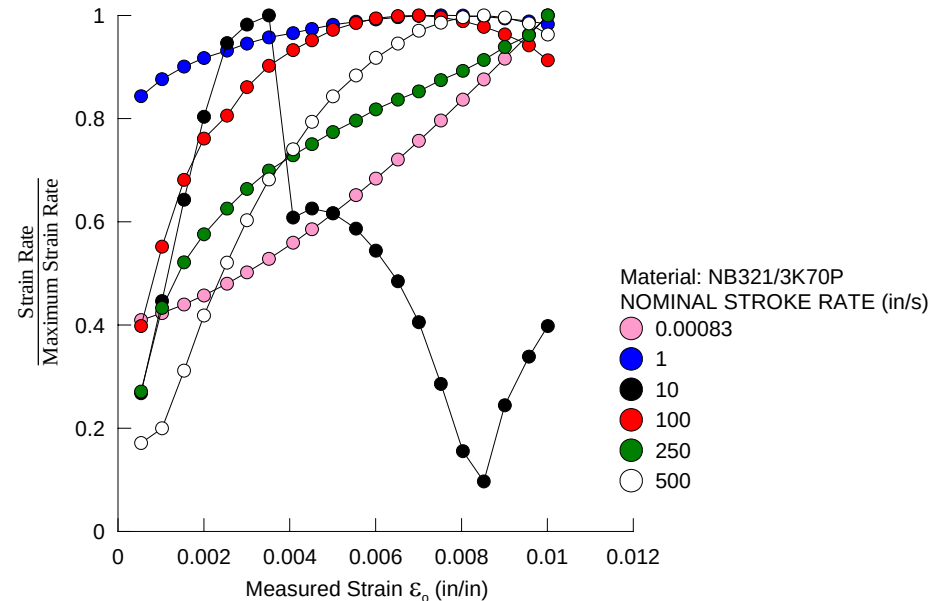
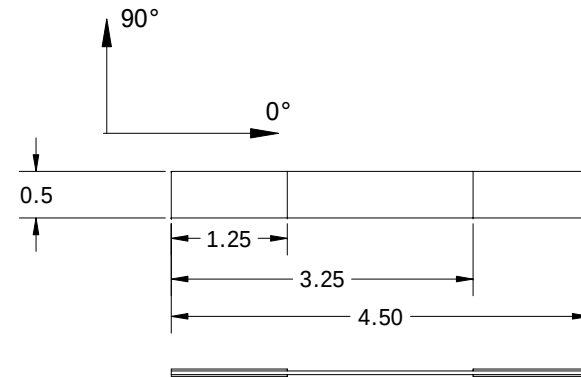
Tension testing – Signal Modulation

- Correction using Experimentally determined Transfer Function



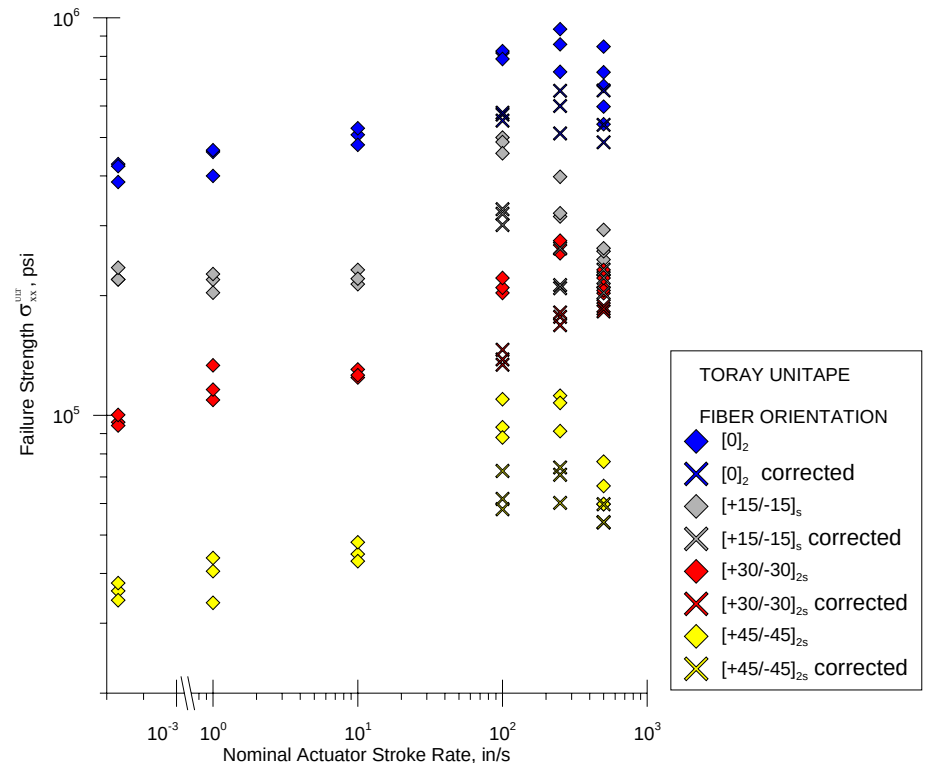
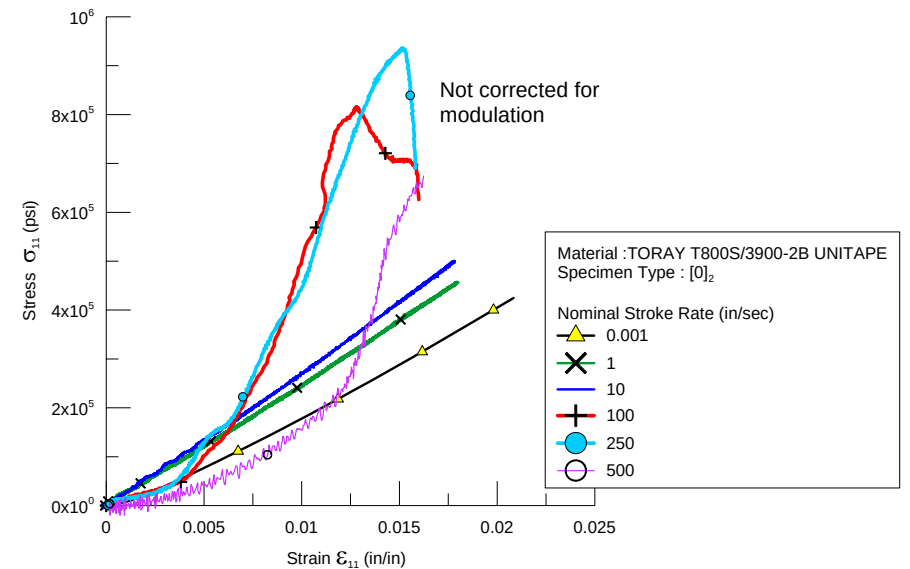
Tension Testing

