

Development of a Multi-Sensor Cargo Compartment Fire Detection Alarm Algorithm

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**Adityanand U. Girdhari
Presented by: David Blake
FAA William J. Hughes Technical Center**

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**Federal Aviation
Administration**



Federal Aviation Regulation 25.858

Requires that the cargo compartment fire detection system provide a visual indication to the flight crew within one minute of the start of a fire.



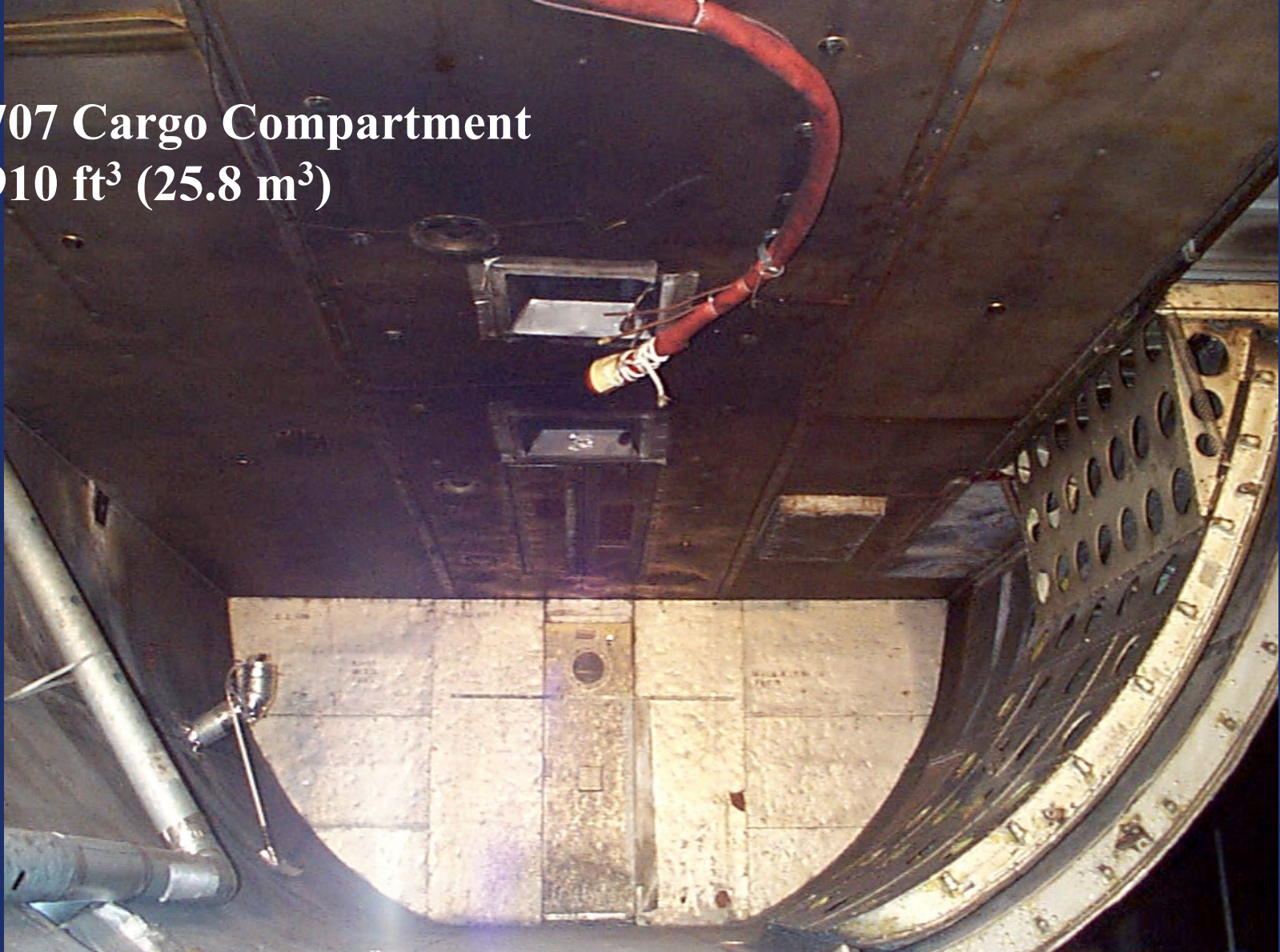
Problem

- The majority of currently installed fire detectors are photoelectric smoke detectors that can not differentiate between smoke particles and other airborne particles such as dust and condensation.
- The ratio of false alarms to the detection of actual fires in the cargo compartments of U.S. registered aircraft is on the order of hundreds to one.



