

# Use of HFC-125 as a Simulant for Engine/Nacelle Fire Extinguishing Testing

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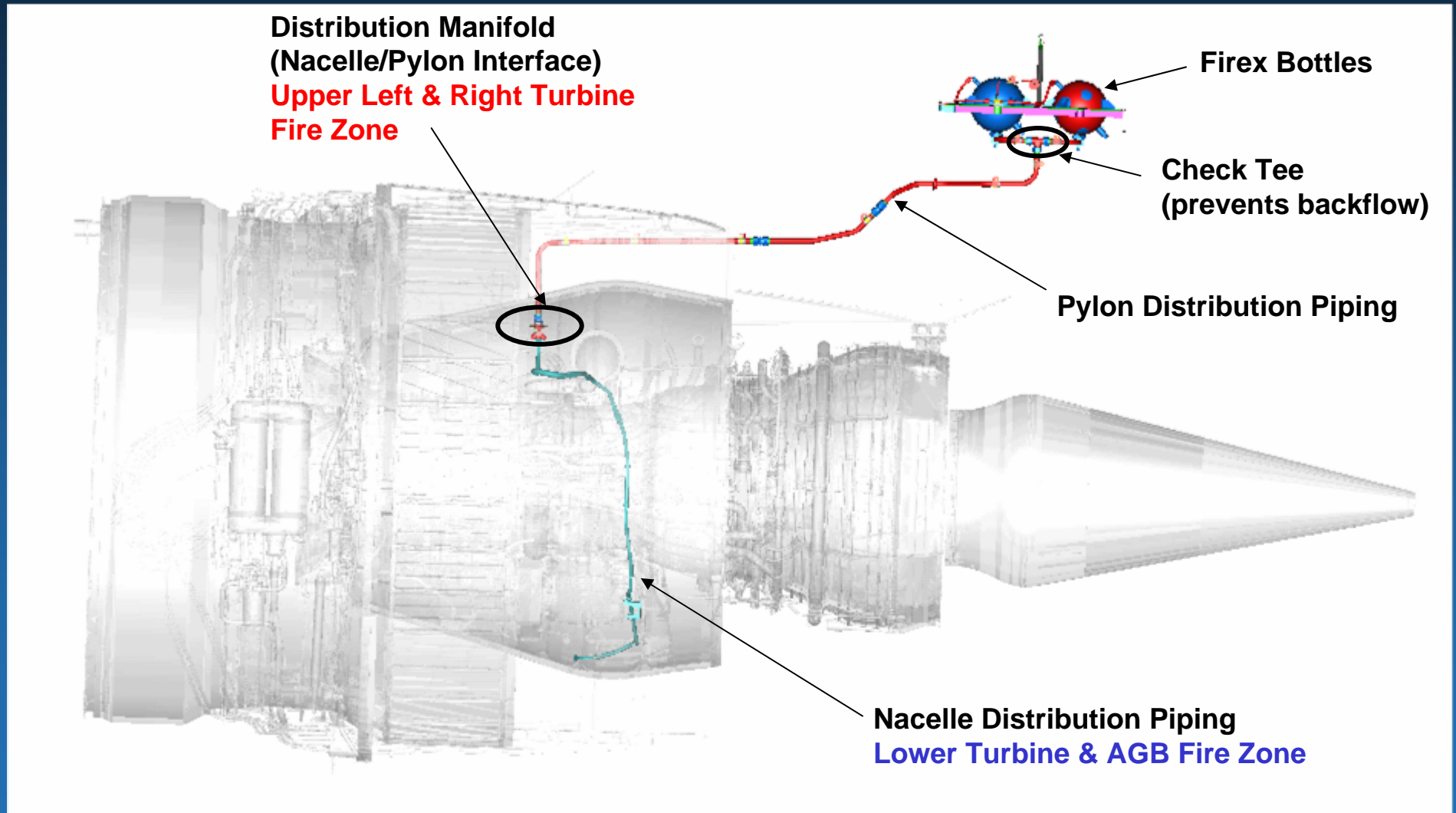
- **Justification**
- **System Description**
- **System Requirements**
- **Agent Comparison**
- **Test Conditions**
- **Test Results**
- **Conclusion**