- SPECIMEN GEOMETRY
 - 2 inch gage length
 - 0.5 inch width
 - Thickness limited by loading capacity of the testing machine
- TEST RATES
 - 1×10^{-4} in/s (quasi-static)
 - 1, 10, 100, 250 and 500 in/s
 - 3 specimens each
- CONSTANT STROKE RATE TESTS
 - Based on actuator displacement
 - Strain rate varies throughout the test
 - Variation of strain rate is dependent on slack inducer element (s) characteristics (stiffness and mass)

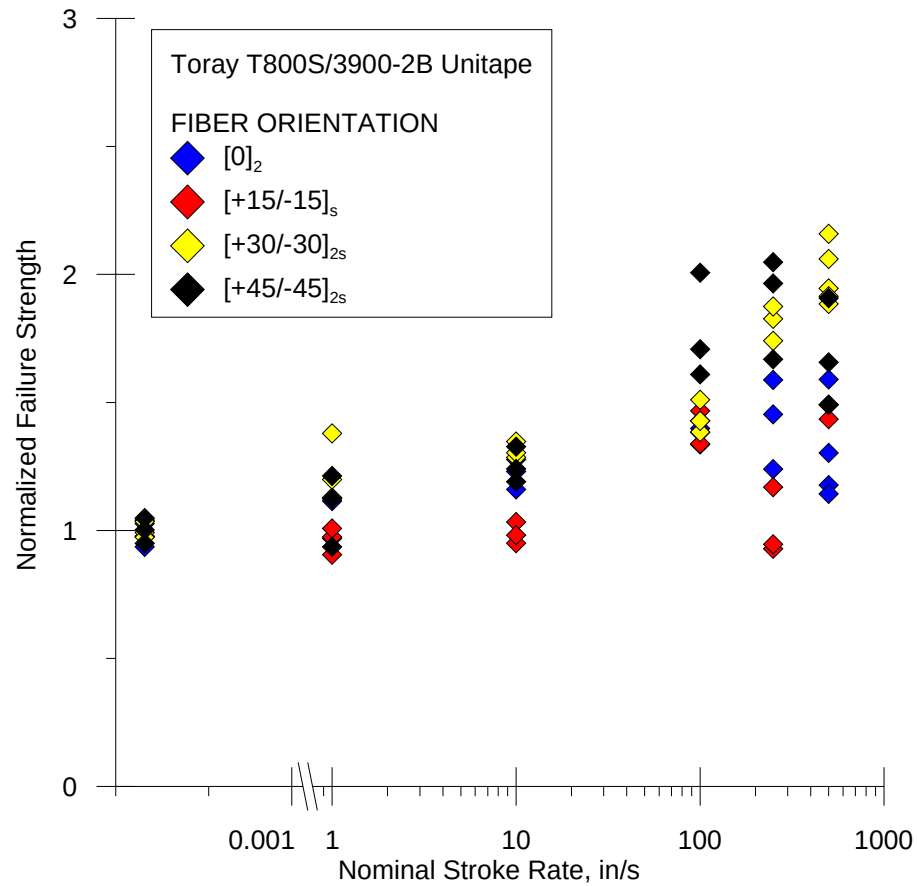


Tension testing – Results

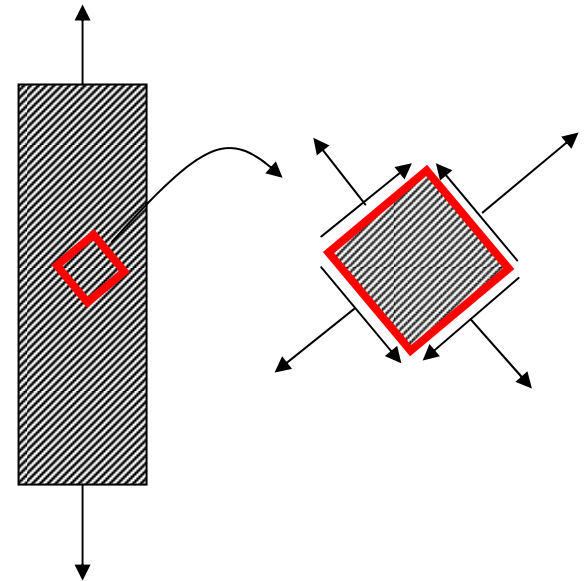
- Maximum strain rate achieved $\sim 250/s$
- Tensile Strengths
 - Tension strength was observed to increase with stroke (strain) rate for all material systems & orientations
 - Magnitude of strength increase was dependent on fiber orientation and material system
 - Newport NB321/7781 fiberglass material exhibited highest strength increase amongst the materials tested



Effects of Combined State of Stress

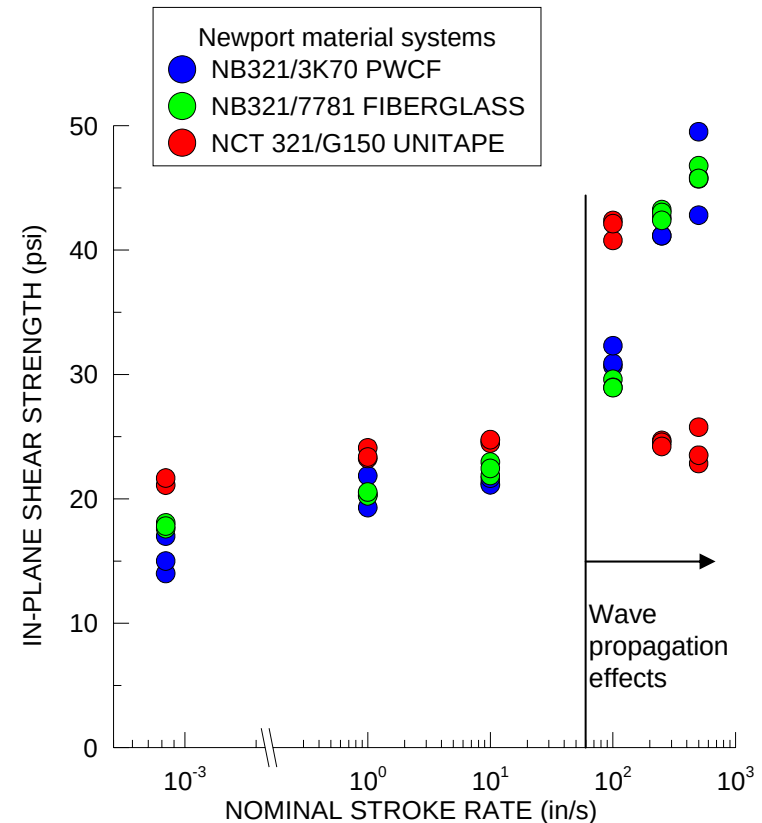
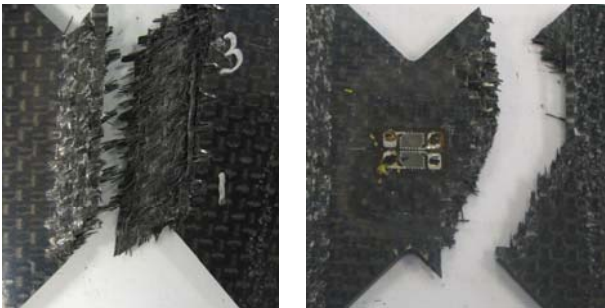