707 Cargo Compartment

910 ft³ (25.8 m³)



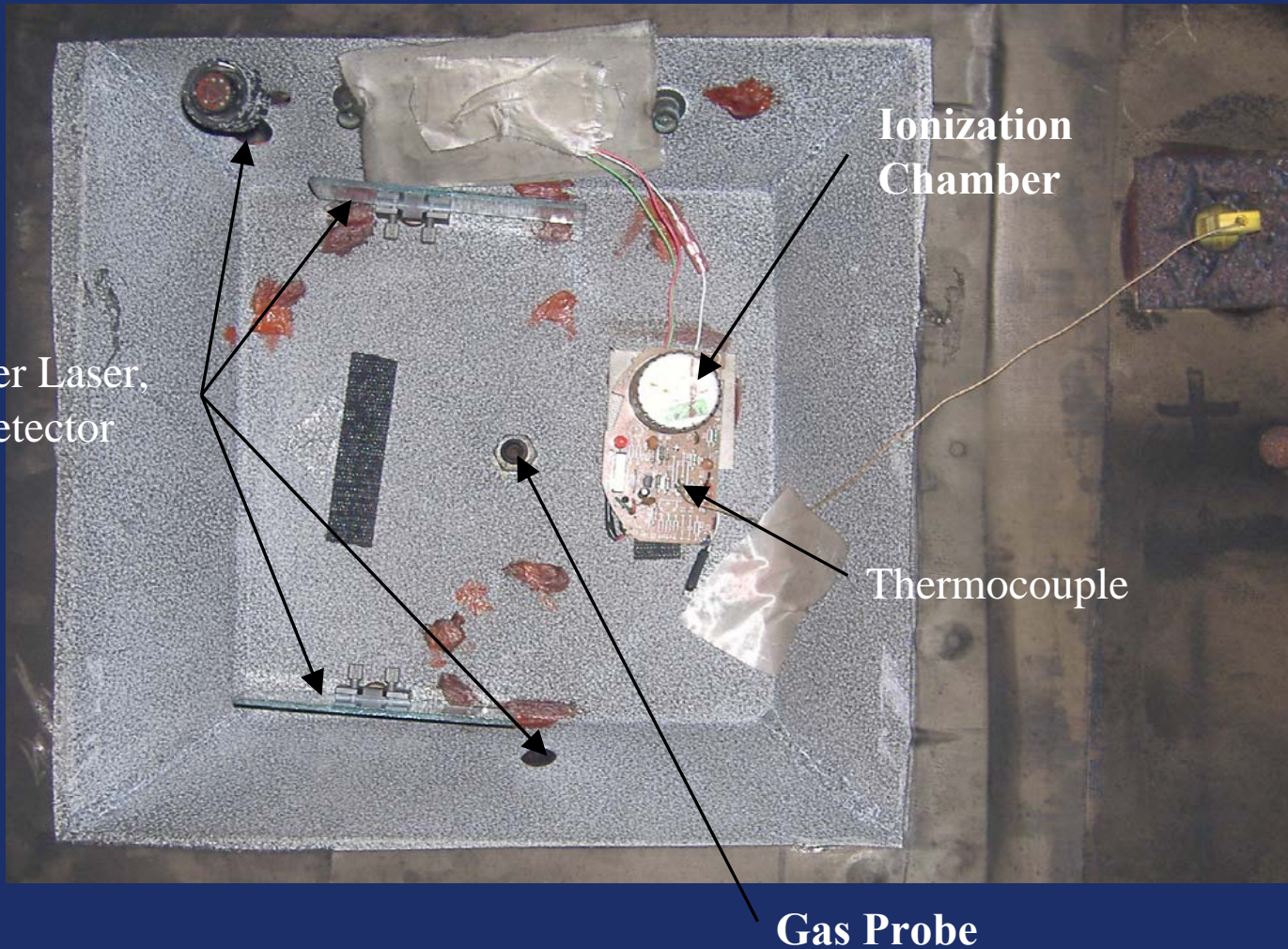
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Recessed pan in 707 ceiling