- **The results presented herein demonstrate the capability to eliminate release of Halon 1301 for development/qualification purposes**



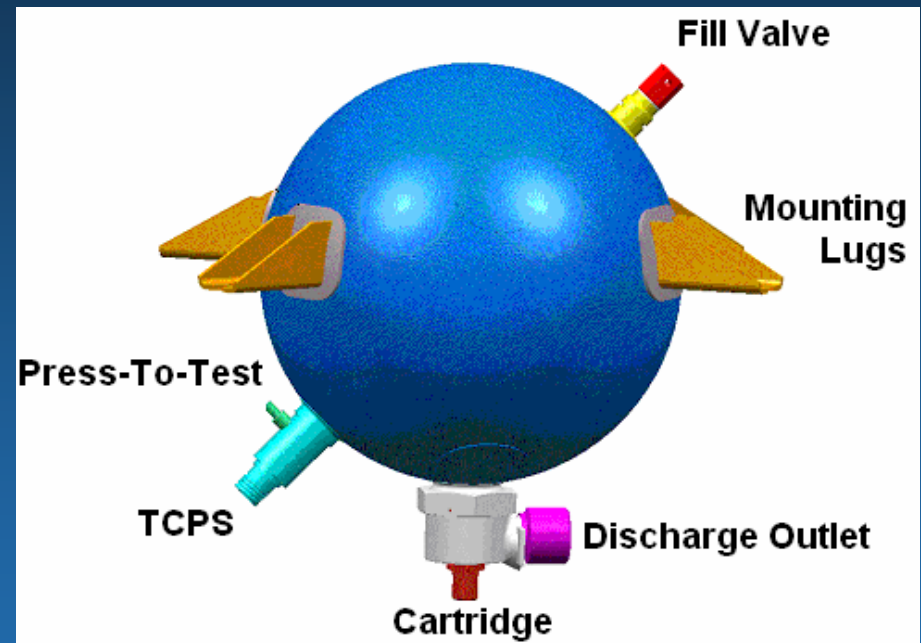
## C-5 Fire Extinguishing (Firex) System



# System Description – Firex Bottles



- **2 bottles** per pylon (“dual shot”)
- **536 in<sup>3</sup>**, hermetically-sealed sphere
- Contains **14 lbs Halon 1301** (CF<sub>3</sub>Br)
- Supercharged with N<sub>2</sub> for faster release
- Operating temp: **-65°F to +250°F**
- Nominal charge pressure: 600 psig
- Electrical current from cockpit ruptures cartridge, releasing pressurized agent thru discharge outlet into distribution piping





- MIL-22285 requires Halon 1301 concentration levels must be greater than **6% by volume in air for a minimum of 0.5 seconds simultaneously** in 12 locations throughout the protected fire zone
  - To guarantee 6%, all Halonyzer channels must = 6.72%
  - AC 20-100 provides requirements for 12 sample probe locations
- **If possible, reduce halon emissions during certification and system development testing by using a simulant agent**
  - **MIL-22285** requires use of HFC-125 for any halon system qual
  - **Clean Air Act 40 CFR 82.270 (b)(3)** requires use of simulant in lieu of halon unless technical reasons prevent
  - **DOT/FAA/AR-TN99/64** defines simulant fill parameters
  - **B777-300ER** certified with simulant by FAA  
(provides Halonyzer system test equipment calibration basis)



- Fill bottle to 77% weight of Halon 1301 (MIL-22285 Sec 4.3.2.2.1)