- Strength increase higher for off-axis specimens



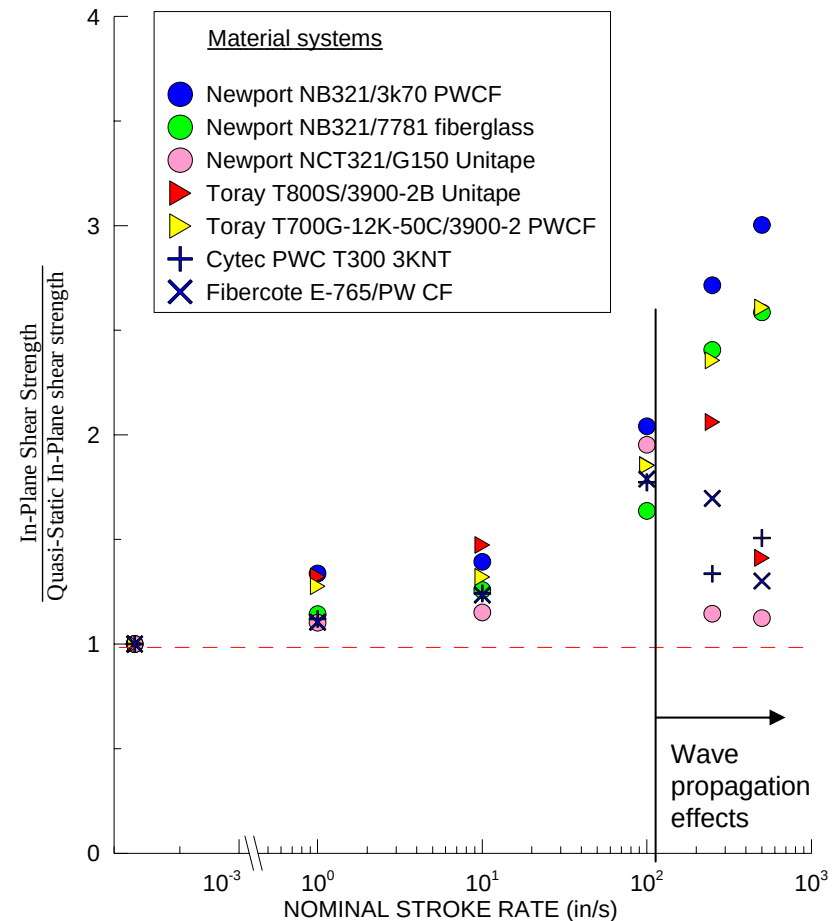
IN-PLANE SHEAR STRENGTH

- **NEWPORT MATERIAL SYSTEMS**
 - **Fabric reinforced systems (3k70P and 7781)**
 - Shear strength increases with stroke rate
 - Failure mode changes at higher rates
 - **Unitape system**
 - Shear strength increases up to stroke rate of 100in/s, but decrease at 250 and 500 in/s
 - No change in failure mode



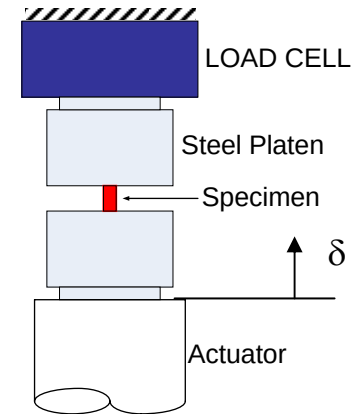
IN-PLANE SHEAR STRENGTH

- **COMPARISON OF SHEAR STRENGTHS**
 - **Fabric reinforced systems**
 - Shear strength increases with stroke rate
 - Failure mode changes at higher rates
 - **Unitape system**
 - Shear strength increases up to stroke rate of 250 in/s, but decreases at 500 in/s
 - No change in failure mode
- **Corrections for modulation of load signal**
 - Transfer function (under progress)



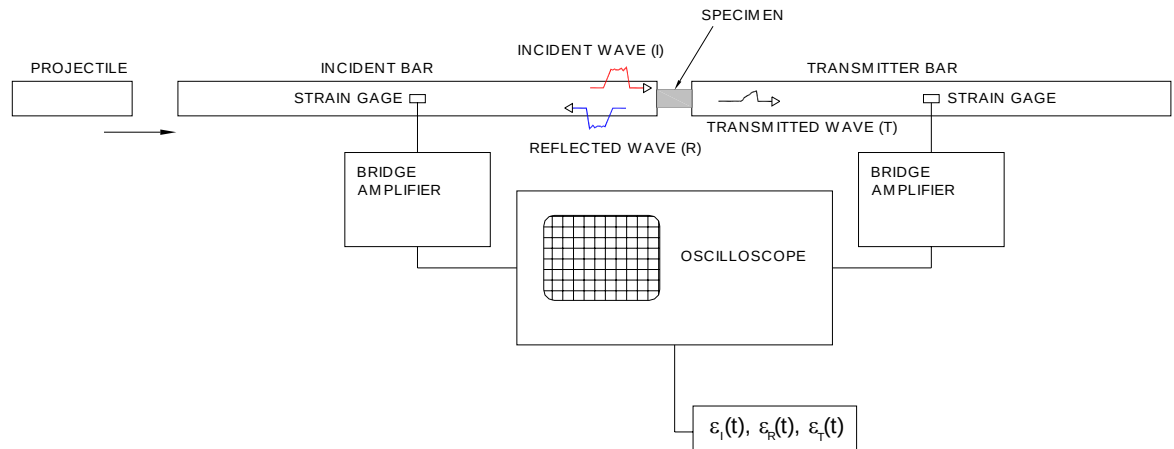
COMPRESSION TEST APPARATUS

- COMPRESSION MODE TESTING
 - Split- Hopkinson Pressure Bar (SHPB)
 - Compressive strength
 - MTS servo hydraulic testing machine
 - Compression at slow to medium rates