Fire Sources



Resin Block



Shredded Newspaper



Pan of Alcohol



Alcohol Soaked Rags



Urethane Foam



Suitcase with Rags

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Nuisance Sources



Vaporizer



Heat Gun



Engine Exhaust



Dust



Human Respiration (CO₂)

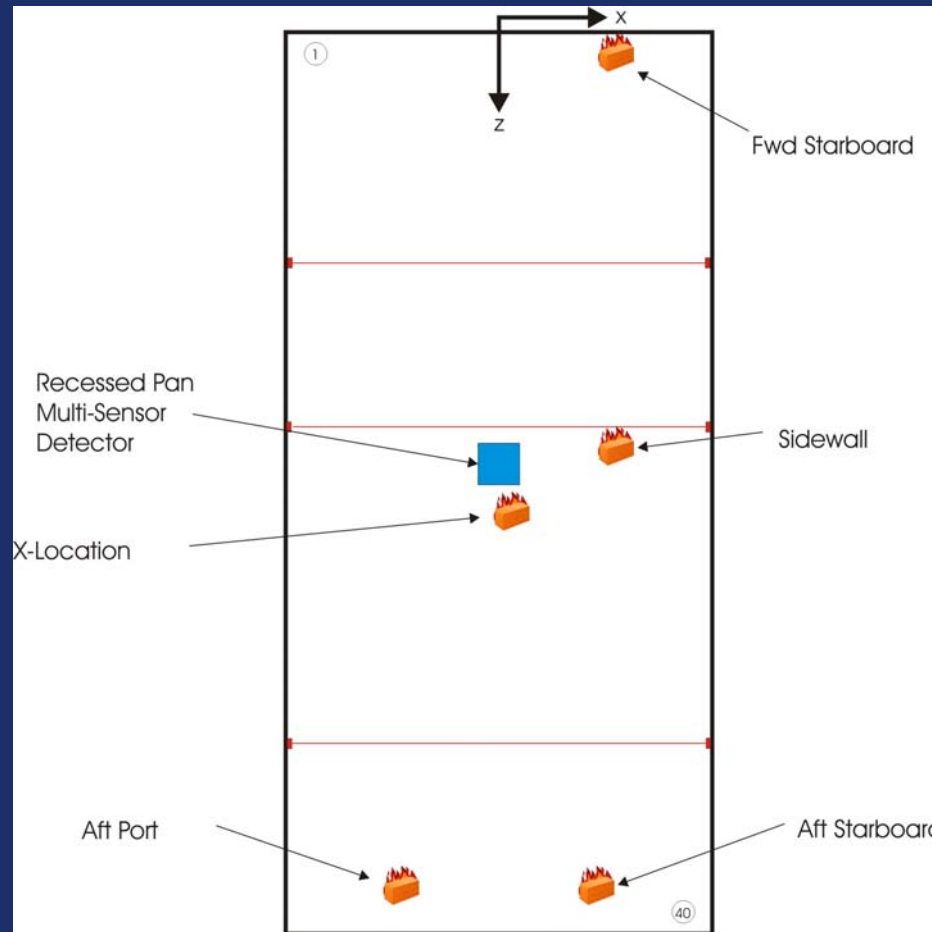
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Tests were conducted at numerous locations throughout the cargo compartment to generate a matrix of sensor readings for various fire and nuisance types and locations.