$$W_{\text{HFC}} = 77\%W_{\text{Halon}}$$

$$W_{\text{HFC}} = (0.77)*(14 \text{ lbs})$$

$$W_{\text{HFC}} = 10.78 \text{ lbs}$$

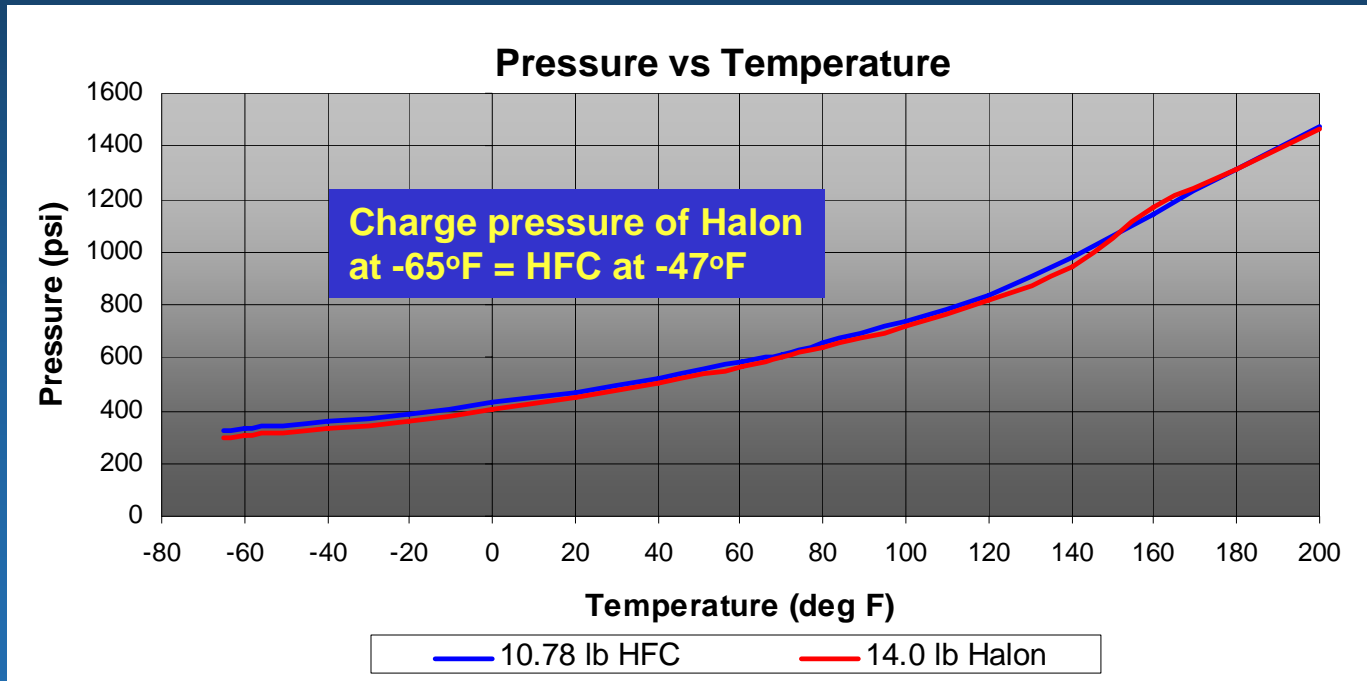
- Nitrogen pressurization of the simulant/test bottle is equivalent to the actual extinguishing system bottle

# Agent Comparison – Physical Properties



- Because of the different gas and liquid characteristics of HFC-125 and Halon 1301, the test conditions were tailored to account for the differences in gas dispersion characteristics, vapor pressure and Jakob's number of the two test materials

Jakob's #,  $Ja_{\text{HFC}, -47\text{F}} = Ja_{\text{Halon}, -65\text{F}} = 0.02$   
Vapor Pressure,  $vp_{\text{HFC}, -47\text{F}} = vp_{\text{Halon}, -65\text{F}} = 17.7 \text{ psia}$