• SHPB SPECIFICATIONS

- Bar diameter : 1.00 inch
- Bar Material : Vascomax 350
- Bar lengths
 - Incident bar : 48"
 - Transmitter bar : 36"
- Barrell length : 48 inches
- Projectiles : 1", 2", 4", 6" & 12"
 - Pneumatically driven (100 psi)
 - Velocities ~ 2000 in/s
- PULSE SHAPING
 - Copper discs
- DATA ACQUISITION
 - Tektronix TDS 3034 Digital Oscilloscope
- SIGNAL CONDITIONING
 - Ectron model 778 (3 MHz bandwidth)



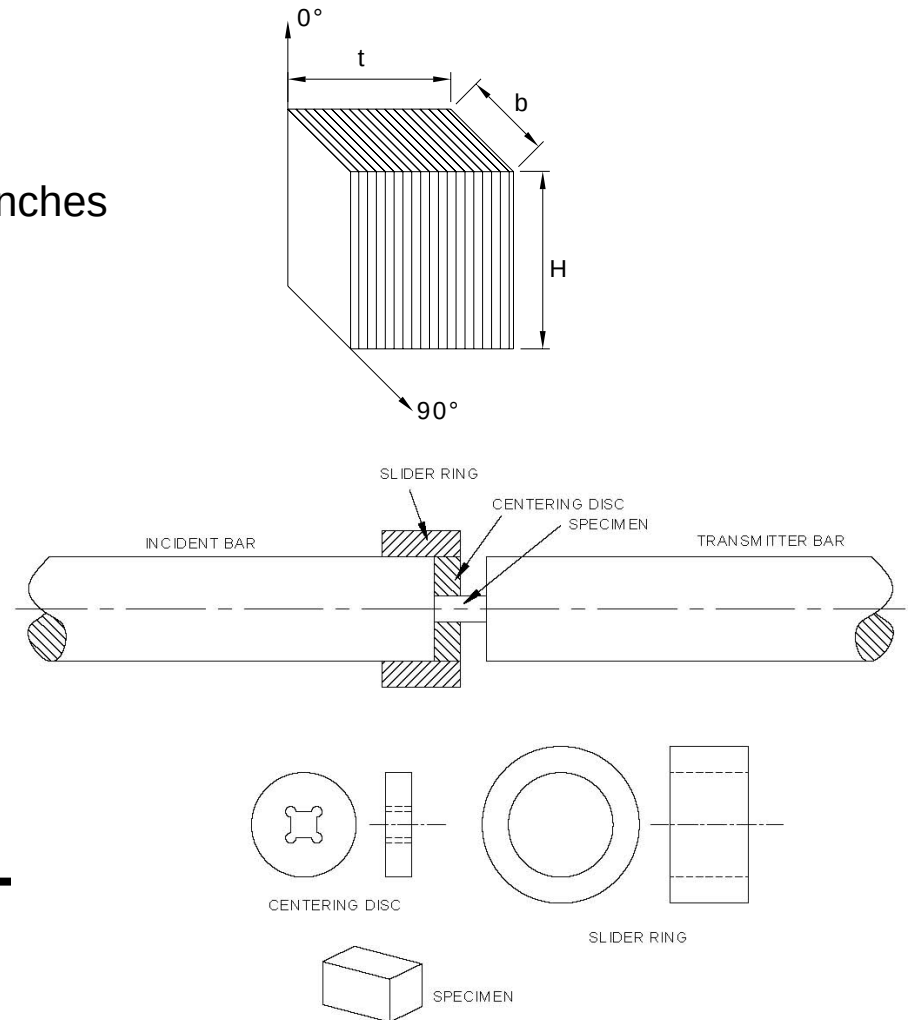
SPLIT-HOPKINSON PRESSURE BAR APPARATUS (SHPB)

- SPECIMEN GEOMETRY^{Ref}

- Rectangular cross-section
- Laminate thickness (t) ~ 0.17 to 0.25 inches
- Specimen width (b) ~ 0.25 inches
- Specimen height (H) ~ 0.25 inches

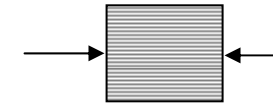
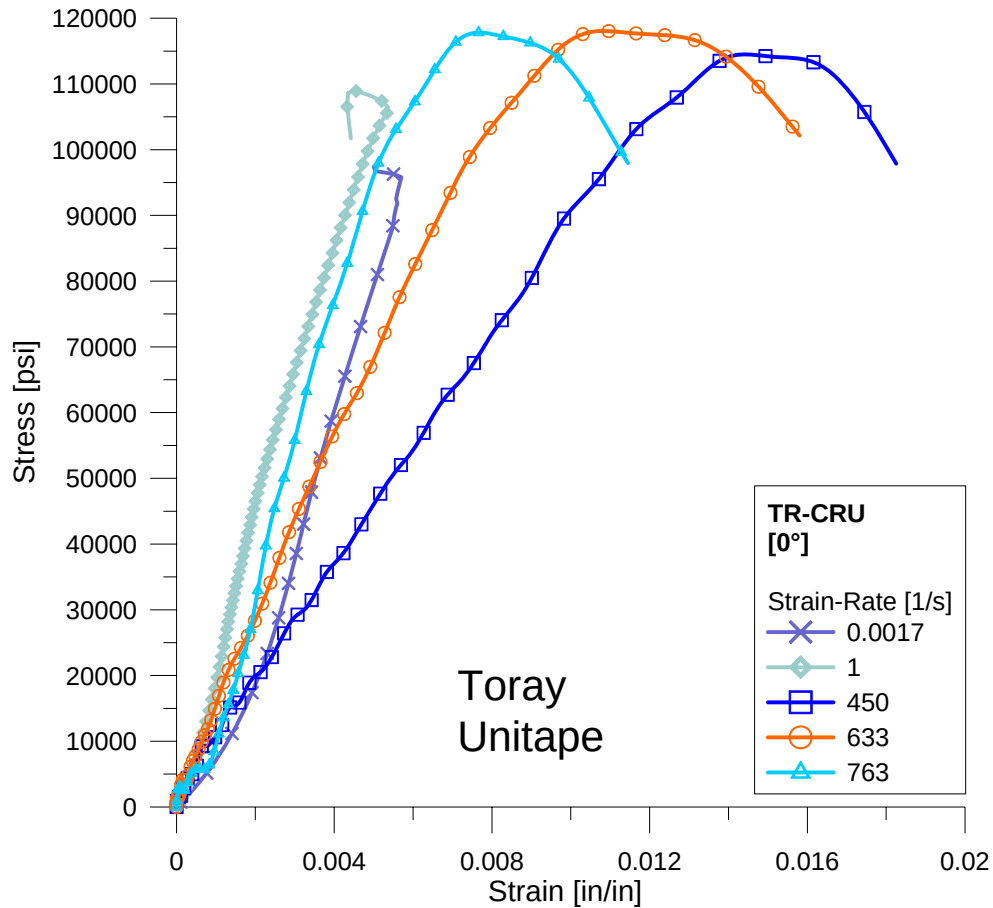
- SPECIMEN ALIGNMENT