| | MIC (Volts) | Rate-Rise (Volts/sec) | Smokemeter (%LT/ft) | Rate-Rise (%LT/ft/sec) | CO (ppm) | Rate of Rise CO | CO ₂ (ppm) | Rate of Rise CO ₂ | Temp. Change (°F) | Temp. Rate of Rise |
|----------------------------------|----------------|--------------------------|------------------------|---------------------------|-------------|--------------------|--------------------------|---------------------------------|-------------------------|-----------------------------|
| REFERENCE SOURCE | | | | | | | | | | |
| Resin Block (X Location) | 0.589 | -0.522 | 48.743 | -3.036 | 108.889 | 4.580 | 1497.116 | 49.026 | 9.831 | 0.815 |
| PERIMETER TESTING | | | | | | | | | | |
| Resin Block (Fwd) | 0.583 | -0.246 | 59.959 | -1.522 | 86.243 | 3.571 | 1076.050 | 34.180 | 3.831 | 0.312 |
| Resin Block (Aft) | 0.447 | -0.340 | 55.755 | -0.010 | 88.763 | 2.369 | 997.473 | 58.431 | 6.782 | 0.302 |
| Resin Block (Sidewall) | 0.691 | -0.391 | 53.372 | -2.722 | 94.696 | 2.777 | 1245.117 | 24.185 | 5.352 | 0.332 |
| NUISANCE SOURCE (X Location) | | | | | | | | | | |
| Arizona Test Dust (Container) | 2.801 | -0.694 | 91.276 | -1.798 | 0.088 | 0.047 | 0.135 | 0.078 | 0.037 | 0.018 |
| Vaporizer (Fog formation) | 4.822 | -0.029 | 41.823 | -4.653 | 0.107 | 0.076 | 5.231 | 0.619 | 2.159 | 0.289 |
| Exhaust fumes (Forklift loading) | 4.845 | -0.046 | 94.126 | -0.149 | 493.172 | 45.242 | 712.394 | 55.237 | 0.294 | 0.137 |
| Heat Gun (Heated container) | 1.854 | -0.262 | 49.049 | -3.982 | 0.274 | 0.106 | 0.539 | 0.144 | 22.967 | 0.889 |
| Occupied compartment (Human) | 4.850 | -0.023 | 98.966 | -0.029 | 0.095 | 0.024 | 307.159 | 23.041 | 0.087 | 0.026 |
| PERIMETER TESTING | | | | | | | | | | |
| Arizona Test Dust (Under pan) | 2.705 | -0.713 | 70.513 | -10.582 | 0.045 | 0.028 | 0.103 | 0.087 | 0.046 | 0.031 |
| Arizona Test Dust (2 feet) | 3.110 | -0.665 | 60.638 | -19.684 | 0.045 | 0.028 | 0.103 | 0.087 | 0.046 | 0.031 |
| Arizona Test Dust (4 feet) | 4.990 | -0.038 | 97.366 | -1.308 | 0.045 | 0.028 | 0.103 | 0.087 | 0.046 | 0.031 |
| FIRE SOURCES (X Location) | | | | | | | | | | |
| FLAMING SOURCES | | | | | | | | | | |
| Denatured Alcohol (40 mL) | 4.552 | -0.038 | 86.089 | -1.239 | 1.624 | 0.119 | 1831.611 | 99.377 | 13.154 | 0.529 |



| | | | | | | | | | | |
|---------------------|-------|--------|--------|--------|--------|-------|----------|---------|--------|-------|
| Alcohol-Soaked Rags | 1.430 | -0.322 | 83.655 | -1.184 | 14.191 | 1.428 | 1880.348 | 110.544 | 14.674 | 1.016 |
| Polyurethane Foam | 1.390 | -0.736 | 91.385 | -0.702 | 15.128 | 2.211 | 2098.261 | 321.620 | 23.051 | 2.844 |

SMOLDERING SOURCES

| | | | | | | | | | | |
|--------------------|-------|--------|--------|--------|---------|--------|----------|---------|--------|-------|
| Shredded Newspaper | 1.491 | -0.497 | 51.799 | -2.808 | 171.324 | 24.803 | 1994.328 | 276.974 | 33.145 | 2.398 |
| Suitcase | 1.965 | -0.103 | 64.367 | -1.744 | 372.643 | 10.697 | 346.922 | 9.406 | 1.423 | 0.095 |