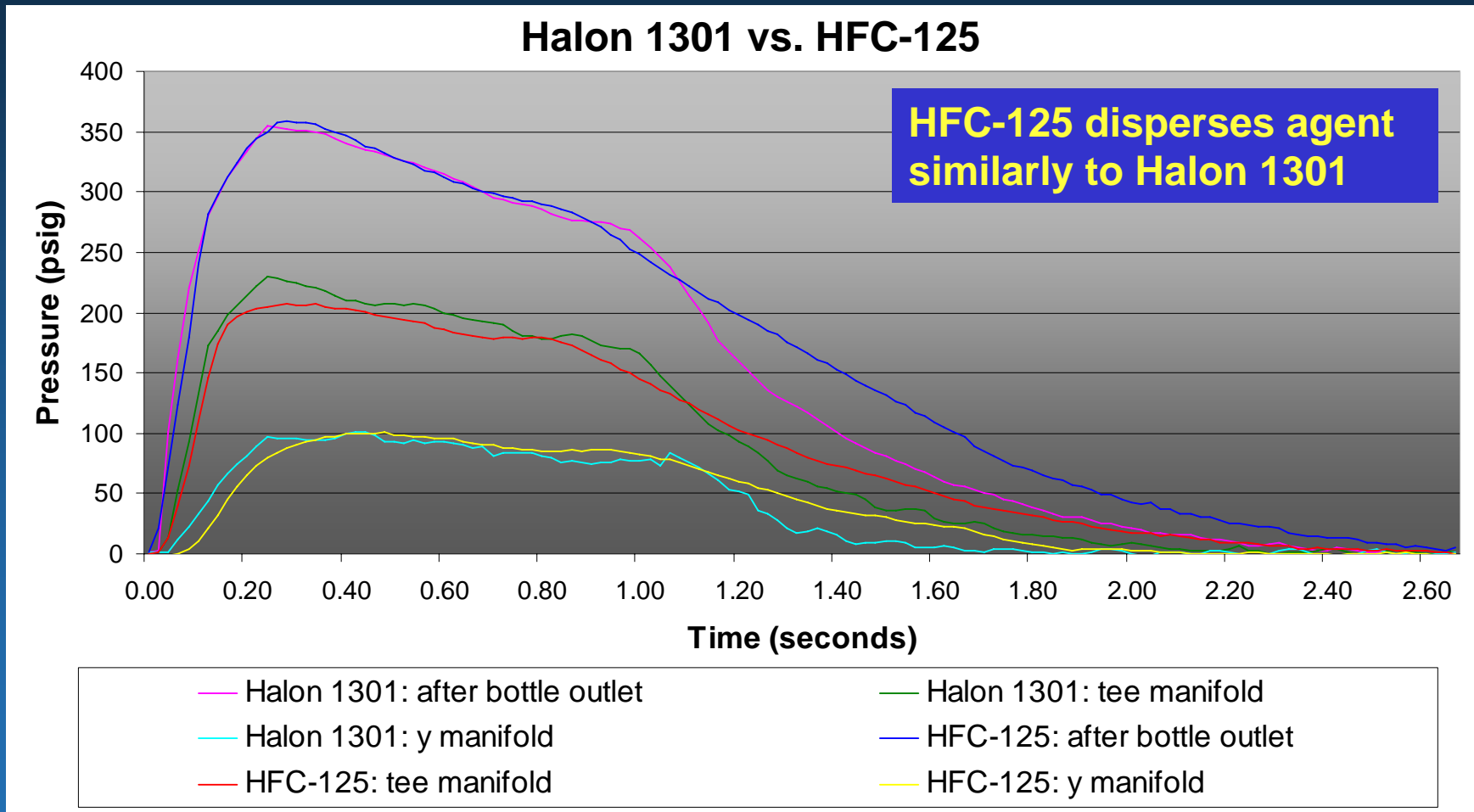
**HFC-125 at -47°F is equivalent to Halon 1301 at -65°F**