- Centering disc & slider ring



Ref: E. Woldesenbet & J.R. Vinson, *AIAA Journal*, Vol.37, Sept. 1999.

Compression Testing...Results



Failure modes



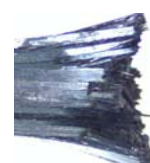
0.0017 s⁻¹



1 s⁻¹



450 s⁻¹

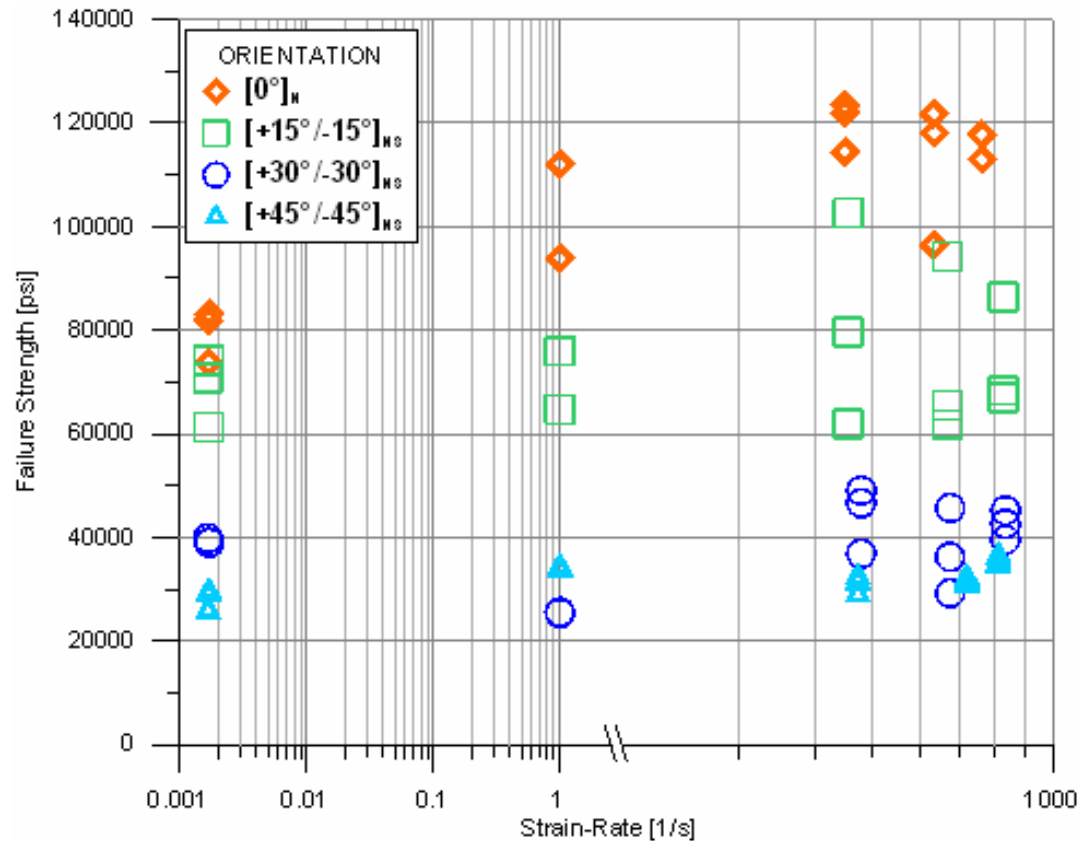


633 s⁻¹



763 s⁻¹

Compression Testing...Results



Toray Unitape

PIN-BEARING RESPONSE

- **Material Systems**

- Newport NB321/7781 fiberglass
- Newport NB321/3k70 PWCF
- Toray T700G-12K-50C/3900-2 PWCF

- **Laminate type**

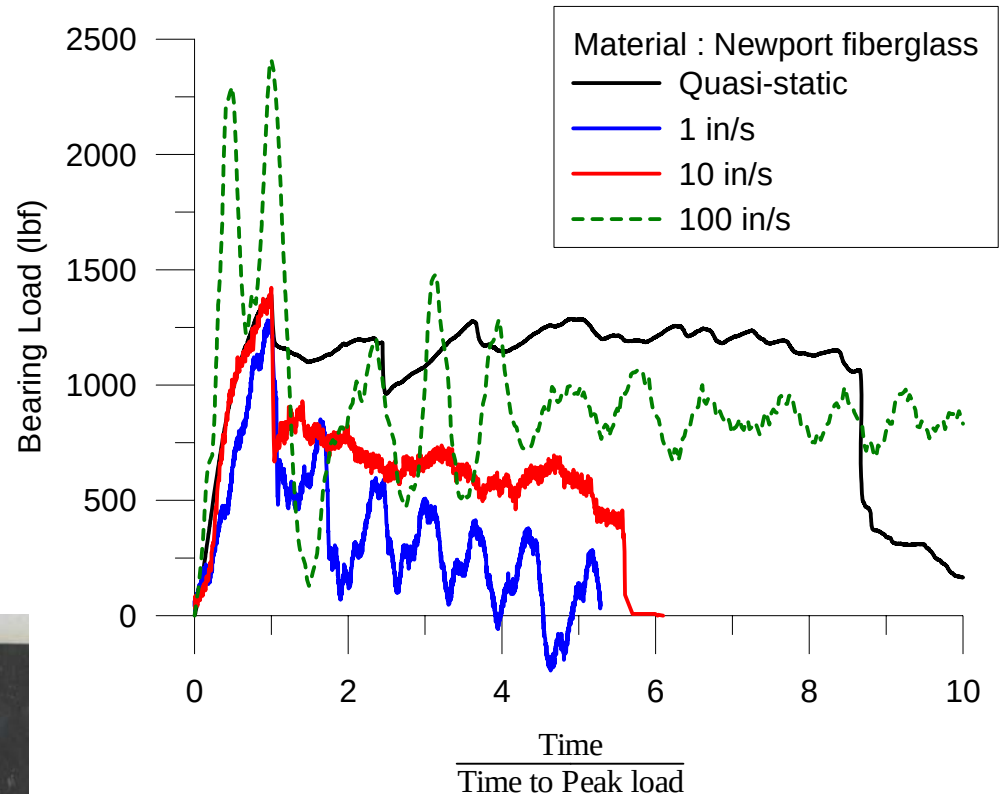
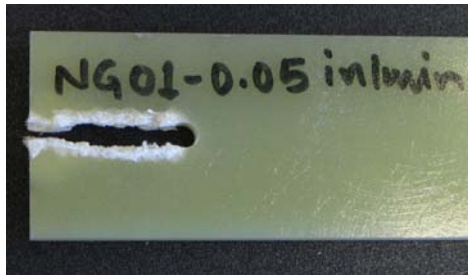
- $[45/0/45/0/45]_s$