PERIMETER TESTING

| | | | | | | | | | | |
|-------------------------------|-------|--------|--------|--------|---------|---------|----------|---------|--------|-------|
| Alcohol-Soaked Rags (Average) | 1.341 | -0.257 | 95.627 | -0.195 | 21.074 | 1.508 | 1885.504 | 83.748 | 4.619 | 0.117 |
| Polyurethane Foam (Average) | 1.216 | -0.247 | 94.604 | -0.373 | 6.703 | 0.779 | 2070.223 | 192.934 | 5.699 | 0.200 |
| Shredded Newspaper (Average) | 0.785 | -0.695 | 72.410 | -2.449 | 157.376 | 19.125 | 1912.648 | 214.622 | 13.945 | 0.391 |
| Alcohol-Soaked Rags (Fwd) | 1.370 | -0.271 | 96.955 | -0.279 | 2426.18 | 112.548 | 1678.543 | 50.625 | 3.659 | 0.166 |
| Polyurethane Foam (Fwd) | 1.278 | -0.501 | 92.476 | -0.754 | 1011.26 | 157.490 | 2044.346 | 385.902 | 5.910 | 0.276 |
| Shredded Newspaper (Fwd) | 0.497 | -0.990 | 74.829 | -1.475 | 1194.61 | 140.035 | 1764.622 | 369.124 | 12.777 | 0.670 |
| Alcohol-Soaked Rags (Aft) | 1.198 | -0.287 | 90.787 | -0.512 | 1385.88 | 172.563 | 2032.288 | 46.734 | 5.055 | 0.139 |
| Polyurethane Foam (Aft) | 1.074 | -0.431 | 94.169 | -0.375 | 838.361 | 43.948 | 2096.167 | 124.795 | 6.656 | 0.225 |
| Shredded Newspaper (Aft) | 0.942 | -0.745 | 69.521 | -3.422 | 1952.91 | 367.176 | 2060.719 | 429.367 | 15.327 | 0.651 |



Five Alarm Algorithms were Designed

1. IF {(CO ppm >2 OR CO₂ ppm >30) AND (°F >3 OR MIC volts <4.7) AND (%LT/ft <97)} THEN →ALARM

Absolute values of gases AND Temperature OR MIC OR Smoke absolute values

2. IF {(d[CO]/dt >1 OR d[CO₂]/dt >10) AND (d[%LT/ft]/dt >0.1 OR d[MIC]/dt >0.1 OR d[°F]/dt >0.15)} THEN → ALARM

Rate of change of gases AND rate of change of Smoke OR MIC OR Temperature

3. IF {(d[CO]/dt >1 OR d[CO₂]/dt >10) AND (d[%LT/ft]/dt >0.1 OR d[MIC]/dt >0.1 OR MIC volts <4.7)} THEN → ALARM

Rate of change of gases AND rate of change of Smoke OR MIC OR MIC absolute

Five Alarm Algorithms were Designed

4. IF {(CO ppm >2 OR d[CO]/dt >1) AND (MIC volts <4.7 OR d[MIC]/dt >0.1 OR °F >3 OR %LT/ft <94 OR d[%LT/ft]/dt >0.15)} THEN → ALARM

CO AND MIC OR Smoke absolute OR rate of change OR temperature rise.

5. IF {(CO₂ ppm >7.5 or d[CO₂]/dt >5) AND (MIC volts <4.7 OR d[MIC]/dt >0.1 OR °F >3 OR %LT/ft <94 OR d[%LT/ft]/dt >0.15)} THEN → ALARM

CO₂ AND MIC OR Smoke absolute OR rate of change OR temperature rise

| | Algorithm | | | | | | |
|---------------------|------------|-------------|------------|------------|-------------|---------------|------------|
| | 1 | 2 | 3 | 4 | 5 | Photoelectric | Ionization |
| Total Tests | 30 | 30 | 30 | 30 | 30 | 30 | 30 |
| | | | | | | | |
| Failure | 4 | 0 | 1 | 1 | 0 | 10 | 8 |
| Successful | 26 | 30 | 29 | 29 | 30 | 20 | 22 |
| | | | | | | | |
| Successful % | 87% | 100% | 97% | 97% | 100% | 67% | 73% |