# Agent Comparison – Discharge Testing

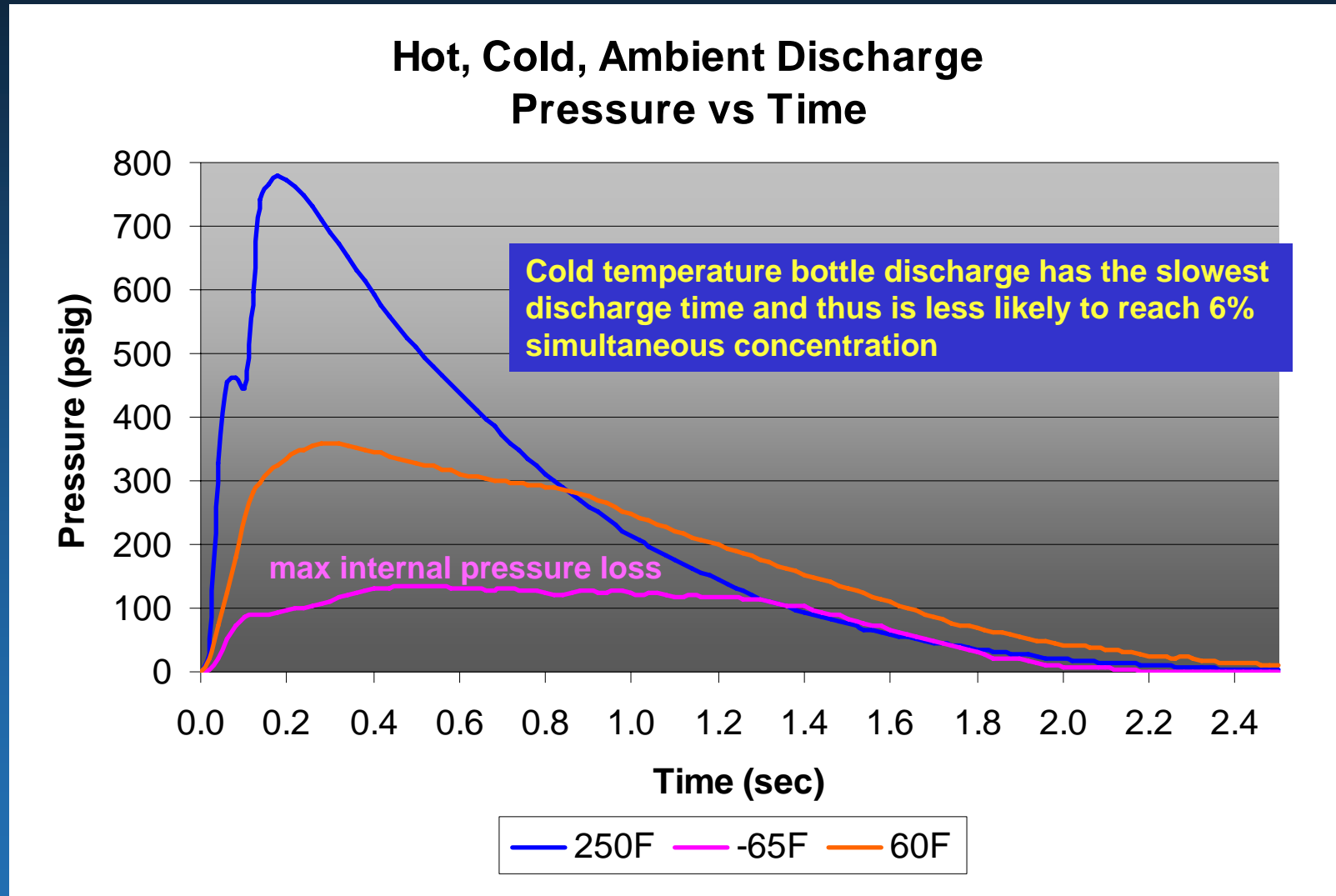


Agent discharge testing was conducted with HFC-125 and compared with Halon 1301 discharge test results