- **Pin diameter : 0.125 inches**

- **Test speeds : quasi-static, 1,10,100, and 250 in/s**

- **RESULTS**

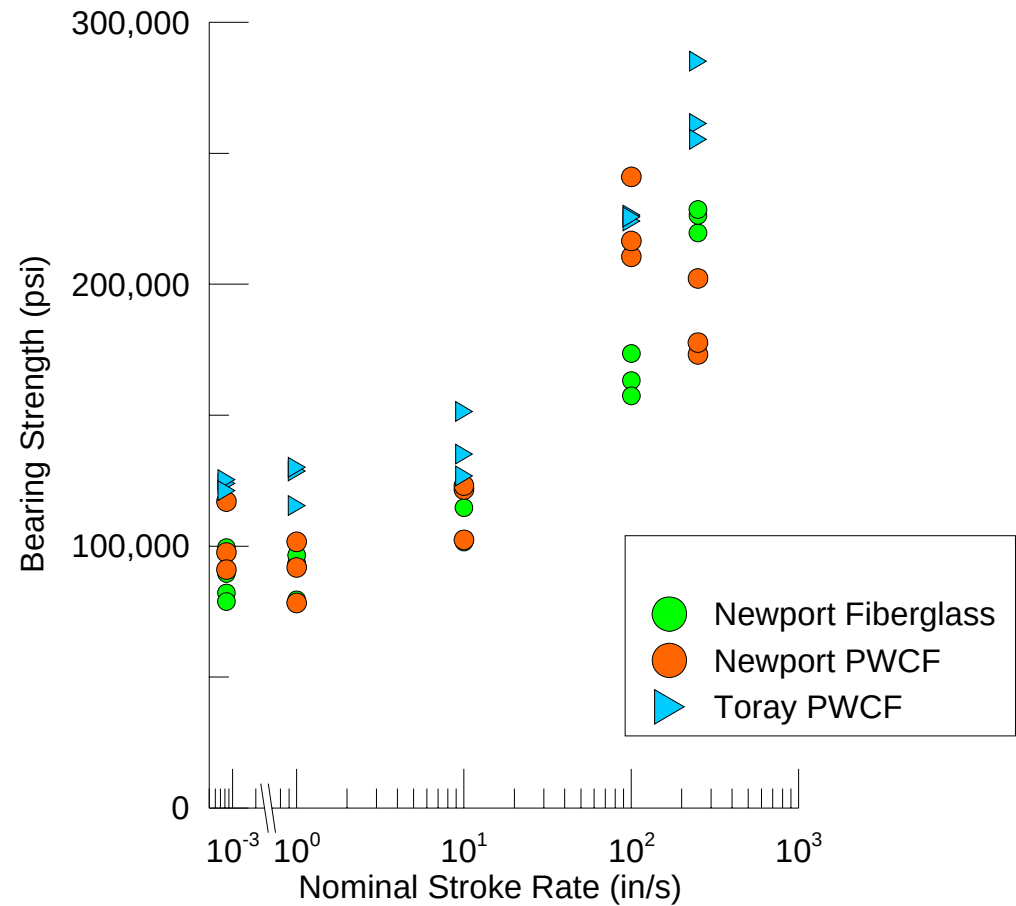
- Sustained loading past initial failure, decreases at higher rates of loading
- Failure mode



PIN-BEARING RESPONSE

- **RESULTS**

- Bearing strengths based on peak recorded load
 - Hole deformation not measured
- Pin bearing strength increases with test speed



FLEXURE TESTS

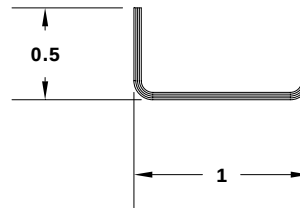
- **LAMINATED BEAMS**

- **Material systems**

- Newport NB321/7781 fiberglass
 - Newport NB321/3k70 PWCF

- **Layup sequence**

- [0/45/45/0]