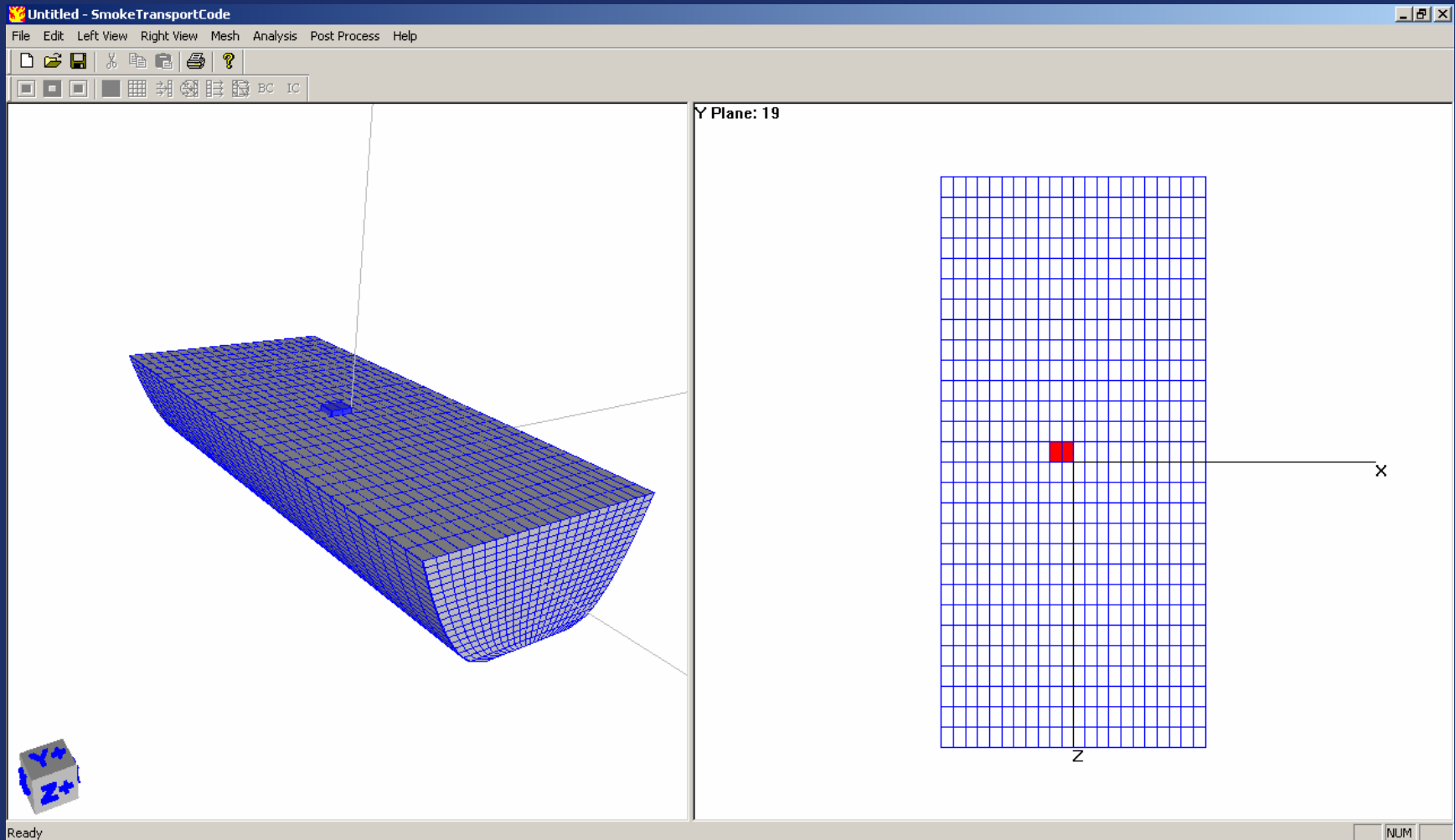
Successful is defined as returning an alarm in less than 60 seconds after the start of a fire and not returning an alarm for any nuisance source.