**Based on discharge test results, HFC-125 is a viable simulant for Halon 1301**

# Test Conditions – Bottle Discharge



**Ground test to be conducted with cold-soaked bottle**

# Test Conditions – Dilution Flow



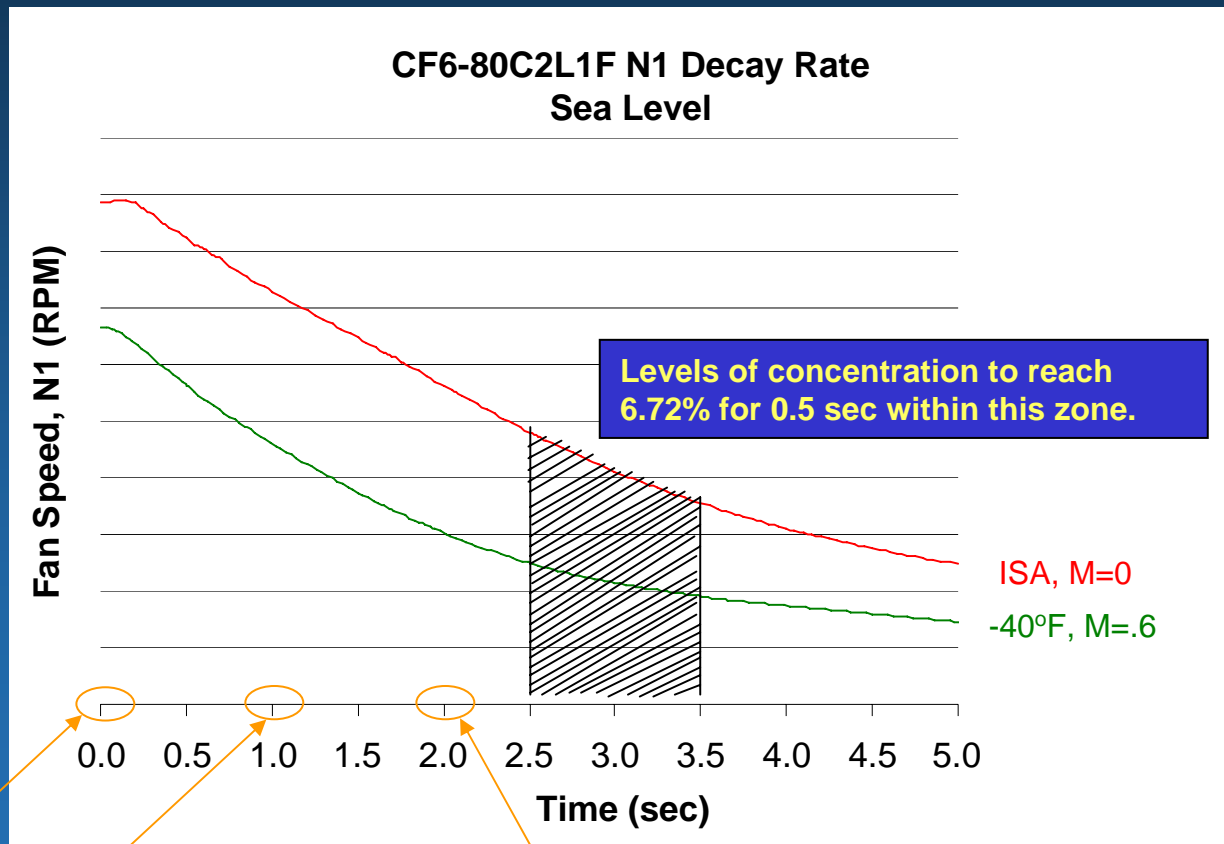
**Dilution flow** is the primary constraint affecting the ability of the agent to diffuse in the nacelle fire zone (i.e. the greater the flow, the more agent needed to extinguish a fire). There are two key parameters to set maximum dilution flow rate:

- 1. Maximum dynamic pressure** occurs at
  - **Max aircraft velocity** (Bernoulli's equation)
  - **Dilution flow DECREASES w/altitude due to density effect so the flight envelope worst-case can be duplicated on the ground**
- 2. Maximum N1**, highest pressure rise across fan & booster stage where core cooling flow is being taken
  - **Discharge of Halon 1301 requires the fire handle to be pulled, shutting off the fuel flow, primary source of fire. But,**
  - **HFC-125 requires a steady state flow so the fire handle cannot be pulled because it shuts down the engine, providing a variable reduction in speed. Instead, the %N1 of the engine at the time the agent reaches the engine must be determined to adequately simulate a fire handle pull**

# Test Conditions – %N1 Decay Rate



- Since HFC-125 requires a steady-state flow, the N1 decay rate is examined to determine the speed at which the engine should be set during ground test
- Calculations take into account the time required for cold day bottle discharge, time to activate fire bottle and time for agent to reach engine