- **SANDWICH BEAMS**

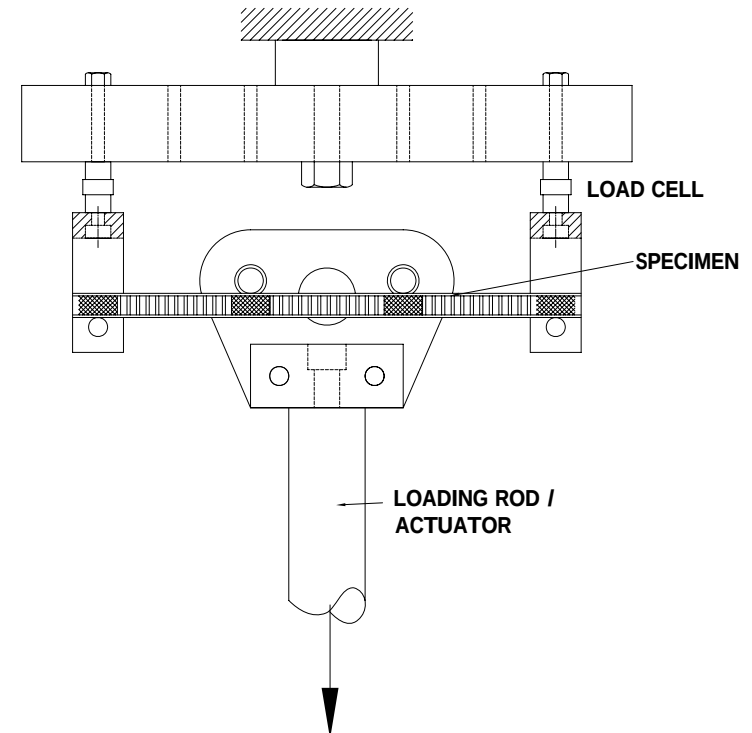
- **Material systems**

- Newport NB321/7781 fiberglass
 - Newport NB321/3k70 PWCF

- **Layup sequence**

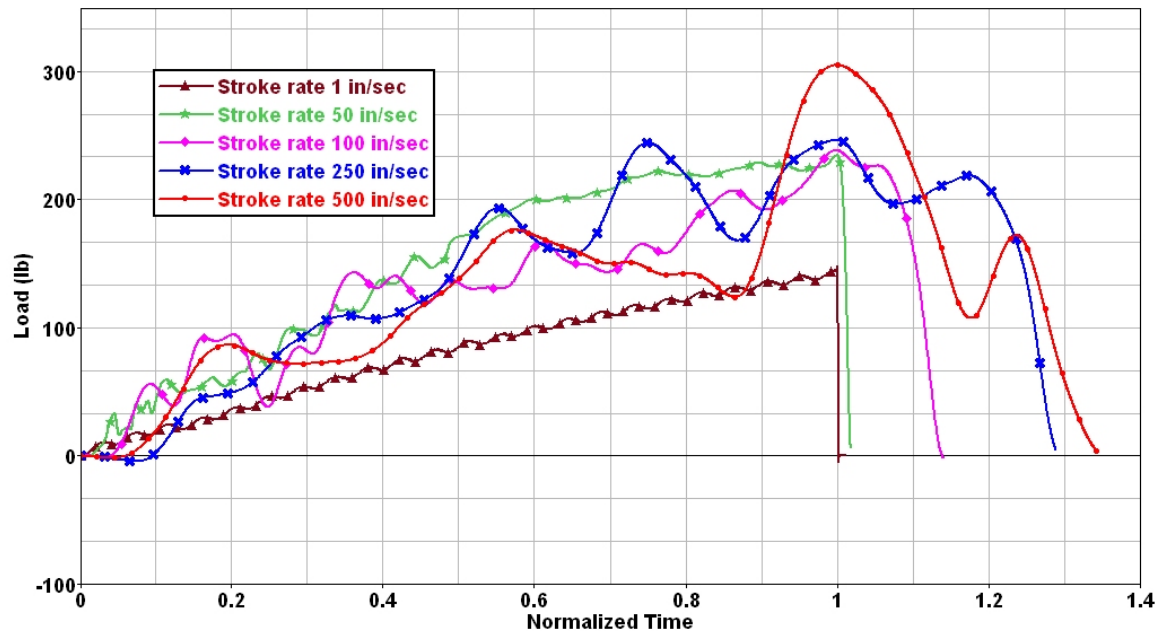
- [0/45/0/45/CORE]_S

- STATUS : Testing completed



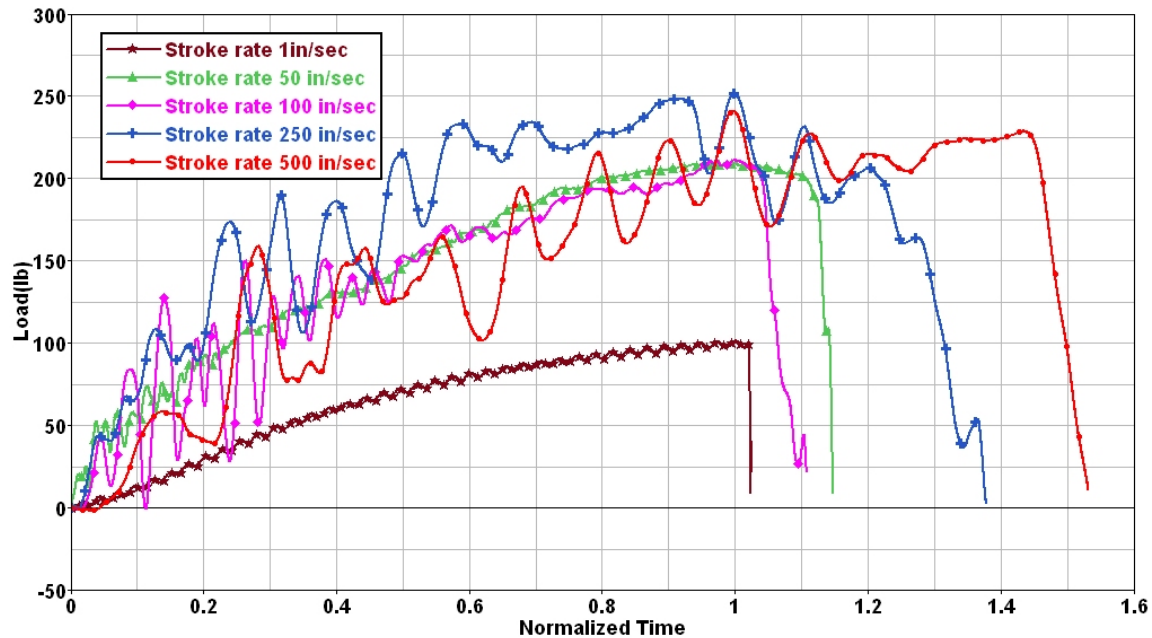
FLEXURE TESTS – Sample results

Peak bending load Vs Normalized time for **Carbon fiber beam specimens at various strokes rates.**