| Fire Sources | Algorithm | | | | | Photoelectric | Ionization |
|---------------------------|-----------|----|----|----|----|---------------|------------|
| | 1 | 2 | 3 | 4 | 5 | | |
| (X Location) | | | | | | | |
| FLAMING SOURCES | | | | | | | |
| Denatured Alcohol (40 mL) | 114 | 20 | 80 | X | 14 | 118 | X |
| Alcohol soaked rags | 22 | 14 | 14 | 18 | 14 | 32 | 14 |
| Polyurethane foam | 12 | 12 | 12 | 14 | 10 | 38 | 10 |
| SMOLDERING SOURCES | | | | | | | |
| Shredded newspaper | 20 | 16 | 16 | 18 | 16 | 20 | 18 |
| Suitcase | 60 | 44 | 44 | 46 | 44 | 62 | 126 |
| PERIMETER TESTING | | | | | | | |
| Alcohol soaked rags (Fwd) | 202 | 30 | 30 | 34 | 30 | X | 34 |
| Polyurethane foam (Fwd) | 24 | 24 | 24 | 28 | 22 | 22 | 20 |
| Shredded newspaper (Fwd) | 38 | 38 | 38 | 40 | 38 | 34 | 36 |
| Alcohol soaked rags (Aft) | 48 | 36 | 34 | 36 | 32 | 50 | 46 |
| Polyurethane foam (Aft) | 46 | 40 | 40 | 46 | 34 | 52 | 36 |
| Shredded newspaper (Aft) | 46 | 28 | 28 | 30 | 28 | 48 | 22 |



Sandia Cargo Compartment Smoke, Gas and Heat Transport CFD Code



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Comparison of Experimental and Computational Alarm Times

| Fire Sources | Algorithm | | | | | Photoelectric | Ionization |
|--------------------------|-----------|----|----|----|----|---------------|------------|
| | 1 | 2 | 3 | 4 | 5 | | |
| EXPERIMENTAL | | | | | | | |
| Resin Block (X-Location) | 20 | 18 | 18 | 24 | 14 | 20 | 20 |
| | | | | | | | |
| PERIMETER TESTING | | | | | | | |
| | | | | | | | |
| Resin Block (Fwd) | 70 | 48 | 48 | 50 | 48 | 54 | 84 |
| Resin Block (Aft) | 50 | 50 | 50 | 54 | 50 | 50 | 42 |
| Resin Block (Sidewall) | 38 | 26 | 26 | 38 | 26 | 36 | 42 |
| | | | | | | | |
| COMPUTATIONAL | | | | | | | |
| Resin Block (X-Location) | 20 | 18 | 18 | 20 | 18 | 18 | 18 |
| | | | | | | | |
| PERIMETER TESTING | | | | | | | |
| | | | | | | | |
| Resin Block (Fwd) | 70 | 52 | 52 | 52 | 50 | 52 | 82 |
| Resin Block (Aft) | 50 | 50 | 50 | 50 | 46 | 48 | 48 |
| Resin Block (Sidewall) | 28 | 26 | 26 | 28 | 26 | 30 | 34 |



Difference in Alarm Times with Experimental Data Versus Computational Data (Seconds)

| Fire Locations | Algorithm | | | | | | |
|--------------------------|-----------|---|---|----|---|---------------|------------|
| | 1 | 2 | 3 | 4 | 5 | Photoelectric | Ionization |
| Resin Block (X-Location) | 0 | 0 | 0 | 4 | 4 | 2 | 2 |
| Resin Block (Fwd) | 0 | 4 | 4 | 2 | 2 | 2 | 2 |
| Resin Block (Aft) | 0 | 0 | 0 | 4 | 4 | 2 | 6 |
| Resin Block (Sidewall) | 10 | 0 | 0 | 10 | 0 | 6 | 8 |



Conclusions

- **Multi-sensor alarm algorithms can simultaneously reduce false alarms to nuisance sources and increase sensitivity to actual fire sources.**
- **The Sandia smoke transport code is an effective tool to create a virtual smoke detector to test alarm algorithms and proximity to fire response times.**