Pull t-handle, engine shutdown

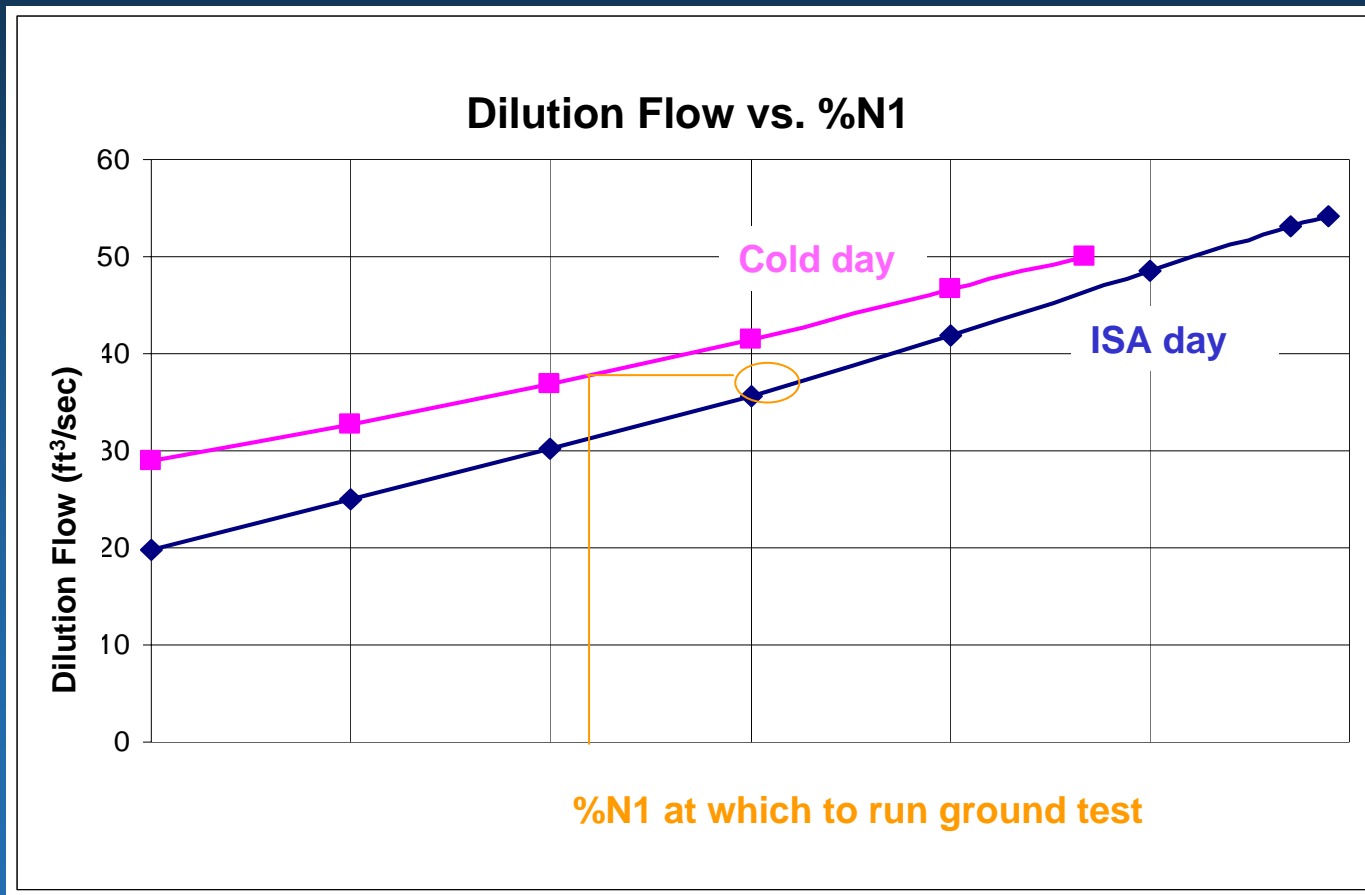
Push agent discharge button

Bottle 90% discharged

# Test Conditions – %N1 Density Correction



- Ground test is conducted with M=0 on a standard day
- To determine correct steady state %N1, a density correction must be performed