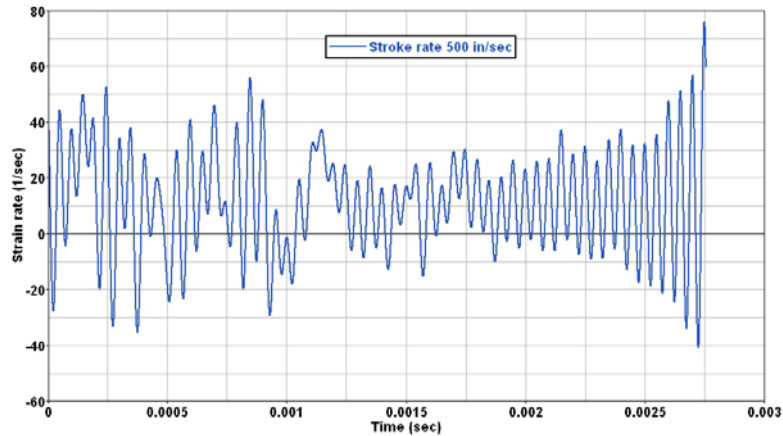
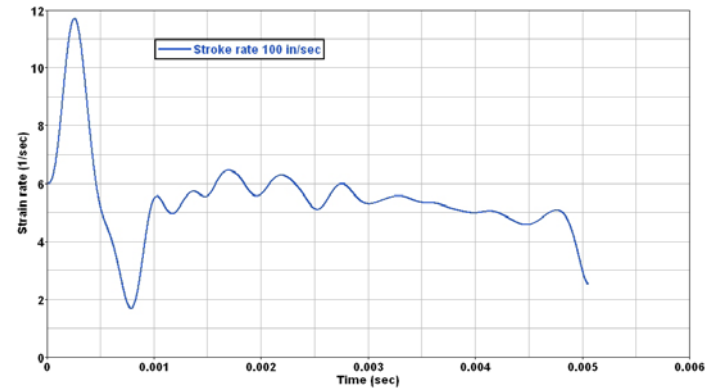
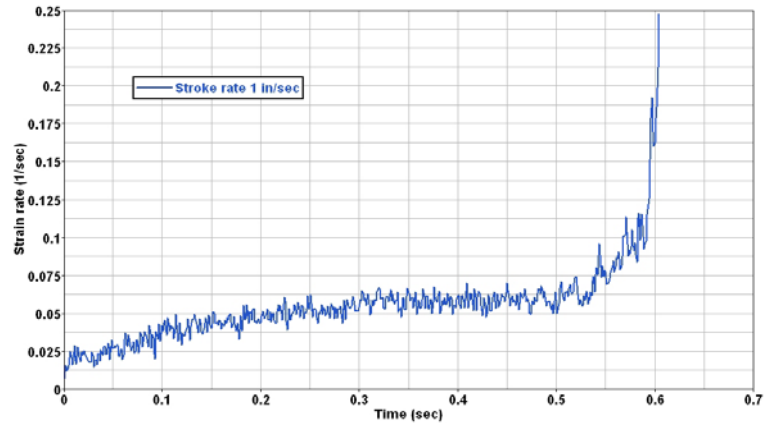
FLEXURE TESTS – Sample Results

Peak bending load Vs Normalized time for **fiberglass beam specimens at various strokes rates**.



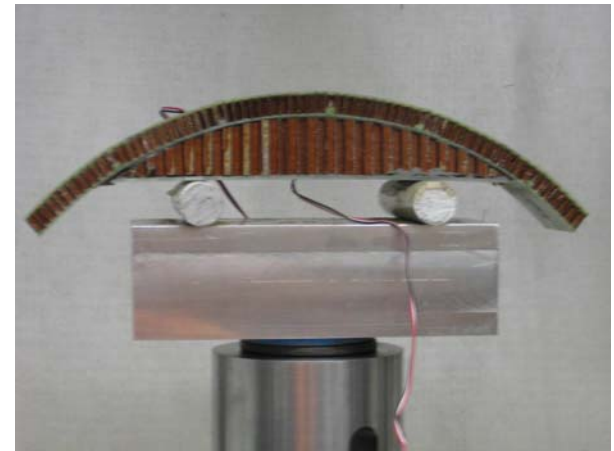
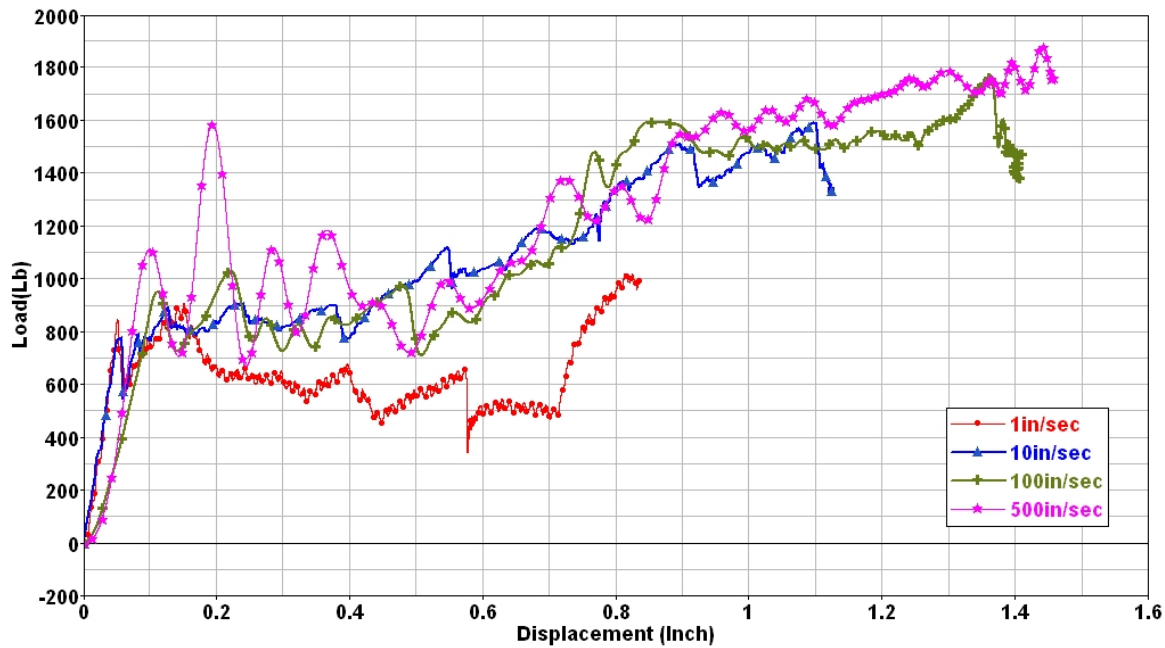
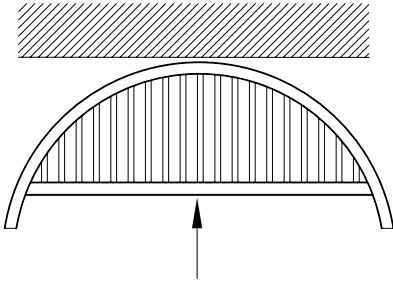
FLEXURE TESTS - RESULTS

Typical strain rates achieved in the gage section of the beams



Maximum strain rate achieved in the test region $\sim 100 \text{ s}^{-1}$

SCALED FUSELAGE SECTION TESTS



Work in Progress

- Rate effects on delamination fracture toughness
 - nearing completion
- Rate effects on behavior of corrugated webs under compression
 - Failure modes
 - Energy absorption
- Signal modulation corrections for test data
- Tensile characterization using SHPB (rates $\sim 10^3$ 1/s)