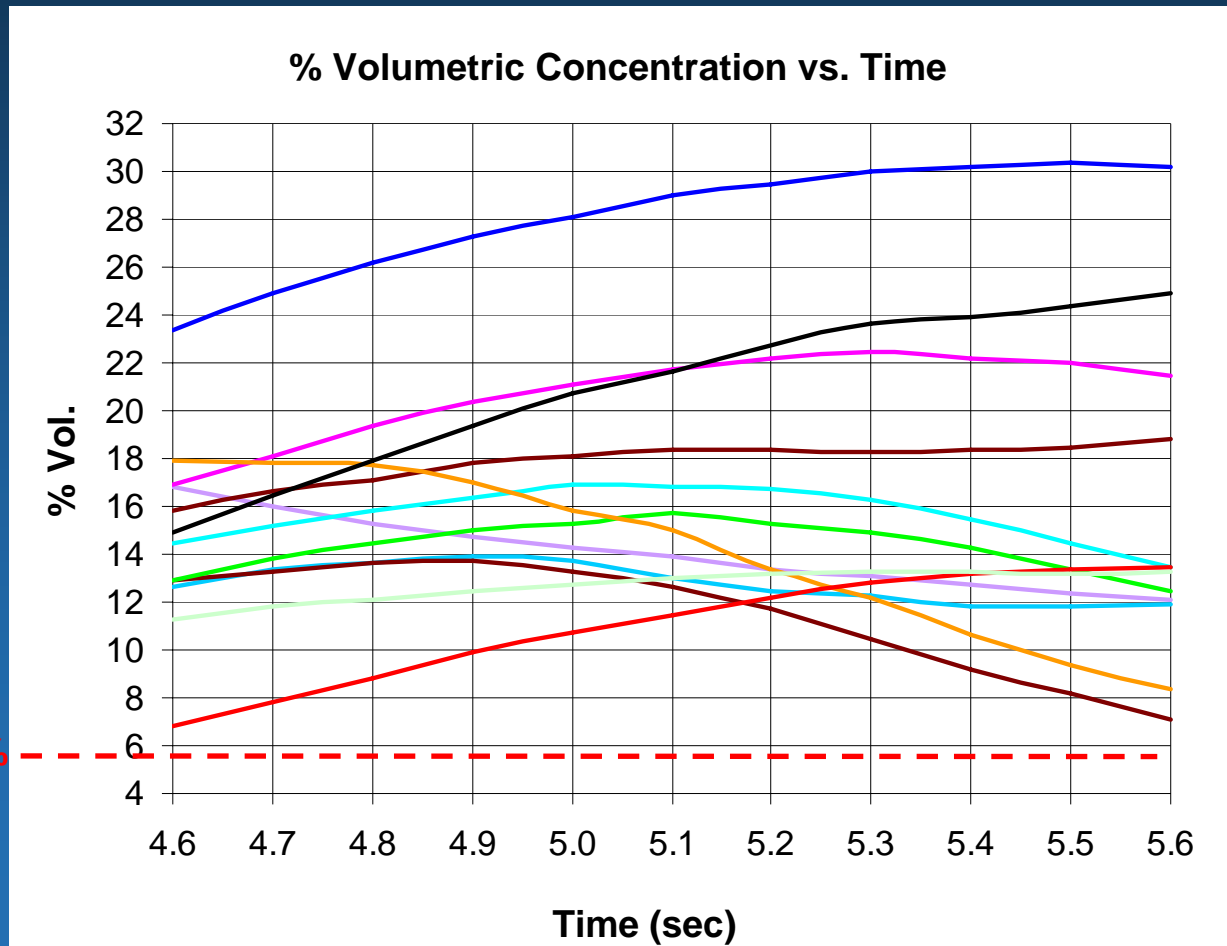


- **Calibration check performed on Halonyzer III System**
  - *Halonyzer authorized for use with HFC-125*
- **Leak check performed on the 12 sampling probes**
- **Insulated 10.78 lb HFC-125 bottle cold-soaked to - 90°F**
  - *Standard day raises bottle temp quickly, even with insulation*
  - *Bottle at -47°F at time of discharge*
- **Relative humidity = 58%**
  - *must be between 25% and 75%*
- **Advanced test engine to required %N1**
  - *Speed stabilized for 1 minute before agent release*

# Test Results



- **March 2006: using HFC-125 as a simulant, the C-5M CF6-80C2L1F engine firex system agent concentration exceeded FAR 25.1195(b) certification requirements**



Concentration levels ranged from 6.8 to 30.2 for 1 full second, **twice** the ½ sec requirement

6.72%



- **HFC-125 successfully simulated an Halon 1301 fire bottle discharge, proving HFC-125 is a viable alternative of Halon 1301**
  - *HFC-125 “environmentally friendly”*
  - *Reduction of Halon 1301 emissions during certification and system development testing (Montreal Protocol)*
- **HFC-125 can be used in lieu of Halon 1301 for purposes other than actual fire extinguishing with the following system modifications**
  - *Refill fire bottle with HFC-125*
  - *Provide steady-state condition*





# Questions?